

NEUTRAL HYDROGEN OBSERVATIONS OF A LARGE SAMPLE OF GALAXIES

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ABSTRACT

A sample of 1787 nearby galaxies has been observed in the 21 cm line with the NRAO 91 m and 43 m telescopes and the Bonn 100 m telescope. A total of 1171 galaxies were detected. The radio observations provide an accurate heliocentric velocity, an H I flux, and a line profile width for each detection. Literature optical magnitudes, dimensions, and morphological types are reduced to common systems and tabulated. Intrinsic luminosities, dimensions, H I masses, and total masses are determined, assuming distances derived from redshifts.

Subject headings: galaxies: redshifts — line profiles — radio sources: 21 cm radiation

1. THE SAMPLE

An extensive program of 21 cm observations of galaxies was motivated by three perceptions.

i) With low noise receivers and large aperture telescopes, we should detect hydrogen line emission from galaxies of late morphological type out to substantial redshifts. For example, with a 4 minute integration on the Green Bank 91 m telescope either of the Magellanic clouds could be detected at a distance of 18 Mpc, and M101 could be detected as far away as 70 Mpc.

ii) Although most redshifts in the literature are of high surface brightness galaxies and, hence, of relatively early morphological types, it is evident from inspection of the nearest groups that late morphological types are numerically predominant outside of large clusters.

iii) Velocities can be determined with sufficient accuracy in the 21 cm line that measurement errors can be essentially eliminated as a source of uncertainty in group and cluster dynamical studies. Moreover, in addition to a redshift, each observation provides an indication of the total mass of a galaxy and the fractional mass in the form of neutral gas.

At the time the program began, before the publication of the *Uppsala General Catalogue of Galaxies* (UGC: Nilson 1973), a satisfactory catalog of late-type galaxies did not exist. The basic reason is that numerous small low surface brightness galaxies which might be quite nearby fall below the cutoff of magnitude limited samples. Because intrinsic luminosities L and dimensions A are related by a power greater than 2 (Heidmann 1967 found $L \propto A^{2.8}$ for spirals), dimensions are more useful than magnitudes for discriminating in favor of nearby

galaxies. Holmberg (1958) knew of this relationship in terms of a dependence between surface brightness and absolute magnitude. It is also possible to discriminate in favor of nearby galaxies on the basis of structural characteristics in galaxies of late morphological type. It was van den Bergh (1960, 1966), with his luminosity classifications, who promoted the use of morphological characteristics as distance estimators. Although there can be considerable uncertainty in distances obtained in this manner (Fisher and Tully 1975; Tammann, Yahil, and Sandage 1979), the method is certainly useful for a factor of 2 guess at a redshift.

A list of candidates was compiled upon a complete reinspection of the Palomar Observatory Sky Survey (POSS) by RBT. The basic selection criterion was that, based on morphology, a candidate was expected to have a redshift less than 2000 km s^{-1} . The hope was to achieve a high degree of completeness to a redshift of 1000 km s^{-1} . Additionally, there was a lower size limit of $1'$ by our estimate, which proves to be equivalent to a UGC diameter of $\sim 1'.5$. There was no explicit cutoff toward early types, but there is obvious incompleteness earlier than type Sc, both because of the difficulty in evaluating structure in high surface brightness objects on the POSS and because of the deficiency of neutral hydrogen in these objects. Galactic latitude was not a consideration in the selection process. The survey for candidates to the southern limit of $\delta = -45^\circ$ of the Green Bank telescopes required the use of the Whiteoak extension of the POSS at declinations below -33° . It was evident at the time, and the ESO and SRC sky surveys have provided ample confirmation, that we were failing to select many objects in the declination interval $-33^\circ > \delta > -45^\circ$ that would have been selected as candidates at more northerly declinations. Our *initial*

¹Operated by Associated Universities, Inc., under contract with the National Science Foundation.

candidates list also excluded galaxies for which systemic velocities were known at the time the list was compiled. This initial list of objects covering the sky with $\delta > -45^\circ$ contained 1250 entries.

Subsequently, we expanded our sample in two ways. In the first place, the UGC became available and provided a means of checking on our completeness. All galaxies in the UGC, except ellipticals, with UGC diameters $3'$ or greater, and all late systems (de Vaucouleurs 1959 types Sd to Im) with diameters $2'$ or greater were observed if they were not on our original list and did not have a known redshift. There were 283 galaxies in this supplementary list which, unfortunately, covers only the northern sky down to $\delta = -2^\circ 30'$. If we were properly interpreting morphological characteristics in terms of a distance, and if our original list were reasonably complete, then the galaxies in this supplementary list should *not* be detected at low redshifts. It will be seen that, with few exceptions, they are not.

We also extended our sample to include ~ 250 galaxies which did have known velocities less than 3000 km s^{-1} . Galaxies were observed if their redshifts were poorly established, or if their neutral hydrogen properties were unknown, or, particularly, if they were potentially useful for the determination of the extragalactic distance scale through the intrinsic luminosity-line profile relationship (Tully and Fisher 1977).

In summary, our sample was meant to include all galaxies north of $\delta = -45^\circ$ with dimensions on the UGC scale of $1/5$ or greater and systemic velocities less than 2000 km s^{-1} . However, it is manifestly incomplete for morphological types earlier than Sc, systemic velocities greater than 1000 km s^{-1} , dimensions less than $2'$, declinations less than -33° , and galactic latitudes within 30° of the plane. In total, we observed 1787 galaxies in the 21 cm line.

II. RADIO OBSERVATIONS

The radio observations were made by JRF, mainly with the 91 m telescope at Green Bank. Galaxies which lie below the 91 m southern limit of $\delta = -19^\circ$ or which would be substantially resolved by the $10/8$ beam of this telescope were observed with the 43 m telescope, with a beamwidth of $22'$. The Max-Planck-Institut 100 m telescope was used to observe some sources in the interval $-30^\circ < \delta < -19^\circ$ which required better resolution and to observe some of the northern sources in the interval $11^h < \alpha < 13^h$ because the 91 m transit telescope could not cope with the pileup of sources at these right ascensions.

With each of the NRAO telescopes, the receiver was a two channel, dual polarization cooled paramp with a system temperature of $\sim 50 \text{ K}$. A 384 channel autocorrelation spectrometer sampled the spectrum in two polarizations, with each section of 192 channels covering a bandwidth of 10 MHz. In the vast majority of cases the

systemic velocity of the candidate was unknown, so the bandpasses in the two polarizations were offset by 7.8 MHz to provide velocity coverage from -400 to $+3000 \text{ km s}^{-1}$ heliocentric. Occasionally, if a galaxy was not detected in this velocity interval, the range 2600 to 6000 km s^{-1} was searched. However, no systematic effort was made to detect galaxies at redshifts above 3000 km s^{-1} . If a systemic velocity was known from the literature or suspected from an earlier observation, candidates were observed with the bandpasses for the orthogonal polarizations both centered at the frequency of expected detection, and there was a consequent gain in sensitivity of $\sqrt{2}$. The velocity resolution after Hanning smoothing was normally 22 km s^{-1} half-power width. Certain objects known to have intrinsically narrow profiles were observed with a resolution of 5.5 km s^{-1} .

Each observation involved taking the difference between an on-source integration and an off-source integration of equal duration from a location at least four beamwidths removed. Integration times with the 91 m were 4 minutes "on" and 4 minutes "off," and with the 43 m were 1 hr "on" and 1 hr "off," with a 10 minute on-off cycle. In view of the difference in apertures, the limiting sensitivities were the same with the two telescopes: without averaging orthogonal polarizations, ~ 5 times rms noise $= 0.09 \text{ Jy}$. The detection limit for one observation with the polarization channels split is $2 \times 10^6 M_\odot \text{ Mpc}^{-2}$ of neutral hydrogen in the case of a line width of 100 km s^{-1} . Details of the system calibration are discussed by Fisher and Tully (1975).

The 100 m observations were made with a single channel, uncooled parametric amplifier with a system temperature of $\sim 80 \text{ K}$ and 384 channel autocorrelation spectrometer split into two sections of 192 channels each. The 192 channels covered a total bandwidth of 10 MHz, and when the systemic velocity of the observed object was known, the spectra from the two sections were averaged to recover some of the $2/\pi$ loss in sensitivity due to one-bit sampling. The observing procedure was essentially the same as was used on the NRAO telescopes with 6 minute "on," 6 minute "off" integration times. The sensitivity limit of the 100 m observations was very nearly the same as with the 91 and 43 m telescopes ($5\sigma \approx 0.09 \text{ Jy}$). Flux density calibrations were made with a number of continuum sources which were also used to calibrate the NRAO telescopes. In addition, six small galaxies with strong H I emission were observed with all three telescopes to check for systematic differences in calibrations. None was found above the 3% level. The beamwidth of the 100 m at 21 cm is $8/5$.

In general, no attempts were made to map the sources. In fact, the larger candidates were looked at with the smaller telescope so that the observed fluxes would more closely represent global measurements. However, either drift scans or maps were made in the vicinity of certain sources suspected of confusion with neighbors or with local emission.

III. THE CATALOG

The results of the survey are presented in three tables. The main catalog is Table 1 which contains information on all galaxies with a firm H I detection and a corrected systemic velocity less than 3000 km s^{-1} . The entries in Table 2 are galaxies with firm H I detections but with systemic velocities *greater than* 3000 km s^{-1} . This separation into two tables serves to emphasize the haphazard nature and the limited number of detections above 3000 km s^{-1} . Finally, Table 3 identifies those candidates which did not have detectable H I within our bandpass, or which were confused with a neighbor at our resolution. The information provided with each entry is described below.²

a) Names

The primary identification for each galaxy is, by order of preference, the *New General Catalogue* number (N), the *Uppsala General Catalogue* number (U), or a name constructed out of the equatorial coordinates. Index catalog numbers are not used because they are not numerous and are difficult to locate by right ascension.

Alternate names are given in the last column of each table. On the first line and in the last files of the second line are other names commonly used to identify the given system. An explanation or source for each name is given in Table 4. On the second line associated with each galaxy (Tables 1 and 2 only) the first entry is the UGC number (often redundant), followed by the identification number in the *Morphological Catalogue of Galaxies* (MCG; Vorontsov-Velyaminov, Krasnogorskaya, and Arkipova 1962–1974), and the code “2” if the galaxy also appears in the *Second Reference Catalogue* (RC2; de Vaucouleurs, de Vaucouleurs, and Corwin 1976).

b) Coordinates

Right ascension and declination for the epoch 1950.0 are given in column 2, lines 1 and 2 (accurate to $\sim 1'$). Sources are the *Catalogue of Galaxies and Clusters of Galaxies* (CGCG; Zwicky *et al.* 1961–1968), the UGC, the MCG, the RC2, or the discovery reference. Galactic longitude and latitude are given in column 3, lines 1 and 2. The galactic poles are taken to lie at $12^{\text{h}}49^{\text{m}}0$, $+27^{\circ}24'$ and $0^{\text{h}}49^{\text{m}}0$, $-27^{\circ}24'$. Supergalactic longitude and latitude (RC2) are given in column 4, lines 1 and 2. The supergalactic poles are taken to lie at $18^{\text{h}}52^{\text{m}}8$, $+15^{\circ}37'$ and $6^{\text{h}}52^{\text{m}}8$, $-15^{\circ}37'$.

c) Morphological Types

The *revised Hubble classification* introduced by de Vaucouleurs (1959, see the RC2 for modifications) is

² Column and line identifications pertain specifically to Tables 1 and 2. The format of Table 3 is slightly different, but the information that has been tabulated is analogous.

given in column 5. We have added two divisions to this system: spiral galaxies of ambiguous subclass are designated $T=12$, and galaxies sufficiently peculiar that they cannot be categorized are designated $T=13$. The compact blue irregulars that are called $T=11$ in the RC2 fall in either $T=10$ or $T=13$ in this catalog.

The presence or absence of a *bar* is signaled in the space following the morphological type, using de Vaucouleurs' terminology “B” for bar, “A” for no bar, and “X” for the intermediate case (cf. RC2). A blank indicates a lack of information. If there is a “P” following the information regarding a bar then the galaxy has some significant morphological *peculiarity*.

The primary sources for the morphological classifications were the first reference catalog (BGC; de Vaucouleurs and de Vaucouleurs 1964) and the UGC, since these data were tabulated before the publication of the RC2 and were subsequently found to be generally consistent with that source. In instances where substantial discrepancies came to our attention the RC2 classification was preferred. Alternative sources are Sandage (1978), van den Bergh (1960, 1966), the ESO Uppsala Survey (Holmberg *et al.* 1974–1979), or our estimates from the POSS. Whatever the source, an attempt was made to interpret the type in de Vaucouleurs' revised Hubble system. We have not carried a measure of the uncertainties in the morphological classifications. The reader is referred to the RC2 and the UGC for this information.

d) Dimensions

Given in column 6, line 1 is the *major diameter* in arc minutes on the Holmberg (1958) system, corrected for galactic absorption. The *galactic absorption correction factor* is listed in column 6, line 2. The *ratio of the minor axis to major axis dimensions* is given in column 7, line 1, and the *inclination* of the galaxy is given in column 7, line 2. The source priorities for dimensions are, in order, Holmberg (1958), the UGC, the MCG, and the BGC.

Conversions of the major axis dimensions from the UGC, MCG, or BGC to the Holmberg scale use the relations derived by Paturel (1975):

$$\log a_H = c_j \log a_j + k_j. \quad (1)$$

The subscripts stand for Holmberg (H), the UGC ($j=N$ for Nilson), the MCG ($j=V$ for Vorontsov-Velyaminov), and the BGC ($j=D$ for de Vaucouleurs). The coefficients c_j and k_j are recorded in Table 5. These adjustments are very similar to those proposed by Dickel and Rood (1978).

Major axis diameters were adjusted to account for the effects of galactic obscuration:

$$a_H^b = a_H f_a, \quad (2)$$

TABLE 1
MAIN CATALOG

NGC/UGC	α	δ	ℓ	SGL	T	b	a_H	r_H	B_T^j	V	σ	W_{20}	tel.	F_c	A_H	log L	log M_T	$\%M_H/M_T$	M_T/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)
U 17	1.1	106.21	308.19	9	4.4	0.70	0.26	0.70	0.26	881.	107	107	1	1.70	14.0	9.78	9.78	3.3	DDO 222	
	1457	-46.09	16.10	4X	1.01	4.7	0.26	4.7	0.26	1081.	20	20	1.07	0.53	42.0	10.37	8.30	1.6	17 02-01-017 2	
N 7817	1.4	108.23	313.86	4X	5.7	0.34	11.58	0.34	11.58	2316.	403	403	1	3.82	42.0	-20.44	11.18	3.0	6.4	
	2029	-40.75	17.13	78	1.01	0.47	0.85	0.47	0.85	2532.	15	15	1.08	1.42	22.5	10.74	9.39	0.10	19 03-01-021 2	
0003-41	3.8	332.83	253.58	78	5.1	0.47	0.43	0.47	0.43	1542.	314	314	2	7.21	22.5	10.74	10.74	3.0	0.10	
	-4146	-72.92	-1.55		1.00	6.4	0.43	6.4	0.43	1502.	20	20	1.02	1.35	11.8	9.21	9.21		-7-01-009 2	
N 14	6.2	108.13	309.05	10	4.4	0.85	12.11	0.85	12.11	860.	143	143	1	5.15	13.7	9.40	10.29	2.9	7.9	ARP 235, VV 80
	1532	-48.83	15.02	5A	1.01	3.3	0.19	3.3	0.19	1059.	10	10	1.08	0.67	13.9	-18.02	8.76	0.23	75 03-01-026 2	
N 24	7.4	43.65	269.42	5A	8.6	0.33	11.33	0.33	11.33	561.	222	222	2	12.28	13.9	9.21	10.17	2.9	0.23	UGCA 2
	-2515	-80.44	3.23		1.00	7.4	0.78	7.4	0.78	595.	10	10	1.04	1.26	11.8	-17.54	8.64	0.27	0.23	UGCA 2
0007-18	7.7	73.84	275.80	10	2.5	0.94	0.08	0.94	0.08	1546.	35	35	3	1.96	11.8	9.40	10.29		7.9	UGCA 3
	-1833	-77.03	5.32		1.00	20.	0.08	20.	0.08	1611.	5	5	1.03	0.38	25.1	8.71	8.71		0.27	-3-01-021
U 99	8.1	108.05	307.03	9	4.4	1.00	0.12	1.00	0.12	1744.	98	98	1	2.59	25.1	8.92	10.17	3.7	18.2	99 02-01-023
	1325	-48.00	14.11	10	1.01	0.23	13.64	0.23	13.64	1935.	10	10	1.09	0.39	12.0	8.78	8.99	12.8	0.66	
U 122	10.7	110.01	310.52	10	3.9	0.23	13.64	0.23	13.64	848.	113	113	1	3.64	12.0	8.78	8.99		0.66	
N 45	16.5	-44.88	18.23	8A	10.0	0.39	10.96	0.39	10.96	1048.	10	10	1.04	0.59	14.9	-16.46	8.60	5.4	0.88	122 03-01-028
	-2327	-80.64	2.94		1.00	3.9	0.14	3.9	0.14	511.	7	7	1.09	2.98	23.5	9.22	10.43		16.1	UGCA 4, DDO 223
U 156	14.2	109.80	306.03	10	4.4	0.70	13.79	0.70	13.79	1135.	152	152	1	3.18	17.0	8.92	10.17	3.7	18.2	UGCA 3
	1204	-49.64	12.35	9	1.01	4.7	0.25	4.7	0.25	1318.	10	10	1.07	0.68	15.1	-16.81	8.74		0.88	-3-01-021
U 191	17.6	110.62	304.78	9	3.9	0.82	13.88	0.82	13.88	1144.	142	142	1	4.40	15.1	8.88	10.25	4.3	23.8	99 02-01-023
N 100	21.5	113.50	310.56	5	7.8	0.20	12.38	0.20	12.38	1320.	238	238	1	0.73	23.5	-16.72	8.88		0.66	122 03-01-028
	1612	-45.89	11.58		1.01	90.	0.74	90.	0.74	1035.	10	10	1.14	1.24	17.0	-17.70	9.13	3.3	0.30	UGCA 4, DDO 223
U 260	24.5	113.47	305.89	5	4.5	0.30	12.57	0.30	12.57	2131.	291	291	1	9.40	30.5	9.89	10.74	9.0	7.1	231 03-02-009 2
U 300	27.5	112.57	298.19	10	2.3	1.00	0.96	1.00	0.96	2305.	20	20	1.05	1.27	10.0	-19.24	9.70		0.64	156 02-01-029
N 134	27.9	338.22	262.85	4X	10.6	0.34	10.28	0.34	10.28	1488.	504	504	4	36.35	48.8	10.47	11.43	3.3	9.1	191 02-01-033 2
	-3332	-82.37	-3.55		1.00	7.4	0.74	7.4	0.74	1572.	10	10	1.07	3.80	16.1	-20.70	9.95		0.30	300 00-02-000
U 328	30.8	112.72	293.93	98	2.6	1.00	0.07	1.00	0.07	1984.	149	149	1	4.12	16.1	8.92	10.74	9.0	7.1	-6-02-012 2
0031-31	-124	-63.64	4.90	9	3.3	0.87	0.10	0.87	0.10	2107.	10	10	1.03	0.73	15.2	9.26	9.26			328 00-02-070
	31.7	347.90	265.50	9	3.3	0.87	0.10	0.87	0.10	1585.	79	79	2	4.50	15.2	9.88	9.88	14.1	0.64	UGCA 6, DDO 224
N 150	31.8	22.06	268.38	48P	5.8	0.56	11.44	0.56	11.44	1593.	329	329	2	10.41	27.1	10.02	10.92	3.2	7.8	UGCA 7
	-2804	-86.14	-2.82		1.00	5.8	0.50	5.8	0.50	1601.	15	15	1.03	1.47	23.0	-19.58	9.43		0.25	-5-02-018 2
0033-25	33.4	58.78	270.80	8X	5.0	0.74	0.16	0.74	0.16	1557.	145	145	2	7.60	23.0	10.32	10.32	9.0		1C 1558, UGCA 8, DDO 225
	-2539	-86.10	-2.49	10	1.00	4.3	0.46	4.3	0.46	1574.	20	20	1.02	0.84	15.2	9.27	9.27			-4-02-024 2
0040-22	40.7	101.53	274.28	10	3.8	0.45	0.46	0.45	0.46	361.	81	81	2	1.55	4.3	8.84	8.84	3.4		1C 1574, UGCA 9, DDO 226
U 477	43.6	121.25	314.78	9	5.1	0.50	13.39	0.50	13.39	388.	20	20	1.01	0.39	42.0	9.74	10.77	11.2	10.6	-4-02-043 2
	1913	-43.36	7.17		1.01	7.7	0.99	7.7	0.99	2657.	256	256	1	8.07	42.0	-18.88	10.77		1.19	477 03-03-002
0043-11	43.6	118.11	284.79	9X	3.6	0.78	0.15	0.78	0.15	1617.	98	98	1	3.90	17.7	9.93	9.93	13.0		DDO 5
	-1148	-74.35	-1.00		1.00	40.	0.44	40.	0.44	1688.	10	10	1.05	0.62	15.5	9.26	9.93			-2-03-009 2
N 247	44.6	113.87	275.97	7X	28.0	0.36	8.72	0.36	8.72	159.	218	218	4	17.47	15.5	-17.67	10.22	3.8	9.0	UGCA 11
	-2101	-83.54	-3.71		1.00	72.	0.67	72.	0.67	190.	5	5	1.46	6.14	27.3	9.26	8.80		0.35	-4-03-005 2
0045-10	45.2	119.86	286.45	58	4.7	0.23	13.46	0.23	13.46	1346.	153	153	1	3.74	19.5	9.97	9.97	8.1		UGCA 14
	-1011	-72.76	-0.94		1.00	83.	1.14	83.	1.14	1423.	7	7	1.06	0.77	2.6	8.88	8.88			-2-03-016 2
0047-21	47.4	119.55	275.90	10	2.7	0.46	0.44	0.46	0.44	303.	47	47	2	1.07	2.6	8.15	8.15	8.2		UGCA 15, DDO 6
	-2116	-83.85	-4.40		1.00	65.	0.44	65.	0.44	331.	8	8	1.01	0.50	14.4	7.07	7.07			4-03-019 2
N 275	48.6	122.72	289.42	68P	2.7	0.74	12.83	0.74	12.83	1735.	301	301	1	7.27	14.4	9.58	10.75	4.3	14.6	VV 81
	-720	-69.93	-0.98		1.00	43.	0.17	43.	0.17	1822.	25	25	1.03	1.26	27.3	-18.47	9.38		0.64	-1-03-022 2
N 289	50.4	298.77	265.11	48	5.8	0.75	11.43	0.75	11.43	1638.	305	305	2	38.06	27.3	-19.61	10.04	8.8	10.4	-5-03-010 2
	-3129	-85.90	-7.60		1.00	42.	0.15	42.	0.15	1614.	10	10	1.03	2.46	33.8	10.60	10.00		0.90	
U 608	56.1	124.24	343.55	8X	3.8	0.50	14.21	0.50	14.21	2760.	215	215	1	3.46	33.8	9.46	10.60	7.7	13.9	608 08-03-001
	4745	-14.83	10.94	78	1.24	62.	0.98	62.	0.98	3000.	15	15	1.04	0.54	22.8	-18.18	9.49		1.08	
N 337	57.3	128.14	289.50	78	4.5	0.73	11.90	0.73	11.90	1651.	260	260	1	14.25	22.8	9.91	10.80	6.7	7.9	-1-03-053 2
	-751	-70.35	-3.20		1.00	4.4	0.18	4.4	0.18	1725.	15	15	1.07	1.58		-19.29	9.63		0.52	

TABLE 1—Continued

NGC/UGC	α	δ	z	SGL	T	a_H^b	r_H	$B_T^{b,i}$	V	σ	W_{20}	tel.	F_c	A_H^b	$\log L$	$\log M_T$	$\%M_H/M_T$	M_T/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	
U 625	58.0	124.58	343.28	4X	7.5	0.34	11.78	2614.	346	1	1.14	9.33	62.3	10.39	11.21	4.7	6.6	IC 65	
	4725	-15.16	10.56		1.23	74.	1.32	2852.	10			1.36		-20.50	9.88		0.31	625 08-03-005 2	
U 634	58.8	127.26	304.25	9X	3.0	0.62	14.28	2211.	148	1	1.03	3.39	20.7	9.22	10.15	13.1	8.5	DDO 7	
	721	-55.17	0.53		1.01	53.	0.29	2347.	15			0.68		-17.57	9.27		1.13	634 01-03-011 2	
00059-07	59.0	130.38	289.60	8X	9.0	0.78	0.15	1084.	100	1	1.31	23.88	30.6	10.18	10.18	21.2		NGC 337A	
	752	-70.32	-3.61		1.00	40.	0.15	1161.	5			1.51		9.51				-1-03-065 2	
01012-06	102.6	132.40	291.17	7X	6.5	0.78	11.83	1092.	191	1	1.16	17.23	22.3	9.60	10.60	5.9	10.1	A 0103	
	629	-68.83	-4.10		1.00	40.	0.15	1172.	8			1.53		-18.51	9.37		0.59	-1-03-085 2	
U 711	106.1	131.83	299.00	5	5.6	0.20	12.86	1979.	226	1	1.08	3.96	34.2	9.69	10.55	4.9	7.2	711 00-04-008 2	
	123	-60.92	-2.84		1.00	90.	1.17	2088.	15			0.59		-18.74	9.24		0.35	DDO 9	
U 731	107.7	126.13	345.53	10	4.9	0.92	0.78	639.	146	5	1.17	9.60	12.7	8.87	10.83	3.5	11.1	731 08-03-000 2	
	4920	-13.15	9.39		1.33	24.	0.78	875.	10			0.85		9.78	9.38			806 00-04-062 2	
N 450	113.0	136.37	297.03	6X	5.0	0.82	12.36	1759.	205	1	1.10	6.92	27.2	-18.98	9.38		0.39		
	1108	-63.11	-5.18		1.00	36.	0.14	1853.	15			0.95							
N 470	117.2	136.65	301.46	4A	4.8	0.61	12.32	2374.	373	1	1.08	3.33	35.0	10.05	11.17	1.4	13.3	858 00-04-084 2	
	309	-58.70	-5.03		1.00	54.	0.29	2481.	20			0.76		-19.65	9.31		0.18		
U 871	117.8	136.00	303.85	10	3.1	1.00	0.09	2274.	103	1	1.05	3.33	20.9	9.24	9.76	4.6	21.5	871 01-04-022	
	535	-56.29	-4.50		1.00	86.	0.09	2294.	15			0.45		-15.61	8.43		1.00	DDO 10	
U 891	118.6	134.26	310.21	9X	4.7	0.52	13.87	646.	142	1	1.07	4.37	10.9	11.02	9.68		0.37	891 02-04-030 2	
	1209	-49.80	-2.83		1.01	61.	0.41	785.	7			0.53							
N 493	119.6	138.93	299.24	5	6.0	0.43	12.42	2340.	292	1	1.10	9.50	42.9	10.00	10.94	6.5	8.7	914 00-04-099 2	
	41	-60.57	-6.28		1.00	67.	0.52	2436.	10			1.33		-19.51	9.75		0.56	UGCA 17	
0123-06	123.7	145.95	292.69	5	4.4	0.21	12.93	1841.	89	1	1.03	6.92	36.1	9.58	9.40			UGCA 18	
	620	-67.38	-9.13		1.00	86.	0.07	1895.	10			1.20		-18.46	11.33			-1-04-044 2	
N 578	128.0	188.30	276.43	5X	7.2	0.63	11.26	1429.	308	2	1.04	1.68	34.2	10.11	11.02	4.6	8.1	ARP 306, VV 173, VV 174	
	2256	-80.11	-13.94		1.00	52.	0.16	1449.	15			1.06		-19.79	9.68		0.37	1102 01-05-002	
U 1102	130.0	141.89	303.50	13 P	2.6	0.89	13.81	1985.	181	1	1.03	3.25	15.9	9.31	9.15		0.69		
	420	-56.76	-7.77		1.00	28.	0.10	2086.	10			0.79		-17.79	9.15				
N 600	130.6	151.35	291.92	78	6.5	1.00	12.93	1841.	89	1	1.03	6.92	36.1	9.58	9.40		0.65	-1-05-007 2	
	734	-67.85	-11.10		1.00	86.	0.07	1895.	10			1.20		-18.46	11.33		0.12	-5-04-044 2	
N 613	132.0	225.02	269.73	48	8.0	0.74	10.63	1487.	383	2	1.06	1.65	34.0	10.26	9.32				
	2940	-80.29	-16.02		1.00	43.	0.16	1449.	10			1.06		-20.18	9.32				
U 1133	132.6	143.14	303.48	10	5.6	0.54	13.81	1986.	119	1	1.10	3.18	34.0	10.12	10.12	10.3		DDO 12	
	607	-56.77	-8.45		1.00	59.	0.36	2067.	10			0.58		-17.79	9.15			1133 01-05-005 2	
N 625	132.9	273.62	257.32	98	9.0	0.49	11.88	404.	98	2	1.10	7.62	8.3	8.44	9.31	3.7	7.4		
	1343	-17.44	-17.72		1.00	63.	0.40	317.	74	4	1.06	90.07	28.3	-15.63	7.88		0.28	M 74	
N 628	134.0	138.62	314.56	5A	12.1	1.00	9.62	659.	5			4.11		-19.89	9.76		0.41	1149 03-05-011 2	
	1532	-45.70	-5.40		1.01	72.	0.13	798.	54	1	1.17	8.23	15.5	9.42	9.42	18.4		DDO 13	
U 1176	137.5	139.74	314.94	10	6.9	0.82	13.81	1985.	181	1	1.03	3.25	15.9	9.31	9.15		0.69	1176 03-05-000 2	
	1539	-45.37	-6.16		1.01	36.	0.20	770.	5			0.59		-17.79	9.15			DDO 13	
U 1195	139.7	141.25	313.25	10 P	5.0	0.38	12.47	767.	145	6	1.10	4.85	13.2	9.11	8.59	6.2	4.9	1176 03-05-000 2	
	1343	-17.44	-17.72		1.01	71.	0.49	895.	20			0.76		-17.29	9.79		0.30	1195 02-05-011	
U 1197	139.8	139.59	317.40	10	3.1	0.36	14.19	2800.	206	1	1.03	2.96	26.9	9.45	10.41	10.1	0.91	1197 03-05-000	
	1803	-42.51	-5.93		1.01	72.	0.77	2942.	20			0.54		-18.15	9.41				
N 660	140.3	141.60	312.98	18P	9.9	0.45	10.97	856.	327	1	1.03	4.183	28.3	9.79	10.86	5.5	12.0	DDO 13	
	1323	-47.36	-7.51		1.01	66.	0.53	982.	8			2.52		-18.99	9.61		0.65	1201 02-05-013 2	
0140+19	140.6	139.23	319.07	10	4.6	0.32	12.47	767.	145	6	1.10	4.85	13.2	9.11	8.59	6.2	4.9	UGCA 20	
	1944	-41.24	-5.57		1.01	75.	0.92	648.	15			1.05		7.95	7.95		4.5	03-05-000	
0142-43	142.9	273.07	255.18	10	5.1	0.56	14.19	2800.	206	1	1.11	2.96	26.9	9.45	10.41	10.1	0.91	A 0143	
	4350	-70.31	-19.71		1.00	58.	0.31	293.	7			1.19		-18.15	9.41		18.4	-7-04-032 2	
U 1249	144.7	137.96	326.34	98	10.5	0.33	11.17	339.	327	1	1.03	4.183	28.3	9.79	10.86	5.5	12.0	IC 1727, VV 338	
	2705	-33.90	-4.03		1.02	74.	0.94	506.	8			2.52		-18.99	9.61			1249 04-05-009 2	
N 672	145.0	138.01	326.46	68	11.6	0.36	10.52	425.	103	1	1.27	2.52	8.6	9.30	7.95			VV 338	
	2711	-33.78	-4.05		1.03	72.	0.84	592.	15			1.05		7.95	7.95			1256 04-05-011 2	
0146-12	146.0	167.50	287.78	9	4.8	0.84	1623.	1644.	110	1	1.34	4.97	23.1	10.26	9.13		7.4	ARP 4, DDO 14	
	1238	-70.10	-15.98		1.00	34.	0.12	1644.	15			1.10		-18.34	9.13			-2-05-050 2	

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	a_H	b	r_H	B_T^i	V	W_{20}	tel.	F_C	A_H	log L	log M_T	$\%M_H/M_T$	M_T/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)		
N 676	146.3	147.88	305.97	0	6.9	0.42	10.88	1508.	1	1.13	3.60	32.4	10.25	8.97	0.05	1270 01-05-034 2			
U 1276	146.5	140.73	320.20	88	3.1	0.50	13.24	2750.	235	1	3.62	26.6	10.58	10.58	8.1	5.8	IC 163		
0146-10	146.7	-40.17	-6.64	6X	3.9	0.86	0.49	2895.	10	1.03	0.93	23.1	-19.07	9.48	0.46	1276 03-05-018			
U 1281	146.7	136.89	331.43	8	6.8	0.28	11.42	163.	139	1	9.89	6.8	8.69	9.44	4.3	5.5	UGCA 21		
0147-13	147.2	-28.71	-2.63	10	2.9	0.88	1.21	343.	79.	1	0.85	14.7	-16.26	8.07	0.24	1281 05-05-014			
N 691	147.9	-70.24	-16.36	5A	1.00	0.29	0.10	1739.	20	1.04	0.95	45.0	10.24	8.46	1.2	12.9	-2-05-057 2		
N 701	148.6	164.67	290.65	58	4.4	0.54	12.56	1839.	280	1	4.27	24.1	9.71	10.71	2.9	10.0	1305 04-05-019 2		
N 755	153.9	166.33	291.61	38	5.4	0.39	0.60	1641.	256	1	8.13	26.4	10.60	9.17	5.7	0.29	-2-05-060 2		
0154-12	154.7	171.28	288.88	88	4.4	0.27	0.76	1860.	173	1	3.30	24.2	10.18	9.36	7.6	0.29	-2-06-005 2		
N 746	154.8	135.12	343.52	108	4.0	0.75	12.43	712.	127	1	4.74	10.8	9.14	9.88	5.2	5.6	UGCA 22		
N 772	156.6	-41.01	-9.45	3A	10.6	0.65	10.77	2473.	490	2	22.06	81.0	-17.38	8.60	2.3	12.6	-2-06-006		
N 779	157.2	163.49	294.98	3X	6.5	0.34	11.10	1397.	382	1	5.72	27.3	10.07	10.94	1.3	7.5	1438 07-05-003		
N 784	158.4	140.91	328.82	8	10.0	0.27	11.04	201.	119	1	16.79	10.6	8.89	9.49	7.1	4.0	ARP 78, TURN 151B		
U 1547	200.6	144.19	322.83	108	3.5	0.92	13.99	2649.	165	6	6.07	28.2	-16.75	8.34	0.28	1501 05-05-045 2			
U 1551	200.8	-37.84	-9.26	88	1.02	0.24	0.21	2788.	133	1	0.69	37.0	-18.24	9.71	1.68	1547 04-05-043 2			
N 803	201.0	147.16	316.95	5	4.7	0.50	12.54	2096.	271	1	7.21	30.0	9.87	10.76	6.2	7.8	1551 04-05-045		
U 1561	201.3	143.45	324.73	10 P	2.6	0.70	14.12	595.	80	1	1.00	5.5	-19.19	9.55	4.1	0.48	1554 03-06-028 2		
0202-06	202.0	-35.75	-8.63	88	4.7	0.52	0.33	740.	10	1.02	0.30	19.3	-15.23	7.74	0.29	7.0	V ZW 173		
U 1670	208.2	155.37	308.53	9	3.8	1.00	0.37	1397.	10	1.11	0.69	18.8	10.26	9.06	6.3	0.29	1561 04-05-048		
U 1807	218.0	-51.05	-16.19	10	4.4	1.00	0.11	1690.	10	1.07	0.44	10.5	10.72	8.22	4.7	10.1	UGCA 24		
N 895	219.2	-17.12	-4.36	6A	1.16	0.75	0.55	815.	263	1	10.72	39.3	-19.71	9.76	0.49	1807 07-05-040			
N 891	219.3	140.37	342.98	3A	17.4	0.25	9.33	529.	490	2	49.38	36.1	10.16	11.25	1.4	12.3	NGC 894		
N 899	219.6	200.79	280.52	10	3.0	0.76	1.58	712.	10	1.17	3.09	13.4	-19.93	10.10	28.2	0.17	1831 07-05-046 2		
U 1839	220.0	-68.42	-25.42	8	4.4	0.21	0.16	1524.	155	6	1.14	20.2	8.98	9.55	4.8	10.3	UGCA 26		
N 907	220.7	-55.63	-21.21	10 P	1.01	0.36	1.18	1567.	20	1.08	0.69	15.2	-16.97	10.17	4.5	0.49	-4-06-030 2		
N 908	220.8	-68.14	-25.66	5A	8.7	0.51	0.69	1683.	20	1.01	2.37	37.3	10.34	8.83	1.7	6.8	1839 00-07-08A		
U 1865	221.9	-68.31	-25.75	9	5.4	0.82	0.38	1466.	10	1.06	1.72	11.6	-20.36	9.41	3.7	0.12	UGCA 28		
N 922	222.8	211.82	276.23	68P	3.0	0.90	0.44	3086.	268	6	5.52	26.6	10.17	9.70	2.7	0.34	UGCA 29		
N 918	223.1	152.18	321.29	5X	5.3	0.62	12.41	1516.	257	6	5.42	25.1	-19.96	10.72	0.32	11.7	DDO 19		
	1816	-38.96	-15.48		1.02	0.53	0.37	1625.	10	1.15	0.79		-18.64	9.16		0.32	1865 06-06-028 2		
																	UGCA 30		
																	SCI 31		
																	1888 03-07-011 2		

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	b_H	r_H	$B_T^{b,i}$	V	W_{20}	tel.	F_C	A_H^b	$\log L$	$\log M_T$	$\log M_H$	$\%M_H/M_T$	M_T/L	M_H/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)
0223-21	223.7	-21.39	203.24	279.98	9	3.4	0.79	0.15	1555.	160	2	3.34	15.0	10.30	3.8	8.88	3.8	UGCA 31, DDO 21		
			-26.44			1.00	39.		1510.	15	1.01	0.74						-4-06-040 2		
0224-24	224.2	-24.31	210.71	276.80	88	4.2	0.58	0.30	1515.	247	2	5.26	17.9	10.50	3.5	10.50	3.5	UGCA 32		
			-26.88			1.00	56.		1459.	25	1.01	0.94						-4-06-041 2		
N 925	224.3	144.89	335.50	7X	14.8	0.61	10.07	0.53	554.	224	4	71.10	30.7	9.87	6.5	10.67	7.6			
			-9.49			1.06	54.		710.	8	1.17	3.26		-19.19	9.55	0.48		1913 05-06-045 2		
N 941	226.0	168.88	301.96	6X	4.5	0.62	12.71	0.29	1627.	157	1	2.59	21.9	9.55	4.2	10.23	4.2			
			-22.80			1.01	53.		1660.	10	1.07	0.72		-18.39	8.85	0.20		1954 00-07-022 2		
N 949	227.8	144.06	339.04	7A	5.7	0.67	11.99	0.15	610.	191	1	4.37	12.8	9.17	1.6	11.0	1.6			
			-8.55			1.09	49.		774.	10	1.11	0.79		-17.45	8.42	0.18		1983 06-06-048 2		
0228-04	228.2	-28.2	172.73	299.35	9	5.0	1.00	0.09	1627.	100	1	4.45	24.2	9.08	1.9	9.08	1.9	UGCA 33		
			-24.05			1.00			1648.	5	1.12	0.54		9.03	8.22	0.15		-1-07-020		
N 959	229.3	145.08	337.70	9	4.2	0.61	12.33	0.58	609.	175	1	2.81	9.3	9.03	8.22	0.15		2002 06-06-051 2		
			-9.56			1.07	54.		767.	10	1.06	0.48		-17.09	8.22	0.15				
U 2014	229.8	143.79	340.61	10	4.1	0.58	12.55	0.17	570.	70	1	2.35	8.9	9.10	10.0	10.0		DDO 22		
			-8.19			1.11	56.		737.	10	1.05	0.36		8.11	9.94	5.6		2014 06-06-054 2		
U 2017	229.9	148.32	331.68	10	3.9	0.82	10.9.	0.68	1019.	104	1	3.63	13.3	8.69				2017 05-07-000		
			-12.64			1.04	36.		1137.	10	1.06	0.54		8.69				DDO 25		
U 2023	230.3	146.19	335.99	10	4.7	0.94	12.70	0.36	611.	56	6	4.24	10.4	8.88	0.33	0.33		2023 05-07-007 2		
			-10.65			1.06	20.		763.	5	1.16	0.42		-16.71	8.39					
U 2034	230.6	143.15	342.34	10	5.7	0.87	12.55	0.55	581.	66	1	8.56	12.5	8.92	11.2	5.1		DDO 24		
			-7.47			1.14	30.		752.	5	1.14	0.60		-16.83	8.69	0.58		2034 07-06-032 2		
U 2053	231.5	148.23	332.68	10	3.7	0.60	14.08	0.50	1034.	64	1	3.81	12.5	8.70	34.0	3.1		DDO 26		
			-12.55			1.04	55.		1173.	5	1.04	0.40		-16.27	8.72	1.05		2053 05-07-015 2		
N 986	231.6	248.65	260.18	28	6.0	0.75	11.62	0.17	1983.	119	2	39.52	20.7	10.09	4.2	1.7				
			-65.63			1.00	42.		1868.	30	1.03	0.57		-19.74	8.93	0.07		-7-06-015 2		
N 988	232.9	181.94	293.69	58	6.0	0.47	12.55	0.17	1509.	290	6	8.40	26.4	10.74	3.4	3.4		UGCA 35		
			-26.54			1.00	64.		1504.	15	1.17	0.90		9.28				-2-07-037 2		
N 991	233.1	178.75	296.11	5X	4.8	0.61	12.17	0.45	1504.	85	1	4.77	21.7	9.70	0.23	0.23		-1-07-023 2		
			-26.07			1.00	25.		1541.	8	1.10	0.60		-18.77	9.05			IC 239		
U 2080	233.3	144.33	341.19	6X	7.3	0.97	11.66	0.47	909.	140	1	26.67	22.8	9.67	0.66	0.66		2080 06-06-065 2		
			-8.66			1.12	14.		1074.	8	1.25	1.39		-18.69	9.49					
U 2082	233.4	150.89	328.87	5	8.6	0.25	11.34	0.47	710.	217	1	11.98	20.8	9.50	4.1	6.5		2082 04-07-016		
			-14.82			1.03	81.		834.	10	1.18	0.89		-18.26	10.30	0.26				
N 1015	235.6	172.18	302.53	18	5.1	1.00	12.29	0.30	2631.	188	1	4.36	39.7	10.12	0.23	0.23		2124 00-07-066		
			-25.15			1.01	0.10		2655.	20	1.13	1.36		-19.83	9.49					
N 1003	236.1	144.00	343.15	6A	8.9	0.45	11.17	0.45	626.	230	1	39.52	20.7	9.52	9.4	8.0		2137 07-06-051 2		
			-17.54			1.15	66.		794.	8	1.22	2.07		-18.33	9.40	0.75				
N 1012	236.3	149.08	333.53	13 P	4.9	0.56	12.37	0.30	986.	222	1	12.20	16.1	9.24	10.35	10.2				
			-13.30			1.05	58.		1123.	10	1.08	1.15		-17.88	9.19	0.70		2141 05-07-027		
N 1035	237.1	181.37	295.32	5A	3.6	0.34	12.10	0.30	1236.	280	1	3.56	13.1	9.53	10.35	2.4				
			-27.26			1.00	74.		1232.	20	1.03	1.15		-18.35	8.73	0.16		-1-07-027 2		
U 2162	237.8	170.08	305.40	10	3.1	1.00	11.94.	0.11	1194.	65	1	1.63	11.2	8.39				DDO 27		
			-24.92			1.01	30.		1226.	25	1.05	0.33		-18.35	8.39			2162 00-07-077 2		
N 1042	237.9	182.07	295.02	6X	6.8	0.88	11.17	0.13	1377.	119	1	12.67	27.3	10.00				UGCA 38		
			-27.53			1.00	29.		1371.	10	1.20	1.00		-19.52	9.38	0.24		-2-07-054 2		
0238-06	238.1	178.86	297.58	10	2.9	0.90	10.90	0.13	1333.	110	1	2.86	11.4	8.71						
			-27.02			1.00	26.		1336.	10	1.04	0.49		-18.35	8.71			-1-07-031		
N 1051	238.6	180.15	296.71	98	3.3	0.87	13.00	0.14	1300.	205	1	5.30	12.6	10.62	2.1	2.1		IC 249, UGCA 40		
			-27.35			1.00	30.		1300.	10	1.05	1.01		-18.35	8.95			-1-07-033		
N 1055	239.2	171.35	304.68	3	12.0	0.40	10.79	0.13	1002.	410	1	32.05	36.0	9.90	11.14	2.4				
			-25.50			1.01	69.		1030.	10	1.37	2.49		-19.27	9.53	0.43		2173 00-07-081 2		
N 1068	240.1	172.11	304.27	3A	10.1	0.80	9.33	0.13	1151.	307	2	8.15	34.6	10.60	11.24	4.4		M 77, ARP 37		
			-25.84			1.01	38.		1176.	20	1.10	1.40		-21.02	9.05	0.03		2188 00-07-083 2		
N 1058	240.2	146.37	340.41	5A	6.6	1.00	11.71	0.44	560.	42	3	19.55	13.0	9.17	8.95	0.60				
			-10.63			1.10			676.	5	1.21	1.01		-17.44	8.95			2193 06-07-001 2		
N 1073	241.1	170.92	305.84	58	6.3	0.87	11.59	0.16	1212.	92	1	17.17	23.0	9.82	10.19	17.0				
			-25.66			1.01	30.		1242.	8	1.17	1.18		-19.08	9.42	0.40		2210 00-08-001 2		

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	d_H^b	r_H	B_p^i	V	W_{20}	tel.	F_C	A_H^b	$\log L$	$\log M_H$	$\log M_T$	% M_H/M_T	M_T/L	Alternate Names
(1)	(2)	(3)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	
N 1090	244.0	-173.50	304.37	58	8.0	0.38	11.93	2765.	338	1	7.48	64.7	10.31	11.22	9.76	3.5	8.3	2247 00-08-011 2	
N 1097	244.3	-226.91	270.25	38	14.1	0.61	9.98	2786.	402	4	35.36	48.8	-20.30	11.39	9.69	2.0	11.0	UGCA 41, ARP 77	
	-3029	-64.65	-31.65		1.00	54.	0.27	1181.	10	1.16	2.44		-20.38				0.23	-5-07-024 2	
U 2259	244.8	-147.15	341.05	88	4.7	0.80	12.89	589.	137	1	5.81	10.1	8.78	10.01	8.51	3.2	17.1	2259 06-07-009 2	
U 2275	245.4	-169.64	308.87	9	8.1	1.00	13.51	1025.	109	4	15.48	25.0	-16.46	9.24			0.53	DDO 28	
U 2302	246.6	-171.73	307.13	9	8.1	1.00	13.12	1061.	71	4	14.22	26.7	-16.82	9.24			2.09	2275 01-08-000 2	
	156	-49.24	-26.72		1.01		0.12	1133.	5	1.08	0.83		-17.15	9.05			1.63	DDO 29	
N 1110	246.8	-183.77	296.26	10	4.4	0.27	13.36.	1336.	193	1	7.62	17.1	10.12	10.12	9.13	10.1		UGCA 43, NGC 10 UNCERTAIN	
0246-02	246.8	-177.06	302.00	10	2.3	1.00	10.94.	118	1	1.05	0.87		9.13	9.13				-1-08-010	
U 2345	249.3	-176.03	303.84	98	6.2	0.80	0.10	1103.	20	1.03	0.69		7.4	8.72				UGCA 44	
N 1140	252.2	-188.35	294.14	10 P	2.7	0.62	12.57	1508.	218	1	8.46	11.8	10.24	10.24	9.51	10.7	5.5	DDO 30	
0252-18	252.3	-202.78	284.13	5	4.9	0.22	1.17	1911.	15	1.02	0.97	27.4	-18.29	9.27			0.58	2345 00-08-035 2	
U 2411	253.4	-130.66	14.18	9	7.8	0.15	1.72	2547.	238	1	0.61	63.1	10.85	10.85	9.15	9.7		UGCA 45	
	7533	14.83	8.04		1.22	90.		2767.	15	1.14	1.44		9.83	9.83				-3-08-042	
0255-02	255.4	-179.08	303.03	98	4.7	0.66	11.34	1539.	217	1	11.16	21.3	10.53	10.53	9.42	7.8		2411 13-03-000	
U 2459	257.1	-143.66	352.17	8	8.6	0.26	1.17	2464.	341	1	9.10	61.6	11.17	11.17	9.42	4.3		IC 1870, UGCA 46	
U 2463	257.4	-148.07	344.72	9X	5.2	0.70	13.13	1899.	220	1	4.16	31.4	10.77	10.77	9.80	3.0	15.7	-1-08-020	
	4003	-16.23	-12.02		1.19	47.	0.72	2051.	25	1.10	0.82		-18.43	9.24			0.48	2459 08-06-000	
N 1169	300.1	-145.41	350.22	3X	11.4	0.61	11.34	2397.	482	1	12.35	85.1	10.47	11.78	9.91	1.3	20.5	2463 07-07-013	
N 1179	300.3	-204.68	284.07	6X	6.2	0.82	11.62	1781.	15	1.41	1.75	31.2	-20.70	9.91			0.28	2503 08-06-025 2	
N 1187	300.4	-212.10	279.25	58	6.7	0.83	10.75	1394.	284	2	14.17	25.8	10.15	10.15	9.53	4.2	7.7	UGCA 48	
	-2304	-60.05	-35.02		1.00	35.	0.15	1314.	10	1.04	1.51		-19.84	9.39			0.33	-3-08-060 2	
N 1171	300.7	-147.02	347.75	5	6.2	0.49	11.89	2747.	267	1	4.57	53.1	10.36	11.04	11.04	3.5	4.8	UGCA 49	
U 2531	302.9	-147.90	347.12	8A	8.8	0.54	11.66	2717.	358	1	11.81	73.4	-20.43	11.41	9.59		0.17	-4-08-016 2	
0304-14	304.7	-197.30	290.14	10 P	2.0	1.00	0.98	2872.	25	1.23	1.39	8.6	-20.63	9.99			0.35	2510 07-07-018	
	-1413	-55.80	-35.06		1.01		0.09	1480.	15	1.02	0.47			8.56				2531 07-07-023 2	
0306-23	306.3	-213.14	279.12	12	3.3	0.48	0.44	2888.	187	6	3.23	27.1	10.38	10.38	9.40	10.5		UGCA 52	
N 1232	307.5	-208.77	282.22	5X	9.5	0.94	10.39	1684.	250	2	29.98	44.8	10.45	11.41	9.99			IC 1892, UGCA 55, ARP 332	
0307-41	307.8	-248.01	256.93	7	6.5	0.45	0.49	804.	149	2	5.95	15.4	-20.64	9.92			0.27	ARP 41	
	-4112	-58.46	-35.45		1.00	66.			10	1.03	0.80			8.59			4.6	-4-08-032 2	
0308-22	308.1	-212.12	279.97	5	5.5	0.23	1.17	1244.	260	2	4.21	20.1	10.44	10.44	8.81	2.4		-7-07-007	
0308-33	308.5	-232.84	266.55	10	1.00	83.	0.09	1009.	15	1.02	0.73			8.46				IC 1898, UGCA 56	
N 1255	311.4	-218.61	275.81	4X	5.6	0.73	11.40	1699.	260	2	8.98	26.3	10.04	10.87	9.36	3.1	6.7	-4-08-036	
	-2555	-58.25	-37.61		1.00	44.	0.20	1600.	15	1.03	1.25		-19.62	9.36			0.21	UGCA 60	
N 1253	311.6	-183.68	303.89	68	7.6	0.50	11.95	1709.	328	1	31.02	37.4	9.87	11.01	11.01	8.6	14.0	-6-08-000	
0311-25	311.6	-217.61	276.51	10	1.01	62.	0.45	1696.	15	1.17	3.21	29.8	-19.20	9.95			1.20	UGCA 62, ARP 279	
0312-04	312.2	-186.15	301.65	10	1.00	79.	1.07	1638.	182	2	8.70	29.8	10.31	10.31	9.37	11.4		-1-09-018 2	
	-458	-49.22	-34.87		1.01	33.	0.17	2197.	12	1.05	0.57			9.30			20.0	UGCA 61	
														-17.78			0.91	-4-08-051 2	
																		DDO 32	
																		-1-09-021 2	

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	α_H	δ_H	r_H	B_T^i	V	W_{20}	tel.	F_C	A_H	$\log L$	$\log M_T$	$\log M_H$	M_T/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	
U 2620	313.0	129.17	18.53	9X	3.9	0.80	13.65	2244.	151	1	4.82	27.8	9.52	10.53	8.6	10.4	2620 13-03-004		
0314-24	800.4	19.23	9.77	10	1.10	38.	0.51	2464.	10	1.06	1.23	12.8	-18.31	9.47	0.88	UGCA 63			
0314-35	314.0	216.03	277.77	10	2.2	0.93	0.11	1982.	74	2	1.07	12.8		8.62		-4-08-000			
0314-35	314.9	237.26	263.41	7	2.9	0.82	0.15	1572.	15	1.01	0.62	12.3		10.27	7.1	-6-08-002			
	-354.2	-58.02	-37.71		1.00	36.		1438.	20	1.01	0.83			9.12					
N 1292	316.0	222.43	275.40	5A	4.1	0.47	12.13	1370.	263	2	6.69	15.2	9.54	10.41	4.1	7.5			
0316-26	316.4	215.55	285.61	4	1.00	64.	0.46	1261.	20	1.01	1.18		-18.37	9.03	0.31	-5-08-026 2	UGCA 64		
0316-23	316.6	217.17	287.74	10	3.8	0.42	0.55	1802.	208	6	2.52	18.9		10.28	3.8	-4-08-057 2	UGCA 65		
0316-23	316.6	215.54	278.31	10	2.6	1.00	0.09	1699.	15	1.07	0.63			8.86		-4-08-000			
	-2358	-56.68	-38.77		1.00			1536.	100	2	3.22	11.0		8.82					
N 1300	317.5	208.16	283.94	4B	8.0	0.60	10.79	1583.	292	2	10.54	35.3	10.23	10.96	2.6	5.3	UGCA 66		
U 2684	317.6	166.33	326.22	10	1.01	55.	0.31	1502.	15	1.05	1.39		-20.09	9.38	0.14	-3-09-018 2			
N 1309	319.8	202.21	288.12	4A	4.4	1.00	0.50	357.	88	1	2.53	3.9		8.91	5.4				
	-1535	-53.15	-38.87		1.01			417.	8	1.03	0.44	26.8		7.64					
0320-11	320.5	196.27	294.46	7B	3.8	0.85	0.16	2138.	161	1	7.23		10.06	9.49	0.27	-3-09-028 2	UGCA 67		
0321-19	321.5	209.32	283.56	12 P	3.1	0.91	0.13	2070.	10	1.09	0.98			11.09	2.7	-2-09-036	UGCA 68		
0321+72	321.7	133.91	12.99	10	4.3	0.31	1.52	2755.	15	1.06	0.75	16.0		9.52		-3-09-033	UGCA 69		
	7240	13.38	4.78		1.30	76.		1753.	15	1.01	0.63	28.5		10.64	6.0	12-04-000			
N 1326	322.0	238.76	261.96	-2B	6.0	1.00	11.20	2074.	269	1	5.02		9.42						
U 2729	322.2	136.39	9.74	9	3.9	0.23	0.20	2284.	15	1.05	0.77			9.97		-6-08-011 2			
N 1325	322.3	212.26	281.32	4A	1.72	0.41	1.19	1363.	280	2	7.01	23.6	9.97	9.02	0.11				
0323-36	323.1	238.52	262.05	9B	2.0	0.74	0.58	1221.	20	1.04	1.19	F	-19.44	11.21	2.0	2729 11-05-000	UGCA 70		
0323-16	323.2	204.01	288.21	9	3.9	0.23	0.20	1936.	260	1	7.28	56.9		9.52		-4-09-004 2			
0323-36	323.4	238.54	262.02	7B	4.8	0.31	0.90	2140.	10	1.31	1.10		9.85	10.88	2.0	NGC 1326A			
	-3632	-56.25	-39.28		1.01			1595.	346	6	6.76	27.3	-19.14	9.18	0.22	-6-08-013 2	UGCA 71		
N 1337	325.7	193.56	298.33	6A	7.3	0.36	11.46	1804.	15	1.04	0.83			9.48	44.8	-3-09-041	UGCA 72		
U 2765	327.2	136.89	9.89	9	10.0	0.45	0.74	1012.	185	2	16.16	18.9		9.48		-6-08-014 2	UGCA 73		
0327-15	327.2	203.17	289.67	9	3.4	0.92	1.03	870.	10	1.01	1.28		9.09	10.14	8.8				
	-1524	-51.46	-40.61		1.01	24.	0.13	1816.	10	1.05	1.12			9.18					
0330-17	330.0	207.28	286.49	10	3.3	0.48	0.46	1861.	160	1	22.74	25.4	9.77	10.61	8.0	7.1	-2-09-042 2	UGCA 74	
N 1359	331.5	210.21	284.12	9B	3.5	0.85	0.16	1760.	15	1.12	0.67		-18.93	9.51	0.56				
0331-21	331.6	213.23	281.52	4B	4.2	0.84	0.16	1676.	239	2	9.31	19.3		11.16	2.4	13.3	-3-10-003	UGCA 75	
	-2137	-52.72	-42.16		1.01	34.	0.16	1883.	15	1.01	1.15		9.77	10.89	4.2	0.56	-3-10-007 2	IC 1953, UGCA 76	
N 1365	331.8	237.94	261.91	3B	13.4	0.59	9.82	1210.	220	6	3.43	21.7	-19.13	9.84	1.5	10.1	-4-09-026 2	UGCA 77	
N 1371	332.8	218.92	276.83	1X	7.5	0.77	11.28	1760.	15	1.12	0.67			9.403	3.3	7.6	-6-08-026 2	UGCA 78	
U 2800	334.9	135.62	12.59	10	5.9	0.54	1.03	1639.	403	4	37.60	52.3	10.52	11.40	3.8	0.25	-4-09-029 2	UGCA 79	
	7114	12.81	3.07		1.34	59.		1492.	20	1.14	2.49	F	-20.82	9.92	1.4	27.1			
N 1385	335.2	218.45	277.38	6B	4.7	0.64	0.28	1472.	412	6	17.99	30.0	9.95	11.38	0.37		-6-08-026 2	UGCA 80	
0335+66	335.5	138.52	9.21		4.6	0.62	1.15	1360.	10	1.35	1.28		-19.39	9.52	8.9	0.17	-4-09-036 2	UGCA 81	
	6634	9.11	-0.16		1.92	53.		1180.	235	1	7.14	23.8		10.56	3.8	9.71	11-05-000		

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	q_H	r_H	$B_{T,i}^b$	V	W_{20}	tel.	F_C	A_H^b	$\log L$	$\log M_T$	$\%M_H/M_T$	M_T/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	
N 1398	336.8 -2630	221.54 -52.77	274.85 -43.29	28	10.1 1.01	0.80 38.	10.32 0.18	1401. 1281.	458 10	1.10	11.77 1.92	37.6 15.3	10.28 -20.22	11.63 9.29	0.5	22.3 0.10	-4-09-040 2	
N 1406	337.5 -3150	229.82 -53.31	268.01 -42.96	58	5.6 1.01	0.25 81.	11.40 1.15	1068. 931.	352 15	1.02	8.54 2.69	15.3 22.0	9.57 -18.44	10.59 10.21	1.9	10.6 0.20	UGCA 83	
U 2813	337.5 7109	135.85 12.87	12.67 2.86	10	4.7 1.33	0.49 63.	1407. 1611.	172 20	1.06	2.60	22.0	10.21 8.83	10.21 9.64	4.1	4.1	2813 12-04-000 NGC 1427A		
0338-35	338.3 -3547	236.99 -53.28	262.23 -42.37	108	3.6 1.01	0.65 51.	2029. 1879.	96 25	1.01	0.63	14.2 F	9.34	9.34	49.9	49.9	-6-09-016 2		
U 2824	338.8 7629	132.50 17.12	16.62 6.46	13 P	9.0 1.15	1.00 42.	11.73 0.52	2511. 2722.	255 40	1.42	71.9 0.94	10.37 -20.44	10.37 -20.44	0.04 2.7	0.04	IC 334 2824 13-03-007		
N 1421	340.2 -1339	202.82 -47.87	292.60 -43.48	4X	5.4 1.01	0.28 79.	10.61 1.06	2099. 2021.	383 15	1.39	0.94	32.2	10.56 -20.92	10.99	10.99	-2-10-008 2		
N 1425	340.3 -3003	227.52 -52.56	269.88 -43.74	3A	6.8 1.01	0.53 60.	11.31 0.39	1510. 1376.	368 15	1.08	8.67 0.72	27.5 10.7	9.94 -19.38	11.00 9.22	1.6	11.4 0.19	UGCA 84 -5-09-023 2	
0341-36	341.2 -3626	238.05 -52.68	261.20 -42.80	9	2.7 1.01	0.75 42.	895. 741.	107 40	1.23	1.03	0.72	10.7 F	9.73 7.89	9.73	1.5	9.73	NGC 1457 -6-09-024	
N 1448	342.9 -4448	251.52 -51.39	250.34 -40.67	6A	11.0 1.01	0.24 82.	10.27 1.18	1178. 1000.	416 15	1.01	31.62 5.85	32.0 2.6	10.08 -19.73	11.05 9.50	2.8	9.4 0.26	UGCA 85 -7-08-005 2	
U 2855	343.3 6959	136.97 12.25	12.17 1.70	5X	8.8 1.38	0.53 60.	11.82 1.09	1210. 1410.	440 10	1.07	24.50 2.26	36.3 2.2	9.76 -18.93	11.28 9.69	2.6	32.9 0.85	2855 12-04-004 2	
0344-35	344.4 -3505	235.83 -52.04	262.81 -43.74	9	5.1 1.01	0.41 69.	1930. 1777.	298 20	1.02	1.03	6.73 1.32	20.1 F	10.62 9.43	10.62 9.33	5.1	5.1	UGCA 86 -6-09-030	
0347-27	347.4 -2708	223.28 -50.57	273.72 -45.61	5	4.9 1.01	0.22 85.	1535. 1404.	225 20	1.02	1.01	3.24 0.98	20.2 2.2	10.35 78.94	10.35 8.80	2.8	2.8	UGCA 87 -5-10-004	
0355+66	355.0 6659	139.77 10.64	10.87 -1.21		2.8 1.57	0.89 28.	0.96 0.96	72. 262.	145 10	1.03	78.94 4.56	2.2	8.73	8.73	8.73	11-05-000		
N 1493	355.9 -4621	253.19 -48.85	247.26 -42.17	68	4.2 1.01	0.88 29.	11.61 0.16	1059. 870.	119 10	1.02	9.14 1.17	10.8 12.5	9.43 -18.09	8.84 10.08	0.26 6.8	0.26 0.37	2	
N 1507	401.9 -219	193.05 -37.56	309.94 -45.89	98	5.3 1.02	0.37 72.	11.92 0.77	864. 810.	205 10	1.02	9.74 0.92	12.5 12.8	9.24 -17.62	10.08 8.81	5.3	5.3	2947 00-11-009 2	
N 1512	402.3 -4329	248.66 -48.16	250.19 -44.39	18	6.0 1.01	1.00 17.	11.34 0.12	911. 725.	271 10	1.08	36.91 2.32	12.8 2.32	9.38 -17.96	8.81 9.29	0.81	0.81	-7-09-007 2	
U 2953	402.5 6941	138.46 13.11	13.18 0.35	2AP	9.1 1.31	0.91 25.	10.67 0.76	898. 1092.	489 10	1.04	23.39 1.61	28.9 18.4	10.00 -19.52	9.45 9.93	9.3	9.3	IC 356, ARP 213 2953 12-04-011 2	
0403-17	403.7 -1755	211.72 -44.38	287.30 -49.55	10	3.5 1.01	0.53 74.	1890. 1777.	146 15	1.03	1.36 0.61	18.4 17.1	8.4 8.82	8.4 8.82	0.28	0.28	UGCA 87 -3-11-011		
0404-17	404.9 -1721	211.13 -43.90	288.20 -49.80	9A	3.3 1.01	0.96 17.	1866. 1754.	98 10	1.05	2.13 0.56	17.1	8.82	8.82	9.3	9.3	UGCA 88 -3-11-012		
N 1532	410.2 -3300	233.17 -46.57	263.87 -49.42	28	11.2 1.01	0.28 79.	10.07 1.07	1212. 1047.	538 10	1.05	54.12 7.00	34.2 12.5	10.23 -20.09	11.32 9.77	2.8	12.5 0.35	-5-11-002 2	
N 1530	417.0 7512	135.20 17.78	17.50 3.95	38	8.0 1.13	0.58 56.	11.53 0.72	2460. 2661.	326 10	1.08	9.06 12.77	62.4 17.2	10.39 -20.50	11.28 10.18	3.3	7.9 0.26	VII ZW 12 3013 13-04-004 2	
0419-21	419.0 -2157	218.59 -42.32	280.85 -53.16	7A	7.7 1.01	0.44 66.	0.44 0.57	906. 768.	191 10	1.20	12.77 1.18	17.2	10.18 8.88	5.0	5.0	UGCA 90 -4-11-010		
N 1560	427.1 7148	138.35 16.04	16.08 0.78	7A	14.0 1.18	0.18 90.	10.59 1.65	-28. 164.	153 10	1.04	45.05 5.00	6.7 1.6	8.39 -15.48	9.50 8.08	3.8	12.9 0.49	IC 2062 3060 12-05-005 2	
0427+63	427.4 6330	144.71 10.51	11.35 -6.04		5.6 1.59	0.54 59.	0.97 0.66	-104. 66.	1 1.10	1.42	5.00	1.6 38.2	9.89 -19.25	8.08	3.8	14.7 0.57	UGCA 92 11-06-000	
U 3130	437.8 7533	135.82 19.00	18.78 3.49	3X	4.5 1.11	0.61 54.	12.89 0.65	2485. 2683.	313 10	1.10	6.14 0.86	38.2	9.89 -19.25	11.06 9.65	3.8	14.7 0.57	IC 381 3130 13-04-007 2	
N 1637	438.9 -256	199.53 -30.02	314.40 -54.70	5X	8.0 1.04	0.82 36.	11.27 0.32	726. 639.	205 8	1.08	17.52 1.22	14.9 21.1	9.29 -17.76	10.57 8.85	1.9	18.7 0.37	UGCA 93 00-12-068 2	
U 3137	439.4 7620	135.22 19.56	19.28 4.10	3	6.0 1.10	0.28 79.	12.79 1.36	994. 1193.	246 10	1.26	1.22 1.01	21.1 16.4	9.23 -17.59	10.43 9.17	5.5	15.8 0.88	3137 13-04-008	
N 1640	440.1 -2032	218.88 -37.21	282.86 -58.15	38	3.9 1.02	0.69 48.	12.12 0.33	1602. 1452.	157 15	1.09	2.27 0.73	16.4	9.67 -18.69	10.18 8.68	3.2	3.3 0.10	-3-12-018 2	

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	q_H	r_H	$B_T^{b,i}$	V	W_{20}	tel.	F_C	A_H^b	$\log L$	$\log M_T$	$\log M_H$	$\%M_H/M_T$	M_T/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)
0440-08	440.5	205.11	305.87	9	3.1	0.71	0.36	2522.	209	1	3.68	21.7	10.57	5.7	UGCA 94				
	-810	-32.18	-56.85		1.03	46.	13.87	2414.	20	1.03	0.67	19.5	9.33	14.6	9.6	DDO 33			-1-12-047
U 3144	441.3	136.56	18.59	108	3.7	0.57	0.69	1830.	158	1	6.08	19.5	9.17	10.15	14.6	9.6	DDO 33		
	745.0	18.74	2.76		1.11	57.	0.69	1830.	10	1.04	0.84	5.6	-17.44	9.31	2.7	1.38	DDO 34		3144 12-05-018 2
U 3174	446.0	197.55	320.56	10	3.2	0.82	0.37	588.	131	1	0.71	5.6	8.18	9.75	2.7	1.38	DDO 34		DDO 34 00-13-014 2
	9	-26.92	-54.97		1.05	36.	0.37	588.	20	1.04	0.71	5.6	8.18	9.75	2.7	1.38	DDO 34		3174 00-13-014 2
0447-29	447.2	230.07	265.98	9	4.8	0.86	0.25	1471.	155	2	4.23	18.0	10.51	2.2	UGCA 95, DDO 228				
	-2917	-38.13	-58.08		1.02	31.	0.25	1471.	10	1.02	0.78	9.9	8.85	8.85	2.2	UGCA 95, DDO 228			-5-12-003 2
N 1679	448.1	233.59	260.98	108	3.9	0.89	0.21	1059.	158	2	9.94	9.9	8.88	8.88	2.2	UGCA 96			UGCA 96
	-3204	-38.54	-57.28		1.02	28.	0.21	1059.	10	1.02	0.98	9.9	8.88	8.88	2.2	UGCA 96			-5-12-004
0450-28	450.0	229.49	266.73	10	2.6	0.54	0.46	1460.	145	6	3.05	9.9	9.76	8.7	UGCA 97				
	-2840	-37.39	-58.85		1.02	59.	0.46	1460.	40	1.04	1.12	1.12	8.70	8.70	2.2	UGCA 97			-5-12-005
0450-25	450.9	225.52	272.97	9X	5.4	0.95	0.21	1374.	98	2	8.89	19.0	9.11	5.5	UGCA 98, DDO 229				
	-2519	-36.32	-59.94		1.02	19.	0.21	1374.	7	1.03	0.69	13.4	9.16	10.32	5.5	UGCA 98, DDO 229			-4-12-019 2
N 1744	457.9	226.59	270.63	78	8.2	0.64	0.38	742.	217	2	36.09	13.4	9.16	10.32	5.5	UGCA 98, DDO 229			
	-2606	-35.03	-61.28		1.02	52.	0.38	742.	7	1.05	1.99	13.4	9.16	10.32	5.5	UGCA 98, DDO 229			-4-12-029 2
U 3234	500.5	185.16	344.52	10	3.8	1.00	0.64	1370.	145	1	6.21	15.3	9.07	9.07	5.5	DDO 35			3234 03-13-000 2
	1620	-15.01	-47.72		1.23	55.	0.64	1370.	10	1.07	0.59	15.3	9.07	9.07	5.5	DDO 35			
N 1784	503.1	211.90	301.13	58	6.0	0.64	0.45	2321.	345	1	16.62	38.5	10.07	11.18	5.3	12.8			
	-1157	-28.85	-63.15		1.04	52.	0.45	2321.	10	1.12	1.45	29.0	10.07	11.18	5.3	12.8			-2-13-042 2
N 1792	503.6	241.70	248.46	4A	9.9	0.59	0.41	1216.	316	2	9.90	29.0	10.02	10.94	1.1	8.3			
	-3803	-36.44	-57.13		1.02	56.	0.41	1216.	25	1.08	1.36	29.0	10.02	10.94	1.1	8.3			-6-12-004 2
0505-16	505.2	216.76	291.40	98	4.0	0.60	0.47	2044.	54	1	4.11	22.3	9.29	74.3	7.1	41.3			
	-1621	-30.15	-64.16		1.03	55.	0.47	2044.	7	1.05	0.52	22.3	9.29	74.3	7.1	41.3			-3-14-001 2
0506-38	506.5	242.19	247.37	10	2.0	0.74	0.31	807.	134	2	16.11	4.8	9.57	28.3	2.3	0.71			
	-3822	-35.92	-57.40		1.02	43.	0.31	807.	7	1.00	1.08	4.8	9.57	28.3	2.3	0.71			-6-12-006
0506-09	506.8	209.65	307.30	10	2.6	0.51	0.61	2693.	215	1	2.75	19.6	10.38	7.5	UGCA 101				
	-919	-26.89	-63.41		1.05	61.	0.61	2693.	25	1.02	0.65	19.6	10.38	7.5	UGCA 101				-2-14-001
N 1827	508.4	240.65	248.97	6	5.5	0.24	1.27	836.	200	2	5.29	13.5	10.45	3.3	UGCA 103, DDO 230				
	-3702	-35.33	-58.50		1.02	82.	1.27	836.	13	1.02	0.93	13.5	10.45	3.3	UGCA 103, DDO 230				-6-12-008
0508-31	508.8	234.27	257.98	9	3.9	0.93	0.23	980.	145	2	7.55	8.8	8.81	8.81	2.3	0.71			
	-3140	-34.66	-61.42		1.02	22.	0.23	980.	10	1.02	0.86	8.8	8.81	8.81	2.3	0.71			-5-13-011 2
0509-14	509.4	215.66	294.97	6A	4.5	0.81	0.35	1976.	233	1	5.01	23.8	10.87	10.87	2.3	0.71			
	-1453	-28.65	-65.08		1.04	37.	0.35	1976.	10	1.08	0.79	23.8	10.87	10.87	2.3	0.71			UGCA 104, A 0509
0509+62	509.6	148.53	15.03	10	9.5	0.67	0.35	1823.	139	1	51.00	7.3	8.08	9.70	7.1	41.3			
	6231	13.66	-9.29		1.28	49.	0.35	1823.	7	1.31	2.64	7.3	8.08	9.70	7.1	41.3			-2-14-004 2
0510-33	510.1	235.96	255.23	10	5.1	0.74	0.88	935.	98	2	18.84	10.9	8.77	9.65	22.4	7.7	UGCA 106, DDO 231		
	-3302	-34.20	-60.99		1.02	43.	0.88	935.	7	1.02	1.18	10.9	8.77	9.65	22.4	7.7	UGCA 106, DDO 231		
N 1843	511.7	211.61	305.00	7	3.2	0.95	0.32	2611.	215	1	6.88	22.7	10.60	9.00	1.70	UGCA 107			-5-13-000 2
	-1041	-26.40	-64.93		1.05	19.	0.32	2611.	15	1.05	0.87	22.7	10.60	9.00	1.70	UGCA 107			UGCA 107
0513-30	513.3	233.32	259.03	68	4.0	0.40	0.73	1481.	245	2	5.37	15.0	9.62	10.32	4.2	UGCA 108			-2-14-008
	-3036	-32.96	-62.77		1.03	69.	0.73	1481.	15	1.01	0.79	15.0	9.62	10.32	4.2	UGCA 108			-5-13-013
U 3273	513.7	156.43	11.61	9	9.4	0.37	12.22	616.	203	1	14.05	20.1	9.04	10.27	4.1	17.2			
	5330	9.01	-17.69		1.96	72.	12.22	616.	8	1.23	0.90	20.1	9.04	10.27	4.1	17.2			3273 09-09-001
0515-37	515.0	241.09	247.22	5	6.7	0.27	0.26	1348.	294	2	16.85	21.9	10.60	5.4	3273 09-09-001				
	-3710	-34.06	-59.47		1.02	79.	0.26	1348.	10	1.03	1.64	21.9	10.60	5.4	3273 09-09-001				
0516-21	516.9	223.56	278.34	10	3.0	0.80	0.34	1661.	143	2	2.85	14.6	10.21	4.9	UGCA 109, DDO 37				-6-12-012
	-2136	-29.49	-66.55		1.04	38.	0.34	1661.	15	1.01	0.70	14.6	10.21	4.9	UGCA 109, DDO 37				-4-13-000 2
N 1879	517.9	235.45	254.93	10X	3.1	0.90	0.26	1038.	145	2	3.45	9.4	9.07	8.57	0.32	UGCA 110, DDO 232			
	-3212	-32.41	-62.82		1.03	26.	0.26	1038.	15	1.01	0.70	9.4	9.07	8.57	0.32	UGCA 110, DDO 232			
0519-37	519.5	241.12	246.23	9	4.5	0.36	0.84	1299.	148	2	2.63	14.3	10.19	8.49	4.4	ARP 123			
	-3701	-33.15	-60.26		1.03	72.	0.84	1299.	15	1.01	0.70	14.3	10.19	8.49	4.4	ARP 123			-6-12-019
N 1888	520.2	213.47	304.12	58P	4.3	0.29	11.68	2310.	111	1	1.09	27.5	10.19	9.86	7.1	0.4	ARP 123		
	-1133	-24.88	-67.16		1.06	78.	11.68	2310.	20	1.05	0.50	27.5	10.19	9.86	7.1	0.4	ARP 123		-2-14-013 2
U 3303	522.3	198.56	336.86	9	6.6	0.77	0.65	528.	179	1	10.39	8.3	8.11	1.5	3303 01-14-000				
	428	-16.92	-59.93		1.17	41.	0.65	528.	8	1.16	1.08	8.3	8.11	1.5	3303 01-14-000				
U 3317	527.2	139.35	20.88	10	3.8	1.00	0.39	1424.	136	1	4.10	15.8	8.30	8.92	DDO 38				
	7341	20.76	0.37		1.08		0.39	1424.	15	1.07	0.69	15.8	8.30	8.92	DDO 38				3317 12-06-006 2

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	d_H^b	r_H	$B_T^{b,i}$	V	W_{20}	tel.	F_C	A_B^b	flag	$\log L$	$\log M_T$	$\log M_H$	$\%M_H/M_T$	M_T/L	M_H/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)	(22)
N 1954	530.5	217.14	298.47	58	6.6	0.51	0.67	3143.	464	1	8.55	57.6			11.51	2.3					-2-15-003 2
	-1405	-23.65	-70.07		1.07	61.		2977.	25	1.13	1.23				9.88						
N 1964	531.2	225.28	275.37	3X	8.6	0.37	10.59	1671.	427	2	16.21	37.2			11.18	2.3					
	-2159	-26.51	-69.70		1.05	72.	0.90	1480.	15	1.05	3.37				10.38						IC 2135
N 1963	531.6	241.07	243.84	5	5.6	0.33	0.97	1324.	250	2	6.98	17.9			10.38	3.5					-4-14-003 2
	-3627	-30.66	-62.44		1.03	74.	0.97	1098.	20	1.02	1.17				8.92						-6-13-004
0539-35	539.3	240.70	242.52	9	5.6	0.71	0.40	1273.	140	2	3.03	17.1			10.12	2.5					-6-13-007
	-3544	-28.58	-64.05		1.04	46.	0.40	1044.	15	1.03	1.08				8.52						
0539-22	539.8	227.08	270.79	10	4.1	0.30	1.18	1731.	172	2	5.37	18.4			10.07	10.8					UGCA 112
	-2258	-25.00	-71.30		1.06	77.	1.18	1532.	15	1.01	0.87				9.10						-4-14-011
0541-19	541.8	223.54	281.84	58	3.5	0.35	1.02	2749.	280	2	5.83	26.5			10.66	8.3					UGCA 113
	-1919	-23.23	-72.69		1.07	73.	1.02	2559.	40	1.01	1.14				9.58						-3-15-011
N 2090	545.2	239.43	242.88	5A	5.3	0.62	11.26	936.	297	2	27.28	11.0			9.39	10.49	4.4				-6-13-009 2
	-3415	-27.43	-65.96		1.05	53.	0.49	707.	10	1.02	2.06				9.13						
0548-14	548.7	219.77	297.72	88P	4.9	0.88	0.48	908.	133	1	6.84	10.3									UGCA 114
	-1447	-19.92	-74.53		1.11	29.	0.49	728.	10	1.10	1.50				8.56						-2-15-011
U 3371	549.9	138.44	22.82	10	7.2	0.82	0.40	820.	149	1	7.90	21.1			10.44	2.9					DDO 39
	7518	22.81	1.44		1.06	36.	0.40	1003.	8	1.21	0.73				8.90						3371 13-05-07A 2
0550-17	550.8	222.99	285.95	6A	4.8	0.85	0.48	3125.	325	1	7.44	41.4			11.48	2.1					IC 438, UGCA 115
	-1752	-20.70	-75.00		1.10	33.	0.48	2934.	8	1.10	0.84				9.81						-3-13-025
0553+03	553.1	203.42	347.73	13 P	3.2	0.90	14.24	805.	149	1	3.85	6.3									UGCA 116, 11 ZW 40
	324	-10.76	-65.93		1.58	26.	0.96	688.	15	1.04	0.55				8.26	5.2					01-16-000 2
0558-28	558.6	234.85	247.50	9B	3.3	0.54	0.64	1392.	189	6	4.23	11.4			10.04						UGCA 117, DDO 233
	-2859	-23.10	-71.71		1.07	59.	0.64	1166.	15	1.06	0.86				8.76	2.7					-5-15-002 2
U 3390	558.8	175.55	13.17	8X	7.0	0.60	1.85	1511.	220	1	5.21	31.4			10.66						3390 06-14-001
	3607	6.63	-36.72		2.00	55.	1.85	1534.	15	1.16	0.84				9.09						
N 2139	559.0	229.52	262.17	6X	3.6	0.88	11.59	1845.	235	2	12.91	17.2									IC 2154
	-2340	-21.14	-75.01		1.09	25.	0.46	1632.	15	1.01	1.28				9.54	0.36					-4-15-005 2
0601-20	601.4	226.76	272.42	7B	3.7	0.96	0.48	1776.	175	2	6.34	19.1									UGCA 118
	-2039	-19.48	-76.81		1.12	17.	0.48	1814.	15	1.02	0.87				9.30						-3-16-010
0602-26	602.8	232.30	262.69	7X	3.7	0.59	0.64	1593.	260	2	5.96	17.3			10.54	4.4					UGCA 119
	-2607	-21.23	-74.32		1.09	56.	0.64	1593.	15	1.01	1.10				9.18						-4-15-008
N 2188	608.4	240.85	233.13	9B	5.5	0.41	11.44	757.	145	2	10.11	8.3			9.61	6.6					
	-3406	-22.80	-68.99		1.08	69.	0.86	515.	8	1.02	0.95				8.43	0.24					-6-14-008 2
0609-21	609.2	228.42	265.06	10	3.3	0.80	0.58	854.	115	2	9.54	6.2			9.65	8.8					UGCA 120
	-2135	-18.17	-78.08		1.14	38.	0.58	641.	10	1.01	0.83				8.59						-4-15-000 2
N 2196	610.1	228.70	263.72	2A	5.0	0.83	11.53	2333.	407	2	5.20	31.1			11.51	0.7					UGCA 121
	-2147	-18.06	-78.17		1.14	35.	0.57	2119.	30	1.02	2.92				9.37	0.14					-4-15-014 2
N 2146	610.7	135.66	24.65	28P	8.8	0.57	10.78	918.	494	1	18.46	28.4			11.30	1.1					
	7822	24.90	4.17		1.04	57.	0.53	1108.	15	1.24	1.54				9.36	21.4					3429 13-05-022 2
0613-26	613.3	233.66	245.13	10	2.5	0.86	0.52	1799.	104	2	1.66	11.3			9.96	4.5					UGCA 122, DDO 234, KAR 48
	-2634	-19.21	-75.71		1.12	31.	0.52	1571.	30	1.01	0.46				8.61						-4-15-000 2
0615-27	615.2	234.61	241.76	3	4.4	0.23	1.56	1696.	314	2	2.39	18.8			10.58	1.3					UGCA 126
	-2722	-19.11	-75.37		1.12	83.	1.56	1465.	15	1.01	0.60				8.71						-5-15-008
U 3439	615.8	135.54	24.93	5	5.2	0.43	12.63	1495.	246	1	8.66	25.6			10.57	6.7					NGC 2146A
	7833	25.19	4.31		1.04	67.	0.72	1685.	10	1.08	1.21				9.39	9.4					3439 13-05-025 2
0618-08	618.5	217.07	336.43	5	8.3	0.32	1.73	739.	315	1	50.45	13.6			10.47	5.4					UGCA 127
	-826	-10.60	-78.97		1.60	75.	1.73	561.	8	1.18	3.58				9.20						-1-17-000
0618-20	618.9	227.88	266.78	12 P	4.3	0.88	0.66	1981.	359	2	13.10	22.0			9.61						UGCA 128
	-2002	-15.48	-80.81		1.21	29.	0.66	1767.	20	1.02	1.61				9.61						-3-17-002 2
N 2223	622.5	230.86	250.40	4X	5.3	0.88	11.51	2716.	392	2	7.16	38.5			10.38						UGCA 129
	-2248	-15.83	-79.87		1.20	29.	0.64	2492.	60	1.03	1.34				9.65	0.19					-4-16-002 2
U 3463	622.6	155.87	22.77	4X	4.3	0.72	12.39	2896.	324	1	5.05	34.9			11.17	2.7					IC 2166
	5907	20.03	-15.01		1.09	42.	0.53	2811.	10	1.07	1.20				9.60	0.30					3463 10-10-001
U 3475	627.0	175.05	20.74	9	5.6	0.58	13.18	487.	190	1	6.55	8.3			9.94	1.9					
	3931	13.13	-34.54		1.32	56.	0.97	512.	20	1.10	0.87				8.22	0.76					3475 07-14-002
U 3496	632.0	127.61	26.38	10	3.6	0.76	0.34	1583.	75	1	1.35	18.9			9.69	8.8					
	8553	27.02	11.51		1.03	42.	0.34	1795.	15	1.05	0.41				8.64						3496 14-04-000

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	σ_H	r_H	$B_T^{b,i}$	V	W_{20}	tel.	F_c	A_H^b	$\log L$	$\log M_T$	$\log M_H$	$\%M_H/M_T$	M_T/L	M_H/L	Alternate Names
(1)	(2)	(3)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(16)	(17)	(18)	(18)
0635475	635.0	138.92	25.67	13 P	1.1	0.85	0.28	794.	80	1	0.59	3.2	9.17	3.8	9.17	3.8	UGCA 130, MARK 5			
7539	25.62	1.31	1.31	6X	4.6	0.87	11.90	2106.	233	1	4.68	29.8	7.75	1.8	7.75	1.8	13-05-000 2			
U 3504	635.6	155.42	24.56		1.07	30.	0.40	2222.	10	1.09	0.65		9.36		9.36		3504 10-10-009			
U 3522	641.0	128.64	26.50	13 P	3.6	0.56	14.32	2137.	208	1	2.76	24.8	9.20	5.0	10.48	5.0	VII 7W 92			
8459	27.11	10.60	10.60		1.03	58.	0.25	2346.	120	1	0.67		17.53		9.18	0.96	3522 14-04-009			
U 3530	642.0	155.37	25.40	7X	4.0	0.64	12.78	2109.	220	1	4.88	26.2	9.77	5.9	10.62	5.9	NGC 22738			
6024	22.75	-13.95	13.95		1.06	52.	0.51	2224.	150	1	0.62		18.96		9.38	0.41	3530 10-10-013 2			
N 2280	642.9	237.31	217.15	6A	11.5	0.47	10.68	1896.	400	2	33.77	55.5	10.36	4.1	11.35	4.1	UGCA 131			
-2735	-13.53	-77.81	-77.81		1.31	64.	1.10	1651.	10	1.09	3.72		-20.41		9.96	0.40	-5-16-020 2			
N 2273	645.6	154.97	25.87	1B	5.7	0.70	11.47	1844.	367	1	2.64	32.6	10.19	0.6	11.22	0.6	MARK 620			
6054	23.31	-13.47	13.47		1.06	47.	0.46	1961.	15	1.12	0.69		19.99		9.01	0.07	3546 10-10-015 2			
U 3574	648.9	158.92	26.22	6A	6.6	1.00	12.25	1445.	172	1	11.08	29.7	9.67		9.42	0.57	3574 10-10-017			
5715	22.76	-17.13	17.13		1.06	56.	0.34	1545.	10	1.21	0.78		18.69		9.85	5.3	3580 12-07-022 2			
U 3580	650.0	145.69	26.52	1A	6.5	0.50	11.52	1204.	236	1	11.61	25.9	10.58	5.7	10.58	5.7				
6939	25.65	-4.73	-4.73		1.04	62.	0.59	1356.	10	1.13	1.30		19.14		9.33	0.30				
U 3587	650.9	195.87	26.01	12	8.6	0.42	11.81	1254.	239	1	11.44	29.5	9.61	4.9	10.60	4.9	9.8			
1922	9.18	-55.01	-55.01		1.95	68.	1.62	1173.	110	1.20	1.50		18.54		9.20	0.39	3587 03-18-003			
U 3598	652.0	155.38	26.67	10B	3.6	0.59	13.92	1996.	115	1	2.30	21.9	9.27	11.7	9.94	4.6	3598 10-10-019			
6043	24.02	-13.67	-13.67		1.05	56.	0.53	2110.	20	1.04	0.38		17.70		9.01	0.55	DDO 40			
U 3647	700.7	160.03	27.91	10B	2.4	0.87	14.25	1382.	76	3	3.09	10.4	8.83	14.0	9.68	7.1	3647 09-12-027 2			
5637	24.16	-17.75	-17.75		1.05	30.	0.35	1475.	8	1.02	0.32		16.59		8.83	1.00				
U 3658	701.8	198.55	30.69	10	4.9	0.45	11.83.	1183.	142	1	1.93	15.8	9.88	3.0	9.88	3.0	3658 03-18-000			
1741	10.78	-56.62	-56.62		1.59	66.	1.37	1089.	15	1.07	0.63		8.36		8.36		3685 10-11-002 2			
U 3685	704.5	154.68	28.19	3B	5.8	1.00	11.94	1797.	101	1	13.37	32.5	9.98		9.69	0.51	3685 10-11-002 2			
U 3691	705.1	201.13	32.56	6A	6.1	0.51	11.87	2208.	265	1	4.74	37.5	19.47	3.0	10.84	5.6	3691 03-19-001			
1515	10.44	-58.98	-58.98		1.65	61.	1.51	2102.	25	1.11	0.64		19.74		9.32	0.17				
N 2337	706.6	172.95	29.61	10B	4.3	0.83	12.24	433.	178	1	9.50	5.9	8.63	1.8	10.06	1.8				
4432	21.80	-29.77	-29.77		1.07	35.	0.43	467.	15	1.07	0.92		16.10		8.32	0.49	3711 07-15-010			
N 2276	710.5	127.67	27.09	5X	4.1	1.00	11.67	2409.	154	1	5.93	31.5	10.36		9.61	0.18	ARP 25, VII 2W 134			
8551	27.71	11.48	11.48		1.03	0.21	0.25	2619.	20	1.08	0.84		20.42		9.61	0.18	3740 14-04-028 2			
N 2357	714.6	194.43	34.67	5	6.3	0.21	12.23	2273.	358	1	5.55	40.8	9.99	2.5	11.03	2.5				
2327	15.90	-50.57	-50.57		1.20	86.	1.68	2201.	15	1.10	1.29		19.48		9.43	0.28	3782 04-17-014			
N 2336	718.0	133.57	27.83	4X	10.7	0.59	10.55	2196.	455	1	17.39	74.4	10.73	2.2	11.66	2.2				
8016	28.20	5.94	5.94		1.03	56.	0.44	2386.	15	1.36	2.07		21.34		10.00	0.18	3809 13-06-006 2			
U 3808	718.0	193.02	35.43	7B	3.6	0.54	13.65	2362.	208	1	3.09	24.2	9.46	5.7	9.92	5.7				
U 3817	719.2	172.94	32.08	10	3.3	0.54	0.80	2317.	10	1.04	0.79		18.17		9.22	0.57	3808 04-18-006			
4512	24.13	-28.89	-28.89		1.05	59.	0.58	471.	5	1.03	0.27		7.77		7.77		3817 08-14-000			
U 3826	720.0	154.87	30.05	7X	5.8	0.89	12.82	1734.	70	3	6.67	31.1	9.60		9.36					
6148	27.53	-12.40	-12.40		1.03	28.	0.27	1847.	5	1.14	0.46		18.51		9.36	0.57	3826 10-11-038			
U 3834	721.6	134.30	28.02	5X	5.1	0.45	11.81	2036.	316	1	5.25	33.4	10.16	3.2	10.91	3.2	IC 467			
7958	28.37	5.66	5.66		1.03	66.	0.63	2225.	15	1.08	1.19		19.93		9.41	0.18	3834 13-06-007 2			
N 2377	722.6	225.31	37.66	3X	5.8	0.90	0.63	2455.	206	1	11.77	38.0	9.77	17.8	9.77		UGCA 132, 3C 178			
-930	24.98	-80.49	-80.49		2.00	26.	3.92	2242.	10	1.15	1.26		17.40		8.66	0.32	-2-19-000 2			
N 2366	723.6	146.44	29.49	10B	10.3	0.53	10.70	102.	116	4	64.74	7.4	8.70	14.8	9.43	5.3	000 42			
6918	28.54	-4.91	-4.91		1.03	60.	0.50	248.	5	1.08	3.26		16.27		9.60	5.3	3851 12-07-040 2			
U 3860	724.8	177.81	33.99	10	3.1	0.70	14.65	355.	55	3	2.82	3.3	7.46	10.1	8.60	0.79	000 43			
4052	23.93	-33.03	-33.03		1.05	47.	0.45	365.	7	1.03	0.31		13.16		7.58	13.1	3860 07-16-003 2			
U 3912	731.6	213.75	52.91	10B	4.9	0.61	12.75	1236.	190	1	3.63	15.4	9.15	2.6	10.24	12.1	3912 01-20-001			
439	11.59	-67.57	-67.57		1.50	54.	1.10	1073.	15	1.08	0.84		17.40		8.66	0.32				
N 2403	732.1	150.57	30.84	6X	29.7	0.52	8.34	132.	247	2	344.44	22.6	9.59	6.5	10.56	7.5				
6543	29.19	-8.53	-8.53		1.02	61.	0.51	261.	20	1.61	11.28		18.74		9.37	0.48	3918 11-10-007 2			
U 3946	735.4	215.51	56.65	10	3.4	0.68	13.19	1198.	109	1	3.46	10.1	8.94	8.4	9.64	5.0				
325	11.87	-68.24	-68.24		1.47	48.	1.02	1028.	12	1.04	0.54		16.87		8.56	0.42	3946 01-20-003			
U 3964	737.8	220.00	65.98	8X	5.4	0.77	13.31	1461.	178	1	2.82	20.1	9.08	1.5	10.48	25.5				
-128	10.13	-72.01	-72.01		1.75	41.	1.15	1271.	15	1.11	0.77		17.21		8.66	0.38	3964 00-20-004			

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	a_H^b	r_H	B_{I}^{I}	V	W_{20}	tel.	F_c	A_H^b	$\log L$	$\log M_T$	$\%M_H/M_T$	M_T/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	
U 3966	738.0	179.23	37.07	10	3.5	0.92	0.30	364.	91	1	4.60	3.8	DDO 46					
U 3974	4014	26.17	-33.17	10	1.04	24.	0.30	368.	10	1.06	0.53	3.4	DDO 47					
U 3975	739.0	203.10	46.57	10	7.7	0.82	12.73	265.	88	1	16.54	3.4	3974 03-20-010 2					
U 4115	1655	18.53	-55.52	88	1.13	36.	0.56	153.	5	1.24	0.94	27.6	3975 12-08-009					
U 4121	739.0	142.29	30.14	88	3.6	0.80	13.64	2480.	88	1	2.21	0.38	DDO 48					
U 4148	7255	29.76	-1.14	10A	1.02	38.	0.28	2639.	10	1.05	0.38	2.1	4115 02-21-000					
U 4238	754.2	207.01	54.26	10A	3.4	0.59	13.63	361.	122	1	5.89	2.9	4121 10-12-046 2					
U 4260	1431	20.89	-56.26	58	1.09	56.	0.64	214.	10	1.04	0.68	8.5	4148 07-17-006					
U 4305	754.8	159.40	35.16	7	3.9	0.58	0.74	1090.	165	1	3.95	6.7	4165 09-13-110 2					
U 4393	5811	31.57	-15.10	7	1.02	71.	13.81	1180.	10	1.04	0.76	27.2	4173 13-06-017					
U 4426	756.5	177.83	40.44	7	3.5	0.20	11.11	737.	148	1	2.95	8.5	UGCA 135					
U 4459	4219	30.10	-30.21	78	1.02	90.	1.29	747.	10	1.04	0.67	6.6	-2-21-004 2					
U 4499	758.2	167.98	37.81	78	4.0	0.95	12.00	519.	122	1	7.93	0.32	4238 13-06-018 2					
U 4514	5054	31.58	-21.96	10	1.02	19.	0.19	572.	10	1.07	0.62	8.91	DDO 49					
U 4173	758.6	133.73	29.53	10	4.9	0.28	13.45	866.	89	1	7.37	15.1	4274 08-15-050 2					
U 4578	8016	29.90	6.27	58	1.02	79.	1.13	1054.	7	1.06	0.76	8.91	4284 08-15-054 2					
U 4582	803.3	231.86	104.77	58	6.9	0.76	11.11	1586.	232	1	4.29	27.2	4260 08-15-047 2					
U 4598	-1117	10.80	-72.31	78	1.64	42.	1.09	1354.	15	1.18	1.00	0.59	ARP 6, MARK 86, VV 138					
U 4609	805.0	137.83	30.89	78	4.3	0.61	12.54	1541.	187	1	6.92	21.4	4274 08-15-050 2					
U 4278	810.4	174.12	41.68	7	6.8	0.19	12.25	565.	206	1	12.53	11.8	IC 2233					
U 2541	4954	33.05	-26.03	6A	1.01	90.	1.25	591.	8	1.11	1.08	8.64	4278 08-15-052 2					
U 4305	811.0	170.18	40.50	10	2.9	0.95	13.55	2254.	154	1	2.77	19.6	0.63					
U 4305	4913	33.47	-22.89	9A	1.01	63.	0.49	596.	8	1.22	1.89	9.9	0.47					
U 4305	814.1	144.28	33.31	10	11.1	0.81	10.94	158.	76	1	91.60	3.9	0.47					
U 2557	809.7	173.80	41.46	108P	2.7	0.89	12.15	452.	116	1	5.08	8.69	0.24					
U 4278	4609	32.96	-25.84	7	1.01	28.	0.23	305.	5	1.49	3.58	1.2	0.24					
U 2559	815.0	246.99	151.70	58P	8.4	0.54	0.54	1571.	419	6	10.44	31.8	1.2					
U 2541	-2719	4.47	-67.62	7	2.00	59.	2.85	1296.	30	1.34	1.07	9.24	UGCA 136					
U 2541	815.7	249.28	157.40	7	6.8	0.79	0.79	1650.	272	2	14.41	27.2	UGCA 137					
U 2552	-2989	3.10	-66.16	9A	2.00	39.	3.83	1370.	99	1.04	1.27	9.43	-4-20-003					
U 2552	815.7	169.10	40.90	9A	5.6	0.70	12.52	527.	157	1	6.91	9.3	-5-20-000					
U 2566	5010	34.30	-21.73	28	1.01	47.	0.28	574.	8	1.11	0.61	2.6	4325 08-15-062 2					
U 2566	816.6	245.54	146.52	28	9.0	0.64	0.64	1649.	223	2	6.03	36.2	UGCA 138					
U 4390	-2520	5.88	-68.13	78	2.00	52.	2.11	1377.	30	1.07	0.94	23.4	-4-20-008 2					
U 4390	822.2	140.86	32.90	78	3.4	0.92	14.04	2167.	205	1	3.41	2.6	4390 12-08-042					
U 4393	734.1	32.71	0.46	128	1.01	24.	0.18	2326.	30	1.05	0.77	9.31	0.90					
U 4393	822.6	174.09	43.75	128	3.8	0.71	12.72	2129.	127	1	4.82	24.1	2.6					
U 4426	4608	35.18	-25.00	10	1.01	46.	0.26	2154.	10	1.05	0.51	0.38	4393 08-16-003					
U 4426	825.2	179.14	46.15	10	3.1	0.54	0.54	392.	96	1	2.64	3.6	DDO 52					
U 4459	4202	35.23	-28.53	10	1.01	59.	0.41	396.	10	1.03	0.49	1.2	4426 07-18-004 2					
U 4591	829.5	149.32	36.29	10	2.9	0.85	14.20	19.	3	1.04	1.2	6.83	VII ZW 238, DDO 53					
U 2591	6620	34.95	-6.09	5	1.01	33.	0.18	144.	277	1	3.71	21.0	4459 11-11-013 2					
U 2591	830.6	135.57	31.64	5	4.8	0.29	11.77	1331.	10	1.06	0.75	10.54	4472 13-07-001 2					
U 2613	7812	31.89	4.83	3A	1.02	78.	1.06	1509.	637	2	22.15	68.0	0.12					
U 2613	831.1	245.35	137.80	3A	16.5	0.32	9.52	1679.	25	1.17	4.78	11.78	UGCA 141					
U 2613	-2248	10.04	-65.73	10	1.81	75.	1.85	1411.	25	1.17	4.78	9.64	-4-21-003 2					
U 2613	831.7	244.50	135.07	10	5.0	0.33	1.73	1777.	224	2	3.35	21.9	UGCA 142					
U 2613	-2141	10.80	-65.82	8	1.66	74.	1.73	1511.	15	1.02	0.96	8.88	UGCA 143					
U 2613	833.6	253.15	156.80	8	7.8	0.33	2.99	1552.	248	2	4.78	28.8	UGCA 143					
U 2613	-3159	5.06	-61.84	8X	2.00	74.	2.99	1266.	20	1.04	1.86	8.88	-5-21-000					
U 4499	833.9	167.11	42.99	8X	4.4	0.82	13.05	686.	142	1	6.96	9.7	22.1					
U 4514	5149	37.18	-19.07	58	1.01	36.	0.18	749.	10	1.08	0.74	8.59	0.74					
U 4514	835.9	164.81	42.44	58	3.5	0.53	13.21	697.	172	1	4.91	7.9	13.4					
U 4514	5338	37.40	-17.30		1.01	60.	0.39	759.	10	1.04	0.79	8.45	0.60					

TABLE 1—Continued

NGC/UGC	α	δ	l	b	SGL	T	q_H	r_H	B_T^i	V	W_{20}	tel.	F_C	A_H^b	$\log L$	$\log M_T$	$\log M_H$	M_T/L	M_H/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)
U 4543	839.9	174.56	46.82	8A	5.2	0.60	13.59	1961.	137	1	6.23	30.3	9.35	10.23	14.3	7.6	1.09	4543	08-16-000	
	4555	38.17	-23.88		1.01	55.	0.32	1983.	15		0.64		-17.90	9.39						
U 4559	841.1	194.08	56.34	4	4.4	0.27	13.16	2086.	357	1	3.99	26.3	9.54	10.84	2.3	20.1		4559	05-21-004	
N 2683	849.6	190.43	55.90	3A	12.2	0.32	9.69	415.	446	2	19.98	13.3	9.46	10.75	0.5	19.8				
	3338	38.77	-33.42		1.01	75.	0.87	373.	10	1.09	1.51		18.17	8.44				4641	06-20-011	2
U 4646	851.0	127.26	28.93	6X	5.3	0.77	11.96	1614.	149	1	3.67	28.3	9.93	10.48	4.0	3.5		IC 512		
	8542	29.52	11.86		1.02	41.	0.30	1822.	15	1.11	0.62		-19.34	9.09				4646	14-05-002	
N 2708	853.6	231.55	97.15	3A	4.7	0.54	2007.		467	1	4.27	24.4	11.16	11.16	0.9					
	-310	25.67	-57.76		1.06	59.	0.60	1795.	40	1.07	1.00		9.14	9.22				00-23-015	2	
U 4683	854.0	157.27	42.01	10	3.1	0.59	0.99.	909.	79	1	0.71		9.22							
	5916	39.12	-11.16		1.00	56.	0.31	999.	15	1.03	5.41	21.7	9.92	10.70	6.1	6.0		4683	10-13-046	
N 2701	855.3	164.04	44.91	4XP	3.1	0.68	12.57	2328.	254	1	1.00		5.41	21.7	9.92	10.70	6.1	4695	09-15-063	2
	5357	40.22	-15.67		1.00	48.	0.23	2391.	10	1.03	1.00		5.41	21.7	9.92	10.70	6.1			
U 4704	855.8	183.19	53.34	8	5.8	0.18	13.27	599.	137	1	5.31	9.9	8.42	9.57	4.9	14.3		4704	07-19-011	
	3924	40.74	-27.95		1.00	90.	1.18	586.	10	1.08	0.73		8.26	8.67				4704	07-19-011	
0859-26	859.3	252.03	141.62	9	3.4	0.92	12.29	2684.	203	1	5.36	26.0	10.11	9.56	0.28					
	-2607	13.10	-58.73		1.00		0.82	1682.	15		0.81		8.67							
N 2750	902.9	201.34	64.74	5X	3.4	0.92	12.29	2684.	203	1	5.36	26.0	10.11	9.56	0.28					
	2538	39.84	-37.99		1.01	24.	0.14	2600.	30	1.05	0.73		8.67							
U 4777	903.6	189.47	57.85	10	3.7	0.24	13.71	2056.	212	1	1.92	21.9	9.32	10.30	3.9	9.7		4777	06-20-024	
	3449	41.81	-30.77		1.00	82.	1.15	2019.	15	1.03	0.46		8.35	9.38	2.0	10.9				
U 4787	904.4	191.30	58.97	8	3.5	0.29	13.15	553.	148	1	1.87	5.2	8.35	9.38	2.0	10.9				
	3328	41.79	-31.74		1.00	78.	0.98	509.	15	1.03	0.39		8.35	9.38	2.0	10.9		4787	06-20-028	
N 2763	904.5	244.01	120.68	6	3.8	1.00	12.25	1892.	208	1	4.43	18.1	9.72	9.08	0.23					
	-1517	20.86	-58.28		1.11		0.45	1640.	15	1.07	0.76		8.67							
U 4797	905.5	224.12	85.77	9	3.9	1.00	14.08	1315.	101	1	1.76	12.9	8.67	8.36				DDO 54		
	608	32.58	-50.59		1.02		0.20	1160.	10	1.07	0.73		8.36					4797	01-24-003	2
N 2770	906.4	191.60	59.48	5A	5.2	0.34	11.59	1953.	342	1	7.95	29.1	10.24	10.87	3.9	4.3				
	3318	42.17	-31.61		1.00	74.	0.77	1908.	15	1.07	1.33	3.5	9.46					4806	06-20-038	2
0907-22	907.5	250.64	134.82	10	2.7	0.72	12.4	724.	84	2	0.95		9.00		1.9			UGCA 148, DDO 56		
	-2248	16.66	-57.46		1.21	45.	0.73	453.	10	1.01	0.70		7.29							
0907-33	907.5	258.64	152.90	10	1.21		1.13	846.	46	2	2.81	23.5	10.30		2.2			UGCA 149		
	-3309	9.83	-54.90		6.4	0.68	1.25	1251.	154	2	0.71		8.64							
0908-32	908.0	258.56	152.51	10	1.84	48.	1.25	1251.	25	1.04	2.54	17.9	9.07	10.06	7.5	9.6		DDO 55		
	-3257	10.04	-54.87		3.3	0.57	14.13	1880.	149	1	0.43		8.94					4837	06-20-042	2
U 4837	909.0	188.44	58.22	9	3.3	0.57	14.13	1880.	149	1	0.43		8.94							
	3543	43.01	-29.38		1.00	57.	0.31	1848.	10	1.03	3.35	17.3	9.04					DDO 57		
0909-14	909.0	244.35	120.04	10	3.3	1.00	0.42	2054.	134	1	3.35	17.3	9.04							
	-1450	21.99	-57.16		1.10		0.42	1803.	15	1.05	0.55		11.23		0.7					
N 2781	909.1	244.17	119.62	1X	6.6	0.57	11.74	2028.	418	1	3.92	34.0	10.00							
	-1436	22.16	-57.11		1.09	57.	0.66	1778.	40	1.14	1.00		9.23					A 0909, HOLMBERG III		
U 4841	909.4	138.64	35.44	7X	4.0	1.00	12.95	1128.	200	1	7.43	15.2	9.23					4841	12-09-032	2
	7426	35.47	2.60		1.01		0.12	1289.	10	1.08	1.02		9.09							
0909-19	909.8	248.70	129.45	7	7.5	0.17	1.61	2178.	356	2	8.89	41.7	11.02		3.1			UGCA 151		
	-1956	18.92	-57.14		1.15	90.	1.61	1514.	15	1.03	1.51		9.51							
0911-19	911.0	248.31	128.13	10	3.0	0.54	0.77	772.	130	2	2.97	4.4	9.31		3.8			UGCA 153		
	-1913	19.60	-56.88		1.14	59.	0.77	509.	25	1.01	0.64		7.89							
U 4888	913.3	139.00	35.92	5A	5.5	0.44	12.11	2258.	308	1	7.29	39.1	10.11	10.95	4.7	6.9		IC 529		
	7358	35.92	2.36		1.01	66.	0.54	2417.	10	1.09	1.32		9.63					4888	12-09-035	2
U 4922	915.2	171.34	51.03	9A	5.6	0.54	12.83	1993.	254	1	3.40	33.2	9.67	10.77	2.4	12.4				
	4805	44.08	-18.83		1.00	59.	0.33	2025.	15	1.10	0.59		9.14					4922	08-17-074	
N 2835	915.7	251.43	133.31	5B	10.0	0.67	10.44	890.	220	2	37.58	18.1	9.60	10.48	4.7	0.30		UGCA 157		
	-2209	18.52	-55.64		1.16	49.	0.69	620.	8	1.08	2.01		18.52							
N 2805	916.4	150.01	41.56	7X	8.0	0.75	11.60	1736.	121	1	19.09	43.4	10.09	10.45	23.1	0.36				
	6419	40.20	-5.48		1.00	42.	0.18	1851.	8	1.24	1.13		9.82					4936	11-12-003	2
0917-12	917.4	243.33	115.57	10	2.6	0.85	0.40	1945.	67	1	3.43	12.7	9.60		25.2			DDO 60		
	-1201	25.34	-34.74		1.06	33.		1703.	8	1.03	0.51		9.00							

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	b	SGL	T	σ_H^b	r_H	B_T^i	A_B^i	V	σ	W_{20}	tel.	F_C	A_H^b	flag	M_B^b	$\log L$	$\log M_T$	$\log M_H$	$\%M_H/M_T$	M_T/L	M_H/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)	(22)	(23)	(24)	(25)	
N 2820	917.7	149.73	41.58	58P	4.7	0.30	12.36	1576.	373	1	13.75	23.3	9.70	10.84	5.7	13.6	4961	11-12-006	2						
	6429	40.27	-5.26		1.00	77.	0.92	1691.	25	1	1.65	23.8	9.78	9.59	0.78										
N 2848	917.8	247.03	122.99	5X	4.4	0.76	12.15	2044.	208	1	7.75	22.8	9.84	10.66	5.5	6.5	UGCA 160								
	-1618	22.71	-55.17		1.09	42.	0.51	1789.	10	1	1.07	1.20	-19.11	9.39	0.36										
0918-12	918.3	243.80	116.26	10	2.1	0.82	11.66	1906.	96	1	2.93	10.3	9.75	14.5											
	-1223	25.29	-54.58		1.06	36.	0.41	1663.	10	1	0.51	8.91	8.91												
N 2841	918.6	166.93	49.56	3A	11.3	0.50	9.73	637.	616	2	4.82	22.6	9.97	23.6											
	5112	44.15	-15.95		1.00	62.	0.37	686.	10	1	1.09	7.46	9.32												
0919-22	919.2	252.10	133.43	10	4.4	0.27	8.99	141	2	7.64	7.3	8.41	9.49	8.3											
	-2217	19.04	-54.82		1.15	79.	1.50	579.	10	1	0.84	0.84	8.41												
0925-31	925.3	260.28	148.73	10	3.7	0.79	10.82	98	2	2.15	8.7	9.63	10.42	2.7											
	-3148	13.48	-51.78		1.38	39.	0.88	794.	15	1	0.52	18.4	9.80												
N 2903	929.4	208.70	73.58	4X	13.9	0.65	9.25	554.	395	2	4.08	18.4	9.80	0.9											
	2144	44.56	-36.44		1.00	51.	0.25	451.	15	1	1.16	2.31	8.95												
0930-16	930.5	249.48	123.80	2X	4.2	0.88	2123.	260	1	6.07	22.8	9.33	10.98												
	-1633	24.92	-52.06		1.07	29.	0.40	1868.	15	1	0.93	0.93	9.33												
0931-32	931.2	261.92	149.74	9	11.2	0.28	929.	243	2	17.41	20.9	10.42	10.42	2.7											
	-3249	13.63	-50.30		1.37	79.	1.72	840.	10	1	0.8	18.4	9.85												
N 2935	934.5	253.60	130.86	4X	5.8	0.83	11.45	2275.	307	2	10.85	34.0	10.22	2.2											
	-2054	22.59	-51.33		1.09	35.	0.48	2009.	15	1	1.03	22.8	9.64												
0935-22	935.6	254.78	132.87	7X	3.6	0.83	2412.	193	2	3.11	22.8	9.15	10.72	2.7											
	-2210	21.89	-51.04		1.10	35.	0.50	2143.	20	1	1.01	1.49	9.15												
U 5139	936.0	140.73	38.79	10	5.3	0.96	12.90	141.	46	4	10.04	4.5	7.95												
	7125	38.65	1.31		1.00	17.	0.10	289.	5	1	0.62	23.9	9.35												
U 5172	938.6	169.23	53.45	9A	3.1	1.00	14.20	2597.	80	1	1.16	20.0	8.91												
	4854	47.76	-15.76		1.00	1.00	0.02	2635.	20	1	0.26	20.0	8.91												
0941-05	941.1	241.83	107.95	7A	3.8	0.89	2028.	102	1	1.99	20.0	8.81	8.81												
	-541	33.87	-47.55		1.02	28.	0.25	1808.	15	1	0.43	5.8	7.95												
0941-31	941.8	263.00	147.59	10	2.1	1.00	12.09.	70	2	2.25	5.8	8.28	10.39	4.4											
	-3157	15.79	-48.35		1.25	48.	0.66	922.	10	1	0.43	11.5	9.04												
0942-31	942.6	262.89	147.03	8X	4.1	0.87	12.56.	164	2	11.64	11.5	8.28	10.39	4.4											
	-3136	16.17	-48.26		1.24	30.	0.69	970.	10	1	1.02	4.0	8.27												
N 2976	943.2	143.93	41.37	5AP	9.7	0.59	10.56	9.	1	12.60	4.0	8.27	10.39	4.4											
	6808	40.91	-0.81		1.00	56.	0.29	142.	15	1	1.30	1.95	7.41												
U 5224	943.3	233.27	96.37	8B	2.7	0.52	14.50	1941.	184	1	2.75	14.0	8.88	6.7											
	312	39.55	-43.82		1.01	61.	0.44	1756.	15	1	0.77	7.8	9.56												
0943-30	943.3	261.97	144.82	10	3.7	0.27	13.70	1787.	148	2	5.11	7.8	9.56	7.3											
	-3008	17.35	-48.41		1.20	79.	1.57	720.	10	1	0.78	37.7	10.02												
N 2997	943.3	262.55	146.02	5X	16.2	0.88	9.94	1083.	279	2	6.63	37.7	10.02	6.7											
	-3057	16.75	-48.25		1.21	29.	0.66	798.	8	1	2.89	2.89	9.59												
N 3001	944.0	262.14	144.87	4X	6.0	0.69	12.07	2474.	398	2	8.87	38.2	11.35	1.9											
	-3012	17.41	-48.24		1.19	48.	0.73	2190.	25	1	1.66	9.18	9.63												
U 5238	944.3	236.07	99.65	7X	3.9	0.42	13.70	1787.	247	1	4.86	17.9	10.41	4.8											
	44	38.36	-44.60		1.01	68.	0.62	1592.	20	1	1.04	15.2	9.09												
U 5245	945.0	238.79	103.07	8	4.3	0.25	13.69	1425.	170	1	2.66	15.2	9.96	4.4											
	-148	37.01	-45.38		1.02	81.	1.22	1220.	25	1	0.5	0.59	8.60												
U 5249	945.2	233.59	97.08	6B	3.7	0.39	13.12	1882.	247	1	5.27	18.5	10.41	5.8											
	251	39.75	-43.53		1.01	70.	0.68	1695.	15	1	0.99	9.18	9.63												
N 3023	947.3	236.51	99.91	6XP	4.8	0.55	12.50	1877.	151	1	6.80	23.4	10.18	12.9											
	51	39.04	-43.86		1.01	58.	0.41	1683.	10	1	1.07	9.28	9.28												
U 5272	947.4	195.42	67.92	10	3.4	0.42	13.97	520.	164	1	4.06	4.7	9.47	3.0											
	3143	50.56	-26.82		1.00	68.	0.49	469.	15	1	1.03	7.95	7.95												
N 3020	947.4	222.36	85.57	6B	4.7	0.60	12.44	1447.	247	1	10.91	18.0	9.45	5.6											
	1303	45.33	-38.16		1.00	55.	0.30	1305.	15	1	1.07	16.3	9.42												
N 3026	948.0	200.02	70.51	10	3.9	0.33	12.70	1497.	225	1	2.91	16.3	9.42	3.4											
	2847	50.30	-28.65		1.00	74.	0.75	1431.	15	1	1.04	2.3	9.08												
0948+08	948.7	228.71	91.34	10 P	2.0	0.65	561.	397.	116	2	6.04	2.3	9.08	9.0											
	804	43.26	-40.41		1.01	51.	0.28	397.	8	1	1.00	0.62	7.98												

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	α_H	δ_H	r_H	B_T^i	V	W_{20}	tel.	F_c	A_H^b	$\log L$	$\log M_T$	$\%M_H/M_T$	M_T/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)		
0949+01	949.1	235.96	99.09	10	2.3	0.87	0.19	1853.	97	1	1.47	11.3	9.92	4.8	UGCA 186, DDO 65				
N 3041	950.4	217.67	82.03	5X	1.01	30.	12.04	1662.	10	1.02	0.39	8.61	10.85	1.3	00-25-024 2				
N 3027	951.2	138.78	35.44	78	1.00	48.	0.21	1295.	30	1.16	0.82	18.52	8.96	0.23	5303 03-25-039 2				
0953-32	953.0	265.51	148.23	6X	6.3	0.54	11.74	1211.	10	1.13	1.74	10.56	9.50	0.98	5316 12-10-009 2				
U 5340	953.8	199.88	71.19	10 P	1.22	59.	0.90	2731.	331	2	10.58	50.7	11.18	6.5	IC 2522, UGCA 189				
U 5349	955.1	186.16	64.34	9	3.9	0.48	13.89	441.	115	1	7.18	5.0	9.90	0.34	-5-24-004 2				
U 5364	956.4	196.90	69.94	10	7.0	0.64	12.90	1381.	220	1	0.66	15.5	8.14	1.68	5340 05-24-004 2				
U 5373	957.4	233.21	95.53	108	7.8	0.77	11.70	1361.	15	1.04	0.56	-17.32	8.83	0.51	5349 06-22-043				
0957-29	957.7	263.93	143.01	5	9.8	0.19	1.59	2197.	15	1.06	3.74	2.0	11.49	0.64	LEO A, DDO 69				
N 3079	958.6	157.77	51.00	98	11.0	0.21	10.09	28.	478	2	26.42	38.6	11.25	8.7	5364 05-24-008 2				
U 5391	958.7	186.16	64.88	9	3.5	0.45	13.68	-25.	10	1.07	1.78	2.9	6.01	0.10	SEX 8, DDO 70				
U 5393	958.8	193.04	68.28	98	3.5	0.60	13.88	302.	63	4	21.23	2.9	7.74	10.2	5373 01-26-005 2				
1000-05	1000.2	245.66	109.98	7	4.9	0.20	0.22	2477.	491	2	12.59	62.7	7.55	0.64	IC 2531, UGCA 191				
N 3109	1000.8	262.10	138.01	10	19.0	0.53	9.22	2197.	15	1.06	3.74	2.0	9.78	0.69	-5-24-015				
1000-21	1000.9	258.71	131.32	7X	2.1	1.00	0.33	2806.	20	1.01	0.30	8.75	9.51	3.2	UGCA 193				
N 3104	1000.9	180.29	62.40	10A	5.2	0.67	12.57	666.	157	1	5.03	6.4	9.51	4.5	UGCA 194, DDO 236				
N 3057	1001.0	130.66	33.78	88	4.2	0.84	13.16	449.	15	1.06	0.84	7.2	8.01	0.71	-1-26-012				
0001-26	1001.3	262.80	139.22	7A	5.5	0.45	0.20	1717.	7	1.22	9.83	17.4	8.58	16.1	UGCA 195				
0001-27	1001.5	263.21	139.99	5X	4.6	0.77	12.37	686.	20	1.02	0.30	8.75	9.51	3.2	-3-26-015				
N 3113	1002.3	263.96	141.18	8	5.4	0.49	0.53	617.	118	1	5.73	9.4	9.66	8.3	ARP 264, W 119				
U 5455	1004.6	139.53	40.86	10	3.1	1.00	0.07	1291.	72	1	1.05	13.0	8.74	0.40	5414 07-21-007 2				
U 5459	1004.8	160.84	53.53	5	6.0	0.20	12.34	1438.	15	1.05	0.45	8.70	8.70	0.29	DDO 67				
U 5460	1004.9	162.63	54.46	78	3.9	0.93	13.14	1084.	15	1.09	1.36	20.7	10.52	4.9	5455 12-10-000				
U 5478	1006.6	198.24	71.96	10	2.9	0.90	14.41	1381.	80	1	1.67	11.2	8.64	0.38	5460 09-17-027 2				
3137	1006.9	265.22	141.90	7	8.5	0.47	0.82	1109.	269	2	29.15	20.8	10.58	0.63	5478 05-24-020 2				
0008-25	1008.3	263.28	137.40	9	3.6	0.83	0.45	2543.	10	1.05	2.02	23.3	9.30	5.4	UGCA 203				
0008-04	1008.5	246.14	109.05	108	9.4	0.92	11.69	325.	64	4	37.61	3.1	9.90	13.5	UGCA 204, DDO 237				
3153	1010.2	226.26	89.20	5	3.5	0.49	12.91	2811.	247	1	2.94	27.4	10.63	1.15	SEX A, UGCA 205, DDO 75				
5518	1011.2	181.98	64.78	10	3.3	0.61	0.39	2672.	15	1.04	0.61	20.3	9.32	4.9	-1-26-030 2				
	3943	55.23	-17.94		1.00	0.54	0.19	2109.		1.04	0.41	8.44		0.28	5518 07-21-028				

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	ϕ_H	r_H	$B_{0.1}^i$	V	W_{20}	tel.	F_C	A_H^b	flag	$\log L$	$\log M_T$	% M_H/M_T	M_T/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)		
U 5522	1011.3	233.88	95.46	6	4.4	0.64	0.64	13.22	1228.	232	1	10.04	13.8	8.96	10.38	4.7	26.7	5522 01-26-025	
	716	47.60	-35.78		1.00	52.	52.	0.26	1065.	15	1.07	1.22		-16.92	9.06	1.25			
U 5539	1013.3	239.45	100.64	108	3.4	0.55	0.55	13.96	1278.	160	1	3.93	11.0	8.69	9.89	6.1	16.0	5539 01-26-029	
	256	45.51	-37.06		1.01	58.	58.	0.36	1097.	20	1.04	1.14		-16.24	8.67	0.97		IC 600, UGCA 209	
1014-03	1014.7	246.34	108.17	88	3.9	0.48	0.48	0.49	1314.	187	1	4.71	12.7	10.05	10.05	5.1		00-26-034	
	-315	41.83	-38.83		1.01	64.	64.	0.49	1109.	15	1.05	1.10		8.76				NGC 3180	
N 3184	1015.2	178.36	63.70	6X	9.5	1.00	1.00	10.41	599.	148	1	29.75	16.8	9.59	9.04	0.28		5557 07-21-037 2	
	4140	55.62	-16.12		1.00			-0.01	604.	8	1.44	1.38		-18.50					
N 3198	1016.7	171.21	60.57	58	11.9	0.41	0.41	10.47	660.	322	4	48.67	23.9	9.68	10.76	4.0			
	4549	54.80	-13.27		1.00	69.	69.	0.48	686.	7	1.09	2.81		-18.71	9.36	12.1		5572 08-19-020 2	
N 3206	1018.5	154.07	51.96	68	4.4	0.70	0.70	12.29	1161.	209	1	8.52	16.0	9.47	10.42	5.0			
	5712	50.15	-5.68		1.00	47.	47.	0.14	1245.	15	1.07	0.75		-18.19	9.12	0.45		5589 10-15-069 2	
N 3223	1019.4	270.80	148.37	3A	5.9	0.71	0.71	11.10	2900.	425	2	7.05	45.1	10.59	11.50	1.5		8.2	
	-3400	19.11	-40.22		1.16	46.	46.	0.66	2617.	25	1.03	1.66		-20.99	9.68	0.12		IC 2571	
U 5612	1020.1	138.17	41.52	88	5.0	0.69	0.69	12.80	1011.	172	1	5.39	17.0	9.20	10.27	3.9		DDO 77	
	7108	41.61	3.57		1.00	48.	48.	0.20	1161.	10	1.09	0.84		-17.52	8.86	0.46		5612 12-10-032 2	
N 3225	1021.8	152.14	51.33	5	3.5	0.56	0.56	12.88	2137.	259	1	4.66	22.8	9.74	10.63	5.4		7.9	
	5824	49.86	-4.57		1.00	58.	58.	0.26	2227.	15	1.04	0.68		-18.86	9.36	0.42		5631 10-15-077	
U 5633	1022.0	225.34	88.66	88	3.9	0.68	0.68	13.92	1390.	179	1	3.39	14.4	10.59	10.22	3.3		24.7	
	1500	53.73	-29.94		1.00	48.	48.	0.18	1264.	15	1.05	0.75		-16.59	8.73	0.80		DDO 79	
N 3239	1022.4	221.64	86.29	98P	8.0	0.70	0.70	12.24	754.	200	1	20.76	14.9	8.91	10.36	3.7		28.1	
	1125	54.82	-28.68		1.00	47.	47.	0.16	639.	7	1.23	1.55		-16.79	8.93	1.04		ARP 263, VV 95	
1023+56	1023.8	154.36	52.95	13 P	0.7	0.61	0.61	10.66	799.	62	1	0.87	1.8	9.44	8.33	31.6		5637 03-27-025 2	
	5631	51.13	-5.57		1.00	54.	54.	0.37	880.	20	1.00	0.28		-18.86	9.36			UGCA 211, MARK 32	
N 3246	1024.1	240.48	100.54	8X	3.5	0.64	0.64	12.85	2150.	262	1	4.96	20.3	9.64	10.66	4.2		10.3	
	407	48.37	-34.12		1.00	52.	52.	0.26	1977.	15	1.04	1.07		-18.63	9.29	0.44		5661 01-27-009	
U 5662	1024.2	201.66	75.73	38	5.2	0.17	0.17	13.94	1327.	235	6	2.74	19.3	8.82	10.33	2.1		32.0	
	2853	58.17	-22.28		1.00	90.	90.	0.08	1269.	40	1.10	0.63		-16.58	8.64	0.67		NGC 3245A	
U 5666	1024.8	140.20	43.67	9X	16.0	0.50	0.50	10.66	38.	117	1	117.77	8.3	8.42	9.47	12.5		0.67	
	6840	43.62	2.29		1.00	62.	62.	0.37	177.	10	1.71	4.15		-15.58	8.57	11.0		5662 05-25-012 2	
U 5675	1025.8	218.21	84.39	9	3.1	0.77	0.77	11.04	1104.	88	1	1.37	9.1	9.66	9.36	4.1		1.40	
	1949	56.46	-26.75		1.00	41.	41.	0.10	1001.	10	1.04	0.34		-18.68	8.70	0.51		5666 12-10-038 2	
U 5688	1026.6	138.44	42.50	98	5.2	0.62	0.62	12.66	1916.	68	1	3.32	31.4	9.76	9.66	30.9		5675 03-27-047	
	7019	42.57	-18.23		1.00	53.	53.	0.25	2063.	8	1.09	0.44		-18.91	9.15	0.8		VII 2M 331, VV 294, DDO 80	
N 3261	1026.9	277.96	161.00	58	6.7	1.00	1.00	11.07	2571.	403	2	11.55	44.8	10.48	10.10	0.25		5688 12-10-044 2	
	-4424	11.20	-36.67		1.64	0.99	0.99	0.99	2280.	30	1.05	2.98		-20.72	8.96	0.20		-7-22-015 2	
U 5707	1028.3	174.22	63.85	6X	3.9	0.75	0.75	13.57	2800.	130	1	2.92	32.1	9.66	10.38	9.6		5.2	
	4323	57.51	-13.16		1.00	42.	42.	0.10	2816.	15	1.06	0.43		-18.68	9.36	0.51		5707 07-22-016	
U 5706	1028.3	190.37	71.09	10	2.5	0.82	0.82	12.91	1494.	65	1	1.20	10.7	9.43	9.6			KAR 70	
	3446	59.16	-18.23		1.00	36.	36.	0.06	1466.	15	1.03	0.26		-18.91	9.15	9.6		5706 06-23-000	
U 5708	1028.6	240.79	100.36	7X	4.9	0.25	0.25	12.79	1177.	205	1	9.02	14.4	9.08	10.10	7.2		10.4	
	4444	49.63	-32.85		1.00	81.	81.	1.12	1007.	10	1.06	0.85		-17.22	8.96	0.76		5708 01-27-014	
N 3264	1029.2	153.54	53.57	58	5.0	0.48	0.48	13.07	942.	182	1	4.74	14.9	9.66	10.10	3.9		12.9	
	5620	51.85	-5.10		1.00	64.	64.	0.35	1023.	10	1.07	0.75		-16.98	8.70	0.52		5719 09-17-069	
N 3274	1029.5	203.78	77.29	6XP	3.3	0.57	0.57	12.91	543.	178	1	13.60	4.6	8.39	9.63	7.4		17.1	
	2755	59.21	-21.83		1.00	57.	57.	0.23	481.	8	1.03	1.15		-15.50	8.50	1.28		5721 05-25-020 2	
N 3282	1030.4	134.80	39.78	68	3.1	0.41	0.41	13.48	1136.	275	1	2.55	11.8	9.03	10.32	2.0		19.6	
	7401	40.06	6.00		1.00	69.	69.	0.56	1299.	30	1.03	0.66		-17.09	8.63	0.40		0.40	
U 5740	1031.7	161.18	58.02	9X	3.4	0.63	0.63	14.39	651.	170	1	3.19	7.0	8.14	9.81	47.8		5732 12-10-049 2	
	5101	54.58	-8.08		1.00	52.	52.	0.18	707.	25	1.04	0.63		-14.86	8.20	2.5		47.8	
1033-24	1033.0	267.58	135.92	88	5.3	0.87	0.87	0.35	1048.	86	2	8.13	12.1	9.85	9.85	7.1		1.15	
	-2430	28.62	-37.84		1.05	30.	30.	0.35	785.	10	1.03	0.69		-15.13	8.70	0.3		5740 09-17-075	
N 3299	1033.8	230.77	92.24	8X	3.1	0.86	0.86	13.21	597.	158	1	1.01	4.2	8.24	9.89	44.7		UGCA 212, DDO 238	
	1257	55.30	-28.33		1.00	31.	31.	0.08	465.	30	1.04	0.40		-15.13	7.34	0.13		-4-25-024 2	
U 5764	1033.9	196.16	74.36	10	3.1	0.64	0.64	14.34	584.	161	1	3.69	4.9	7.93	9.62	2.6		5761 02-27-029 2	
	3149	60.43	-18.91		1.00	52.	52.	0.17	543.	20	1.03	0.59		-14.33	8.04	1.28		ARP 267, DDO 83	

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	q_H	r_H	B_T^i	V	W_{20}	tel.	F_c	A_H^b	log L	log M_T	% M_H/M_T	M_T/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	
1033-36	1033.9	275.11	151.55	10	1.00	0.51	0.58	959.	67	2	3.69	0.65	29.5	8.57	5.2			-6-24-000
N 3321	1036.3	18.25	119.73	5	4.5	0.51	0.48	2489.	277	1	6.06	2.20	29.5	10.78	5.2		UGCA 214	
N 3319	1036.4	175.99	65.95	68	8.8	0.49	0.45	743.	218	4	18.36	2.03	19.4	9.37	4.5	10.1		-2-27-010
	4156	59.37	-12.81		1.00	0.63	0.33	754.	10	1.06				-17.94	9.02	0.45	5789 07-22-036 2	
1038-23	1038.9	267.97	134.24	10	3.1	0.86	0.33	1199.	155	2	4.77	8.5	8.5	10.19	2.7		UGCA 215, DDO 85	
U 5829	1039.8	190.06	72.51	108	7.2	0.86	13.11	633.	97	1	15.55	12.8	8.63	9.95	6.5	27.3	DDO 84	-4-25-058 2
N 3346	1041.0	228.82	90.90	68	3.9	0.96	12.46	1257.	175	1	4.92	13.0	15.81	8.76	1.74		5829 06-24-006 2	
	1508	57.88	-25.80		1.00	17.	0.03	1137.	20	1.07	0.59			-17.82	8.80	0.30	5842 03-28-001 2	
1041-09	1041.1	258.59	117.90	7	2.9	0.85	0.20	2077.	182	1	4.17	15.9	15.9	10.57	3.9			
U 5846	1041.2	147.02	51.09	10	3.1	1.00	14.10	1018.	69	1	4.08	10.2	8.65	9.16			DDO 86	-2-28-001
U 5848	1041.3	151.84	54.30	9	3.3	0.70	14.20	829.	134	1	2.07	8.8	8.43	8.71	1.15		5846 10-16-002 2	
	5641	52.98	-3.56		1.00	47.	0.13	914.	15	1.04	0.64		-15.61	9.24	2.9	0.64	5848 09-18-015	
N 3359	1043.4	143.58	48.91	58	9.0	0.62	10.80	1013.	263	1	50.17	29.7	29.7	10.81	9.9	6.8		
N 3365	1043.7	247.76	104.83	5	6.4	0.25	11.86	986.	251	1	12.51	15.1	15.1	9.81	4.1	0.67	5873 11-13-037 2	
N 3368	1044.2	234.46	94.34	2X	10.8	0.72	9.96	899.	375	4	26.41	24.1	24.1	10.30	10.7	10.7	5878 00-28-006 2	
	1205	57.03	-26.40		1.00	45.	0.14	766.	10	1.10	3.07		-19.46	9.19	1.1	14.4	M 96	
U 5889	1044.7	230.96	92.13	9	2.7	0.95	14.12	571.	77	1	1.63	3.5	3.5	7.85		0.16	5882 02-28-006 2	
U 5918	1046.2	140.51	47.21	10	4.4	1.00	0.03	336.	83	1	4.70	6.0	6.0	7.52	0.46		DDO 88	5889 02-28-007 2
U 5947	1047.8	221.53	87.02	10 P	2.3	0.61	14.51	1253.	98	1	1.69	7.8	7.8	8.01	9.9	7.0	DDO 87, KAR 72	
	1955	61.34	-22.20		1.00	54.	0.19	1158.	12	1.02	0.35		-15.81	9.36	0.68		5918 11-13-039 2	
N 3423	1048.7	244.17	101.00	6A	5.7	0.96	11.56	1008.	179	1	12.35	14.2	14.2	8.95	0.33		DDO 89 11-13-039 2	
1048-19	1048.9	268.02	130.21	68	3.9	0.27	0.06	2054.	278	6	6.14	20.6	20.6	10.52	6.0		5947 03-28-017 2	
U 5979	1049.2	138.29	45.35	10A	2.9	0.80	14.40	1121.	111	1	2.13	10.7	10.7	8.63	4.8	16.5	UGCA 221	
	6815	45.44	3.83		1.00	38.	0.11	1261.	10	1.03	0.43		-16.10	8.53	0.79		-3-28-015	
N 3433	1049.4	238.31	96.62	5A	5.6	0.91	12.39	2720.	262	1	5.94	42.2	42.2	10.06			5979 11-13-043	
N 3432	1049.7	184.74	71.71	98	8.2	0.29	10.86	611.	273	4	29.69	14.4	14.4	9.60	0.35	0.35	5981 02-28-023 2	
N 3437	1049.9	215.18	84.14	5X	4.2	0.38	12.16	1291.	341	1	4.68	14.9	14.9	10.36	4.7	8.9	ARP 206, VV 11	
	2312	62.82	-20.25		1.00	71.	0.55	1212.	30	1.05	0.74		-18.26	8.84	1.8	12.5	5986 06-24-028 2	
N 3443	1050.3	225.99	89.32	7A	3.9	0.51	13.66	1132.	183	1	2.56	11.7	11.7	10.01	2.6	18.2	5995 04-26-016 2	
N 3447	1050.7	227.57	90.15	7X	5.9	0.59	12.55	1073.	148	1	0.76	16.6	16.6	8.43	0.48		6000 03-28-025	
N 3445	1051.5	149.61	54.63	9X	2.7	0.95	12.79	2026.	181	1	5.07	16.7	16.7	8.96	0.66		VV 252	
	5715	53.67	-2.10		1.00	19.	0.01	2116.	25	1.03	0.53		-18.84	9.36	0.42		6006 03-28-027 2	
U 6027	1051.7	141.79	48.82	10	2.3	0.61	0.21	1701.	82	1	1.00	12.2	12.2	9.41	12.9		ARP 24, VV 14	
U 6035	1052.8	227.34	90.02	108	2.2	0.93	14.84	1073.	56	1	1.73	6.2	6.2	8.52			6021 10-16-023 2	
N 3486	1057.8	202.06	79.43	5X	9.8	0.73	10.75	679.	246	4	33.36	18.1	18.1	8.21	0.95	0.95	6027 11-13-000	
	2915	65.52	-15.81		1.00	44.	0.11	632.	10	1.09	2.54		-18.25	9.12	2.9	14.6	6035 03-28-035	
U 6112	1059.9	229.71	91.19	7	3.5	0.41	13.36	1037.	190	1	5.02	9.5	9.5	8.79	5.5	13.1	6079 05-26-032 2	
N 3501	1100.2	227.31	90.01	5	5.4	0.21	12.35	1139.	319	1	4.39	16.4	16.4	8.64	0.71		6112 03-28-050	
	1815	63.39	-20.31		1.00	86.	1.08	1040.	15	1.07	0.72		-17.74	8.68	1.4	17.5	6116 03-28-051	

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	a_H	r_H	$B_T^{b,i}$	V	σ	W_{20}	tel.	F_C	Δ_H^b	log L	log M_T	% M_H/M_T	M_T/L	Alternate Names
(1)	(2)	(3)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
N 3507	1100.8 1824	227.14 63.58	89.93 -20.11	38	4.9 1.00	0.84 34.	11.36 0.05	977. 879.	158 10	1.10	5.44 0.79	12.6	9.54 -18.36	10.32 8.62	2.0	6.0 0.12	6123 03-28-053 2		
N 3511	1100.8 -2250	272.87 -31.40	134.31 -31.40	5A	8.2 1.03	0.43 67.	10.88 0.69	1104. 854.	325 10	1.29	21.15 1.79	20.3	9.70 -18.78	10.70 9.19	3.1	10.0 0.31	UGCA 223		
N 3510	1101.0 202.38	79.87 66.21	15.24 -15.24	98	5.9 1.00	0.28 79.	12.40 0.93	710. 664.	200 10	1.09	11.74 1.11	11.4	8.88 -16.71	9.98 8.71	5.4	12.8 0.68	6126 05-26-040 2		
N 3513	1101.3 -2258	273.07 33.32	134.47 -31.29	58	4.5 1.03	0.85 33.	11.67 0.30	1195. 945.	110 8	1.14	5.91 0.70	12.5	9.47 -18.21	10.02 8.72	5.0	3.5 0.18	UGCA 224		
N 3521	1103.2 14	255.52 58.82	108.58 -26.23	4X	13.6 1.00	0.51 61.	9.33 0.38	804. 628.	466 10	1.13	66.53 9.51	25.0	10.06 -19.66	11.15 9.42	1.9	12.5 0.23	6150 00-28-030 2		
U 6151	1103.2 2005	224.11 64.77	88.57 -18.88	9	2.9 1.00	1.00	-0.01	1330. 1241.	41 7	1.04	1.46 0.20	10.5	9.46	8.35		DDO 91	6151 03-28-057 2		
U 6157	1103.7 1746	229.10 63.93	90.85 -19.75	8A	2.9 1.00	0.90 26.	14.12 0.03	2959. 2859.	160 15	1.04	2.88 0.48	24.2	9.46 -18.16	9.37		0.82	6157 03-28-058		
U 6162	1103.9 5128	155.23 58.86	60.49 -3.66	6	3.8 1.00	0.53 60.	13.39 0.28	2203. 2268.	223 10	1.04	4.15 0.88	25.2	9.55 -18.39	10.53 9.33	6.3	9.6 0.60	6162 09-18-086		
U 6161	1104.0 4400	167.85 63.19	66.95 -7.44	88	4.4 1.00	0.58 56.	13.25 0.22	765. 703.	133 10	1.06	5.56 0.68	10.2	8.69 -16.25	9.72 8.54	6.7	10.7 0.71	6161 07-23-024		
U 6171	1104.6 1850	227.10 64.58	89.92 -19.11	10 P	3.8 1.00	0.76	13.98 0.80	1212. 1118.	173 15	1.04	3.10 0.51	12.4	8.70 -16.26	9.90 8.59	4.9	16.0 0.77	6171 03-28-061		
1106-28	1106.5 -2806	277.06 -30.44	140.53 -30.44	10	3.7 1.05	0.33 74.	10.16 1.03	1499. 1239.	182 15	1.01	5.83 0.87	13.3	9.98 8.95			9.4	UGCA 226		
1107-23	1107.5 -2326	274.84 33.57	135.16 -29.92	4A	3.5 1.03	0.93 22.	12.33 0.27	2090. 1841.	59 8	1.11	5.77 0.50	21.0	9.79 -19.00	8.95 11.21		0.32	IC 2627, UGCA 227		
N 3549	1108.1 5340	151.32 57.84	58.91 -1.99	5A	4.8 1.00	0.37 72.	11.89 0.58	2867. 2944.	419 10	1.06	5.38 0.84	41.3	10.37 -20.45	9.29 9.67	2.9	6.9 0.20	6215 09-18-097 2		
N 3556	1108.7 5557	148.29 56.26	56.98 -0.77	68	11.1 1.00	0.41 69.	10.16 0.48	697. 785.	328 8	1.32	47.99 2.18	25.4	9.92 -19.31	10.80 9.47	4.7	7.7 0.36	6225 09-18-098 2		
U 6251	1110.5 5352	150.58 57.95	58.92 -1.58	9X	3.0 1.00	0.76 42.	14.48 0.09	928. 1006.	61 7	1.03	2.76 0.33	8.8	8.41 -15.53	9.18 8.45	18.5	5.9 25.1	DDO 92	6225 09-18-098 2	
U 6258	1111.2 2147	221.81 67.11	87.79 -16.47	10	3.3 1.00	0.31 76.	14.38 0.80	1460. 1382.	215 20	1.03	2.48 0.53	13.3	8.72 -16.32	10.12 8.68	3.6	0.90	6251 09-19-006 2		
N 3583	1111.4 4836	158.09 61.63	63.58 -4.05	38	4.0 1.00	0.76 42.	11.65 0.09	2135. 2188.	362 25	1.06	5.99 1.26	25.6	10.21 -20.05	11.19 9.46	1.9	9.4 0.18	6258 04-27-008		
N 3596	1112.4 1504	236.86 64.41	94.36 -18.92	5X	6.1 1.00	1.00	11.56 -0.01	1193. 1084.	135 10	1.18	8.69 0.82	19.3	9.64 -18.61	9.46 9.01		0.23	6263 08-21-008 2		
N 3600	1113.0 4152	170.31 65.66	69.64 -7.05	1	6.1 1.00	0.31 76.	11.55 0.80	719. 740.	221 10	1.10	11.83 1.15	13.2	9.31 -17.80	10.14 8.81	4.7	6.8 0.32	6277 03-29-013 2		
N 3614	1115.5 4602	161.54 63.77	66.17 -4.68	5X	6.4 1.00	0.64 52.	11.85 0.17	2339. 2381.	310 10	1.14	7.63 0.78	44.5	10.21 -20.03	11.15 9.64	3.1	8.8 0.27	6283 07-23-038 2		
N 3621	1115.9 -3234	281.24 64.08	145.72 -28.54	7A	12.6 1.07	0.52 61.	9.24 0.66	734. 470.	290 10	1.12	157.72 7.47	17.3	9.84 -19.12	10.59 9.54	9.0	5.7 0.50	6318 08-21-015 2		
N 3623	1116.3 1323	241.29 64.23	96.38 -18.69	1X	11.9 1.00	0.38 71.	0.66 0.56	806. 692.	508 20	1.09	6.18 1.09	24.1	10.03 -19.59	11.15 8.47	0.2	13.2 0.03	UGCA 232		
U 6345	1117.6 248	257.43 57.10	107.11 -22.01	108	3.8 1.00	0.64 52.	13.25 0.22	1609. 1450.	142 15	1.05	5.77 0.62	16.1	9.21 -17.56	10.03 9.08	11.3	6.5 0.75	M 65, ARP 317		
N 3627	1117.6 1317	241.92 64.42	96.60 -18.43	3X	13.8 1.00	0.47 64.	9.34 0.37	737. 623.	382 15	1.13	14.30 1.20	25.1	10.04 -19.63	10.96 8.74	0.6	8.2 0.05	6328 02-29-018 2		
N 3628	1117.7 1353	240.82 64.80	96.03 -18.19	3 P	18.0 1.00	0.24 82.	9.08 1.07	846. 734.	478 8	1.19	65.21 3.60	38.6	10.29 -20.25	11.26 9.55	1.9	9.3 0.18	6346 02-29-019 2		
N 3629	1117.9 2714	208.19 69.79	83.35 -12.78	6A	3.3 1.00	0.78 40.	12.47 0.08	1520. 1471.	253 20	1.04	5.62 0.83	14.2	9.54 -18.37	10.65 9.08	2.7	13.0 0.35	6350 02-29-020 2		
N 3631	1118.3 5328	145.48 59.03	59.82 -0.76	5A	7.2 1.00	1.00	11.04 -0.01	1161. 1239.	133 8	1.06	12.25 0.93	26.1	9.96 -19.43	9.27		0.21	6352 05-27-058 2		
N 3655	1120.3 1652	235.59 66.97	93.38 -16.48	5A	2.6 1.00	0.66 50.	12.15 0.15	1481. 1384.	325 20	1.02	3.32 0.69	10.5	9.61 -18.56	10.58 8.80	1.7	9.3 0.16	6360 09-19-047 2		

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	b_{dH}	r_H	B_V^i	V	W_{20}	tel.	F_C	A_H^D	$\log L$	$\log M_T$	% M_H/M_T	M_T/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	
U 6399	1120.6	152.05	62.01	9	4.8	0.31	13.30	805.	173	1	2.39	12.2	8.75	9.90	2.3	13.8		
N 3659	1121.1	233.09	92.29	98	3.1	0.54	12.51	1291.	263	1	1.06	0.46	-16.41	8.26		0.32	6399 09-19-060	
N 3657	1121.1	149.21	60.25	5XP	4.3	1.00	12.22	1200.	30	1	1.03	1.73	-17.89	8.90		0.35	6405 03-29-040 2	
N 3664	1121.8	258.01	106.64	98P	3.0	0.90	12.91	1370.	134	1	5.44	10.7	-18.34	9.15		0.42	6406 09-19-065 2	
N 3666	1121.8	246.39	98.63	5A	6.2	0.33	11.59	1067.	280	1	1.04	0.62	-17.1	8.91	3.9	0.51	ARP 5, VV 251, DDO 95	
N 3669	1122.6	143.34	56.09	9	3.4	0.30	12.15	1940.	410	1	1.10	1.42	-18.29	9.06		0.36	6420 02-29-025 2	
N 3673	1122.7	280.08	138.91	38	5.2	0.71	11.97	1946.	337	2	3.26	25.7	-19.40	9.10	1.8	0.14	6431 10-16-135 2	
N 3675	1123.5	163.63	68.75	3A	8.9	0.56	10.66	771.	426	4	1.02	0.82	-19.18	8.97	0.8	15.6	UGCA 236	
U 6446	1123.8	147.58	59.71	7A	5.8	0.67	12.72	643.	157	1	1.06	1.88	-18.87	8.98	0.9	19.5	6439 07-24-004 2	
U 6456	1124.6	127.84	36.91	13 P	2.6	0.60	14.34	-92.	10	1	1.12	0.96	-16.58	8.76	5.3	15.9	6446 09-19-079	
N 3705	1127.5	252.07	101.21	2X	6.9	0.49	11.11	1017.	361	1	12.36	18.0	-10.66	10.49	1.0	10.3	VII ZW 403	
N 3717	1129.1	283.14	143.02	2A	8.8	0.24	10.81	1731.	433	2	1.67	38.0	-18.64	8.99	5.8	0.22	6456 13-08-058 2	
N 3718	1129.9	146.99	60.71	18P	8.1	0.58	11.04	987.	480	4	1.83	25.3	-20.04	9.43	1.3	0.11	6460 03-29-051 2	
U 6531	1130.1	171.87	73.37	88	3.1	1.00	14.29	1565.	97	1	1.66	14.3	-17.76	9.02	1.6	0.53	6491 06-25-077	
U 6534	1130.4	136.56	51.58	6	4.4	0.33	12.42	1273.	149	1	1.05	0.34	-16.70	8.62	1.8	13.4	6498 02-29-039 2	
N 3726	1130.7	155.34	66.20	5X	8.2	0.77	10.86	861.	290	4	1.90	21.9	-18.31	8.80	1.6	0.17	UGCA 238	
U 6561	1130.8	151.89	64.23	10	2.2	0.58	13.59	250.	58	1	0.71	2.0	-18.95	9.22	1.9	0.17	ARP 214	
N 3733	1132.2	144.39	59.24	5	6.6	0.51	11.95	1188.	255	6	1.02	0.21	-13.90	6.85	1.3	0.34	6524 09-19-114 2	
N 3738	1133.0	144.59	59.61	10 P	4.4	0.73	11.99	1278.	115	1	1.21	1.02	-18.58	9.35	0.56	0.56	6531 07-24-022	
N 3735	1133.2	131.73	44.98	5A	6.0	0.28	11.27	2696.	509	1	7.56	50.0	-15.50	7.74	7.2	0.19	6534 11-14-030 2	
N 3755	1133.9	177.97	76.12	5XP	5.2	0.44	12.76	1572.	286	1	1.09	0.96	-21.01	9.79	1.9	0.28	6537 08-21-051 2	
N 3756	1134.0	144.60	59.87	5X	5.5	0.56	11.91	1294.	302	1	1.08	1.19	-18.23	9.37	3.5	3.5	MARK 178	
N 3782	1136.6	154.48	67.11	6XP	2.3	0.55	12.90	740.	133	1	0.76	5.3	-18.79	9.08	5.4	0.12	6541 08-21-053 2	
U 6616	1136.7	140.01	56.39	7A	4.4	0.82	13.29	1154.	119	1	0.74	16.2	-16.60	8.64	2.2	0.16	6565 09-19-123 2	
N 3780	1136.7	141.91	58.24	5A	4.5	0.82	11.73	2393.	317	1	3.83	32.7	-17.21	8.78	5.0	0.54	ARP 234	
U 6628	1137.4	155.21	67.70	9A	5.0	1.00	12.92	851.	56	1	5.75	13.2	-16.85	8.67	2.1	0.22	6565 09-19-130 2	
1138-09	1138.0	275.74	121.60	6X	3.9	0.96	-0.01	1736.	127	1	0.48	17.6		9.15	4.5	6.9	6567 12-11-036 2	
	-548	49.02	-20.48		1.01	17.	0.12	1540.	10	1	0.80				1.7	15.5	6577 06-26-008 2	
															0.23	6579 09-19-134 2		
															16.7	3.9	6618 08-21-087 2	
															4.5	0.65	6616 10-17-035	
															1.7	0.51	6615 09-19-150 2	
																0.17	6628 08-21-089 2	
																0.55	UGCA 241	
																	-2-30-014	

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	b_H	r_H	$B_{\rm T}^j$	V	W_{20}	tel.	F_c	Δ_H^b	$\log L$	$\log M_{\rm T}$	% $M_{\rm H}/M_{\rm T}$	$M_{\rm T}/L$	Alternate Names
(1)	(2)	(3)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
N 3804	1138.2	141.64	58.30	58.38	5A	3.8	0.71	12.99	1381.	179	6	4.22	16.4	9.34	10.31	4.5	9.5	6640 09-19-153 2
	5628	58.30	3.12	3.12		1.00	46.	0.12	1479.	10	1.08	0.65		-17.86	8.96		0.42	
N 3810	1138.4	252.94	99.97	99.97	5A	6.1	0.66	11.09	993.	277	1	12.29	15.7	9.65	10.62	2.3	9.3	6644 02-30-010 2
	1145	67.22	-14.22	-14.22		1.00	50.	0.16	882.	15	1.13	1.38		-18.64	8.98		0.21	
N 3813	1138.7	176.20	76.39	76.39	5A	3.3	0.61	12.11	1468.	317	1	6.72	14.2	9.69	10.64	3.3	9.1	6651 06-26-019 2
	3649	72.43	-4.79	-4.79		1.00	54.	0.19	1474.	25	1.04	2.13		-18.73	9.16		0.30	
1139-06	1139.0	273.68	117.94	117.94	10 P	2.6	0.72	16.98	1698.	115	1	1.22	11.5	9.79	10.52	4.5		UGCA 242
	-612	52.38	-19.38	-19.38		1.00	45.	0.20	1515.	25	1.02	0.36			8.45			-1-30-022
U 6667	1139.7	146.27	62.66	62.66	5	5.0	0.22	12.95	974.	205	1	2.74	15.3	9.06	10.12	2.3	11.6	6667 09-19-157
	5153	62.28	1.46	1.46		1.00	85.	1.08	1051.	20	1.06	0.52		-17.16	8.48		0.26	
U 6670	1139.8	238.31	93.50	93.50	10B	4.5	0.35	13.10	918.	217	1	4.03	11.0	8.80	10.06	2.5	18.2	6670 03-30-053 2
	1836	71.83	-11.52	-11.52		1.00	73.	0.65	838.	15	1.05	0.93		-16.52	8.45		0.45	
U 6682	1140.4	138.54	55.82	55.82	9	2.7	0.84	13.28	1328.	93	6	2.60	11.3	9.81	9.81	8.3		DDO 96
	5923	55.50	4.55	4.55		1.00	34.	0.05	1439.	10	1.05	0.44			8.73			6682 10-17-049 2
U 6706	1141.5	142.01	59.62	59.62	9 P	3.3	0.87	13.32	1431.	175	1	1.82	14.7	9.23	10.56	1.2	21.1	NGC 3846A, VV 320
	5519	59.53	3.08	3.08		1.00	30.	0.04	1525.	20	1.05	0.46		-17.60	8.63		0.25	6706 09-19-169 2
U 6713	1141.8	149.29	65.33	65.33	9	3.1	0.86	14.12	901.	103	1	3.53	8.7	8.51	9.84	4.8	21.2	MARK 186
	4907	64.72	0.66	0.66		1.00	31.	0.04	966.	7	1.04	0.58		-15.80	8.52		1.02	6713 08-21-094
1142-09	1142.8	277.41	121.90	121.90	4B	4.2	0.32	12.99	1299.	232	1	5.63	18.9	10.34	10.34	6.0		UGCA 245
	-949	49.47	-19.33	-19.33		1.01	75.	0.87	1536.	15	1.05	1.06			9.12			-2-30-027
N 3850	1142.9	140.86	58.93	58.93	5B	3.4	0.50	13.48	1166.	185	1	2.51	12.5	9.00	10.05	3.6	11.0	6733 09-19-174 2
	5609	58.90	3.59	3.59		1.00	62.	0.32	1264.	25	1.03	0.75		-17.03	8.60		0.40	
N 3870	1143.3	146.98	64.16	64.16	-2	2.0	0.80	10.69	750.	115	1	1.31	4.8	9.53	9.53	2.6		MARK 186
	5030	63.74	1.43	1.43		1.00	38.	0.28	822.	15	1.02	0.38		7.95	7.95			6742 08-22-001 2
N 3877	1143.5	150.72	66.68	66.68	5A	7.5	0.28	10.69	894.	347	1	5.86	20.9	9.87	10.72	1.0	7.1	6745 08-22-002 2
	4746	65.56	0.38	0.38		1.00	79.	0.93	954.	10	1.14	1.33		-19.21	8.73		0.07	
N 3887	1144.6	281.57	129.03	129.03	4B	5.2	0.91	11.42	1212.	263	1	12.78	15.1	9.62	9.10		0.31	-3-30-012 2
	-1635	43.33	-20.32	-20.32		1.01	25.	0.18	998.	10	1.12	2.47		-18.58	9.10		12.4	MARK 188
N 3888	1144.9	140.31	58.96	58.96	4X	2.7	0.84	12.66	2408.	283	1	3.92	19.8	9.93	11.02	2.4		6765 09-19-189 2
	5614	58.97	3.88	3.88		1.00	34.	0.05	2507.	15	1.03	1.09		-19.34	9.39		0.29	
N 3893	1146.1	148.11	65.72	65.72	5X	6.4	0.58	10.88	977.	308	1	20.14	19.5	9.88	10.73	4.1	7.2	6778 08-22-007 2
	4900	65.23	1.26	1.26		1.00	56.	0.22	1043.	8	1.13	1.21		-19.21	9.34		0.29	
U 6782	1146.3	222.59	88.83	88.83	10	3.1	1.00	-0.01	528.	92	1	1.71	4.3					DDO 97
	1146.3	75.52	-8.12	-8.12		1.00	0.35	12.96	477.	10	1.05	0.35			7.59			6782 04-28-057 2
U 6780	1146.3	273.12	113.92	113.92	7AP	5.0	0.35	0.71	1736.	239	1	7.99	23.0	9.40	10.46	6.8	11.5	6780 00-30-024
	-145	57.18	-16.44	-16.44		1.00	73.	0.71	1574.	10	1.07	1.17		-18.02	9.30		0.79	UGCA 247, DDO 239
1146-28	1146.3	286.56	141.20	141.20	9B	3.6	1.00	0.26	1692.	125	2	6.23	17.9		9.25			-5-28-007 2
	-2801	32.58	-21.69	-21.69		1.04	78.	0.88	1056.	10	1.02	0.74						IC 740
N 3913	1148.0	140.11	59.68	59.68	7A	4.4	0.94	12.71	956.	64	1	3.48	13.5	9.15				6813 09-20-001 2
	5538	59.70	4.05	4.05		1.00	20.	0.01	1053.	8	1.09	0.43		-17.40	8.59		0.27	VV 273, DDO 98
U 6816	1148.1	139.11	58.67	58.67	10B	2.6	0.83	14.15	896.	140	1	3.13	7.6	8.53	9.97	3.3	27.3	6816 10-17-086 2
	5844	58.73	4.47	4.47		1.00	35.	0.05	998.	10	1.03	0.47		-15.84	8.49		0.92	
N 3917	1148.2	143.61	62.96	62.96	6A	6.9	0.29	11.40	975.	279	1	5.18	21.3	9.68	10.55	1.6	7.3	6815 09-20-008 2
	5207	62.79	2.76	2.76		1.00	78.	0.88	1056.	10	1.12	1.12		-18.72	8.76		0.12	
U 6817	1148.2	166.25	74.96	74.96	10	6.5	0.48	12.80	248.	67	1	9.55	5.1	7.93	8.76	12.0	6.8	DDO 99
	3909	72.74	-2.16	-2.16		1.00	64.	0.35	269.	5	1.12	0.63		-14.35	7.84		0.81	6817 07-24-035 2
U 6818	1148.2	151.75	68.55	68.55	13 P	3.3	0.48	13.91	803.	163	1	3.50	8.3	8.49	9.74	4.7	17.7	
	4605	67.78	0.47	0.47		1.00	64.	0.50	857.	15	1.03	0.50		-15.76	8.41		0.83	6818 08-22-015
N 3930	1149.1	168.25	75.83	75.83	5X	6.2	0.80	12.32	919.	191	1	8.54	16.9	9.21	10.52	2.3	20.7	
	3817	73.41	-2.32	-2.32		1.00	38.	0.07	936.	20	1.15	0.88		-17.54	8.87		0.46	6833 06-26-045 2
U 6840	1149.5	142.94	62.79	62.79	9B	4.4	0.85	13.34	1019.	151	1	14.2	14.2	8.94	10.35		25.9	DDO 100
	5223	62.66	3.04	3.04		1.00	33.	0.05	1102.	15	1.08			-16.87	10.35			6840 09-20-019 2
N 3936	1149.9	287.01	139.84	139.84	5	5.8	0.25	11.67	2026.	335	2	3.73	30.1	9.08	10.84	1.7	6.5	UGCA 248
	-2638	34.13	-20.72	-20.72		1.03	81.	1.29	1789.	30	1.02	0.81		-19.59	9.08		0.11	-4-28-004 2
N 3924	1150.0	145.18	64.75	64.75	9	2.9	0.95	14.56	1003.	103	6	1.51	9.1	8.43	8.43		0.65	6849 08-22-026
	5018	64.49	2.34	2.34		1.00	19.	0.01	1077.	15	1.06	0.41		-15.60	8.24			

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	a_H^b	r_H^i	$B_T^{b,i}$	V	W_{20}	tel.	F_c	A_H^b	$\log L$	$\log M_T$	$\%M_H/M_T$	M_T/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	
11150-03	1150.0	275.50	115.82	10	2.2	0.86	0.11	1665.	122	1	1.51	0.38	9.6	10.03	3.2			IC 2969, UGCA 249
	-323	56.09	-16.01		1.00	31.	0.11	1499.	40	1.02	0.38	14.12	23.0	8.53				00-30-000
11150-28	1150.9	287.80	141.60	8	5.4	0.29	0.29	1702.	287	6	1.42	1.46		10.61	7.5			UGCA 250
	-2816	32.62	-20.71		1.04	78.	1.16	1461.	10	1.12	1.08	10.6		9.48				-5-28-015
N 3949	1151.1	147.63	66.83	4A	4.2	0.64	11.23	804.	284	1	1.08	1.28		10.45	2.7	7.5		
	4808	66.41	1.70		1.00	52.	0.17	868.	10	1.06	0.81			-18.46	8.88	0.20	6869 08-22-029 2	
N 3953	1151.2	142.21	62.67	5B	9.4	0.69	10.62	1054.	418	1	9.67	31.3		10.06	0.6	17.7		
	5237	62.58	3.37		1.00	48.	0.13	1139.	10	1.31	0.91			-19.66	9.10	0.11	6870 09-20-026 2	
N 3956	1151.4	285.19	133.23	5A	5.3	0.39	0.71	1660.	320	2	8.29	22.3		10.72	3.3			UGCA 251
	-2018	40.31	-19.41		1.02	70.	0.71	1439.	25	1.02	1.27			9.23			-3-30-016 2	
11152-16	1152.3	283.99	129.41	8	3.1	0.50	0.47	1811.	215	1	4.72	14.7		10.25	6.9			UGCA 254
	-1635	43.52	-18.51		1.01	62.	0.47	1601.	10	1.03	0.81			9.08				-3-30-019
N 3972	1153.1	138.86	59.98	4A	5.8	0.31	11.76	848.	265	1	3.30	16.0		9.44	1.2	8.8		
	5536	60.05	4.71		1.00	76.	0.80	947.	15	1.09	0.62			-18.12	8.47	0.11	6904 09-20-032 2	
U 6903	1153.1	273.27	111.15	6X	3.8	0.89	13.22	1894.	202	1	5.43	19.4		9.39				6903 00-31-002
	132	60.87	-13.92		1.00	28.	0.08	1748.	15	1.06	0.91			9.22		0.68		
N 3976	1153.4	267.53	105.77	5X	5.2	0.37	11.88	2504.	448	1	14.96	36.1		10.19	11.21	10.4		6906 01-31-001 2
	702	65.74	-12.23		1.00	72.	0.60	2381.	20	1.07	1.93			-20.00	9.93	0.55		
N 3981	1153.6	285.58	132.60	4 P	6.9	0.54	11.92	1717.	329	2	20.65	30.3		9.78	10.96	5.1	15.1	UGCA 255, ARP 289, VV 8
	-1936	41.12	-18.78		1.02	59.	0.45	1499.	15	1.04	1.78			-18.96	9.67	0.77		-3-31-001 2
U 6912	1153.7	136.44	57.32	13 P	3.7	0.51	14.21	1357.	134	6	3.78	15.9		8.84	9.87	11.0	10.8	VII 2N 430, VV 57
	5828	57.47	5.80		1.00	61.	0.46	1468.	10	1.07	0.52			-16.62	8.91	1.18		6912 10-17-104
U 6917	1153.9	143.47	64.61	9B	6.6	0.66	12.48	919.	206	1	7.44	19.2		9.20	10.45	2.6	17.8	
	5042	64.46	3.06		1.00	50.	0.15	996.	10	1.15	0.97			-17.51	8.87	0.47		6917 09-20-038
N 3982	1153.9	138.82	60.21	4X	3.7	0.92	11.72	1110.	236	6	5.57	13.1		9.67				
	5524	60.28	4.74		1.00	24.	0.02	1208.	15	1.10	0.76			-18.69	8.91	0.17		6918 09-20-036 2
U 6923	1154.2	140.51	62.05	10	3.4	0.42	13.52	1083.	170	1	1.93	11.6		8.92	9.90	3.3	9.5	
	5327	62.05	4.09		1.00	68.	0.46	1172.	15	1.03	0.69			-16.82	8.42	0.32		6923 09-20-040
U 6930	1154.7	144.56	65.73	7X	6.2	0.96	12.72	779.	140	1	5.02	15.4		8.96		0.72		6930 08-22-046 2
	4933	65.52	2.77		1.00	17.	0.01	851.	8	1.18	0.82			-16.93	8.82			
N 3992	1155.0	140.10	61.91	48	9.6	0.68	10.46	1051.	475	1	19.16	32.0		10.12	11.42	1.0	19.6	
	5339	61.93	4.27		1.00	48.	0.14	1142.	10	1.32	1.25			-19.83	9.40	0.19		6937 09-20-044 2
U 6955	1155.8	165.10	76.25	10	8.0	0.54	12.53	917.	160	1	7.95	21.9		8.96	10.19	4.5	16.7	DOO 105
	3821	74.39	-1.07		1.00	59.	0.27	938.	10	1.19	0.84			-16.93	8.84	0.77		6955 06-26-063 2
U 6956	1155.8	142.31	64.25	9B	4.0	0.93	0.88	935.	71	1	2.94	11.6						DOO 102
	5112	64.16	3.52		1.00	22.	0.01	995.	7	1.07	0.42			8.46				6956 09-20-050 2
11155-22	1155.9	287.17	135.38	10	3.9	0.71	0.32	1784.	160	2	3.59	17.7		10.25	4.9			UGCA 257, DDO 106
	-2211	38.78	-18.70		1.02	46.	0.32	1561.	15	1.01	0.73			8.94				-4-28-008 2
N 4010	1156.0	146.70	67.69	9	5.6	0.29	11.81	905.	276	1	8.98	15.8		9.44		9.3		
	4732	67.36	2.25		1.00	78.	0.88	968.	10	1.08	0.81			-18.12	8.93	0.31		6964 08-22-049 2
N 4013	1156.0	151.83	70.77	4	6.9	0.29	11.34	835.	398	1	7.98	17.8		9.55	10.78	1.0	16.9	
	4414	70.09	1.07		1.00	78.	0.88	883.	10	1.12	0.88			-18.39	8.79	0.18		6963 07-25-009 2
U 6962	1156.0	154.07	71.91	6X	3.8	0.85	12.76	784.		1	5.09	9.2		8.92				IC 749
	4301	71.05	0.63		1.00	33.	0.05	827.		1	1.06			-16.83	8.54	0.42		6962 07-25-008 2
N 4020	1156.3	193.95	83.46	7	3.1	0.54	12.81	757.	188	6	3.09	6.7		8.81		10.1		-971 05-28-066 2
	3041	78.03	-3.70		1.00	59.	0.27	742.	15	1.05	0.83			-16.54	8.23	0.26		UGCA 259
11156+46	1156.3	148.81	69.14	10	1.9	0.83	0.05	1154.	350	1	1.41	6.7		10.71		0.4		08-22-000
	4600	68.68	1.75		1.00	35.	0.05	1210.	20	1.01	0.30			8.31				
U 6983	1156.6	140.26	62.62	6B	6.1	0.75	12.77	1078.	200	1	8.55	20.8		9.22	10.57	3.1	22.3	
	5259	62.63	4.26		1.00	42.	0.10	1166.	10	1.14	1.04			-17.56	9.07	0.70		6983 09-20-051 2
N 4030	1157.8	277.35	113.81	4A	5.9	0.78	11.74	1463.	349	6	15.57	22.6		9.73	11.13	2.0	25.3	
	-49	59.22	-13.44		1.00	40.	0.14	1311.	15	1.22	0.80			-18.85	9.43	0.50		6993 00-31-016 2
U 6998	1158.3	276.76	112.79	9	2.9	0.80	0.12	1797.	74	1	1.74	15.2			9.65	12.4		
	15	60.25	-13.03		1.00	38.	0.12	1789.	15	1.03	0.38			8.74				6998 00-31-000
11158-24	1158.6	288.60	137.68	8	3.6	0.21	1.30	1808.	211	2	4.28	16.6		10.17		7.2		UGCA 263
	-2417	36.51	-18.43		1.02	86.	1.30	1581.	20	1.01	0.91			9.03				6998 00-31-000
N 4037	1158.8	260.04	99.78	5BP	4.2	0.90	12.46	936.	97	1	0.97	10.3		9.06		0.06		7002 02-31-015 2
	1340	71.95	-8.90		1.00	26.	0.03	844.	25	1.08	0.35			-17.17	7.84			

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	a_H^b	r_H	$B_T^{b,i}$	V	W_{20}	tel.	F_C	A_H^b	log L	log M_T	% M_H/M_T	M_T/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	
U 7007	1158.9 3337	179.97 77.56	80.50 -2.16	9	3.1 1.00	1.00	-0.01	786. 786.	67 10	1 1.05	0.89 0.30	7.1	7.74		7.74			7007 06-26-06.8
U 7009	1159.2	132.67	53.62	10	2.7 1.00	0.36 72.	13.68	1120. 1230.	187 15	6 1.03	1.83 0.59	9.9	8.91	9.89	3.7	9.4		
N 4051	1200.6	53.84	7.84	4X	8.0 1.00	0.73 44.	0.61 0.11	710. 763.	269 15	1.23	10.25	17.8	9.62	10.73	1.1	0.35	7009 11-15-010 2	
N 4062	1201.5	148.90	70.53	5A	6.6 1.00	0.47 64.	11.54 0.36	769. 764.	307 10	1 1.13	0.79 1.22	14.7	9.30	8.78	1.1	0.14	7030 08-22-059 2	
N 4068	1201.5	138.90	62.98	10A	4.4 1.00	0.64 52.	12.62 0.17	213. 302.	83 7	1 1.07	8.78 0.68	3.9	8.10	8.94	9.2	0.18	7045 05-29-004 2	
U 7056	1201.7	63.05	4.91	68	3.1 1.00	0.95 19.	13.47 0.01	1275. 1406.	116 10	6 1.07	1.39 0.45	12.7	9.10	7.90	0.64	6.9	7047 09-20-079 2	
U 7053	1201.8	53.77	8.17	10	2.9 1.00	0.85 35.	0.01	1406. 1463.	10 140	1 2.50	0.45 0.57	11.1	-17.27	8.44	0.22	0.22	7056 11-15-014 2	
1202-27	1202.2	290.57	141.52	9	3.6 1.03	0.88 29.	0.11	1311. 1787.	25 242	1.04	0.57	16.4	10.18	10.58	2.8		DDO 108	
N 4088	1203.0	140.35	65.00	5XP	4.4 1.00	0.40 67.	0.76	1618. 1618.	15 15	1.09	1.07	21.0	-19.33	9.08	3.4	9.0	UGCA 267, DDO 240	
1203-27	1203.2	290.78	141.36	58	4.4 1.03	0.40 69.	0.76	1618. 1618.	15 15	1.09	1.07	21.0	-19.33	9.08	3.4	9.0	ARP 18	
N 4094	1203.3	286.69	127.62	6	6.1 1.01	0.43 67.	11.91 0.57	1428. 1232.	271 10	1 1.10	6.61 2.15	21.8	9.61	10.58	2.6	9.4	UGCA 269	
U 7089	1203.4	149.94	72.00	9	5.0 1.00	0.32 75.	12.99 0.76	778. 826.	157 10	1 1.07	4.19 0.52	12.1	-18.54	9.00	4.4	9.5	-2-31-016 2	
1203-22	1203.5	38.84	-17.03	108	3.9 1.02	1.00	0.20	1498. 1498.	8	1.12	0.95	16.9	-16.59	8.46	0.42		7089 07-25-020	
N 4096	1203.5	143.54	67.92	5X	8.9 1.00	0.42 68.	10.55 0.46	577. 644.	340 15	1 1.21	17.39 1.62	16.7	9.59	10.66	1.6	11.7	UGCA 270	
N 4100	1203.6	141.11	65.93	5A	7.5 1.00	0.40 69.	11.04 0.50	1076. 1153.	415 20	1 1.15	12.74 1.72	25.2	-18.49	11.00	1.7	0.19	7090 08-22-067 2	
N 4102	1203.8	138.10	62.98	3X	4.7 1.00	0.63 52.	12.12 0.18	862. 953.	298 30	1 1.07	3.01 0.63	13.1	-19.27	9.23	0.7	0.21	7095 08-22-068 2	
1204+40	1204.8	155.97	75.23	10	2.2 1.00	0.86 31.	0.04	881. 914.	67 10	1 1.02	1.30 0.32	5.9	9.29	9.29	5.6	0.14	7096 09-20-094 2	
N 4116	1205.1	277.87	110.61	88	5.1 1.00	0.73 44.	12.25 11.77	1310. 1177.	235 15	1 1.10	12.82 1.50	17.5	9.43	10.60	4.5	14.8	UGCA 271, DDO 109	
N 4123	1205.6	277.96	-10.45	48	5.9 1.00	0.85 33.	11.77 0.08	1339. 1207.	211 10	1 1.14	13.70 1.60	20.8	-18.10	9.25	3.1	0.66	07-25-000 2	
N 4127	1206.0	126.12	39.73	4	4.7 1.00	0.55 58.	12.57 0.34	1821. 2006.	277 15	6 1.11	4.72 1.13	27.6	-18.64	9.30	3.2	10.0	7111 01-31-022 2	
U 7125	1206.2	163.31	78.15	9	6.5 1.00	0.24 82.	12.61 1.06	1078. 1098.	187 10	1 1.10	11.93 1.02	20.8	-18.94	9.28	9.5	8.8	7116 01-31-023 2	
N 4136	1206.7	193.68	84.58	5X	5.9 1.00	1.00 76.	11.75 0.80	618. 606.	112 8	1 1.17	11.63 0.80	10.4	-17.59	9.16	0.85	0.45	7122 13-09-012 2	
N 4142	1207.0	136.79	62.76	68	3.4 1.00	0.55 58.	13.47 0.25	1163. 1257.	187 10	1 1.04	3.42 1.40	12.5	-17.16	8.63	4.5	12.1	7125 06-27-014	
N 4145	1207.5	154.25	75.32	7X	8.5 1.00	0.69 48.	11.37 0.13	1013. 1048.	242 10	1 1.25	16.27 1.27	26.0	9.00	10.08	3.2	10.0	7134 05-29-025 2	
N 4144	1207.5	143.16	69.11	6X	9.0 1.00	0.31 76.	11.05 0.80	267. 331.	179 10	1 1.20	13.47 1.10	8.7	-18.73	9.25	2.4	0.37	7140 09-20-102 2	
1207-29	1207.7	292.36	143.38	5A	7.6 1.04	0.30 77.	11.08 1.12	2142. 1907.	308 15	2 1.04	14.33 2.45	43.4	10.32	10.95	5.9	4.3	7154 07-25-040 2	
N 4151	1208.0	155.09	75.81	2X	8.8 1.00	0.87 30.	11.09 0.04	999. 1022.	137 10	4 1.08	2.45 1.31	26.3	-20.32	9.72	0.25	0.25	TURN 57A	
U 7164	1208.0	127.86	45.98	9X	2.9 1.00	0.85 33.	0.04 0.08	2124. 2288.	101 15	1 1.03	1.44 0.49	19.4	-18.96	10.14	5.5	0.22	7166 07-25-044 2	
	7047	46.23	11.11		1.00									8.88			7164 12-12-000	

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	α_H^b	r_H	$B_T^{b,i}$	V	W_{20}	tel.	F_C	A_H^b	$\log L$	$\log M_T$	$\log M_H$	$\%M_H/M_T$	M_T/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)
U 7170	1208.1	252.34	95.31	5	4.4	0.15	13.78	244.4	232	1	6.05	30.6	9.43	10.51	10.6	12.0		7170	03-31-055
U 7175	1208.4	154.04	75.51	9	3.5	0.31	14.13	1168.	148	6	2.96	11.6	8.70	9.74	7.8	10.9		7175	07-25-046 2
U 7178	1208.5	280.17	111.52	10	2.5	0.70	0.80	1202.	30	1	0.63	8.8	-16.27	8.63	12.8	0.85		DDO 110	
	217	63.08	-10.02		1.00	47.	0.17	1205.	15	1.02	0.70			8.59				7178	00-31-036 2
N 4157	1208.6	138.46	65.33	3X	9.9	0.24	10.59	771.	431	1	29.25	24.7	9.82	10.97	2.3	14.3			
N 4163	1209.6	163.21	78.97	10A	3.3	0.96	13.04	170.	55	1.23	2.25	1.8	7.52	9.33	0.32			7183	09-20-106 2
U 7207	1209.8	160.37	78.18	10	3.8	0.53	0.28	1077.	104	1.08	0.36	11.9	-13.33	6.86	0.22			7199	06-27-026 2
	3718	77.11	1.17		1.00	60.			20	1.07	0.42			8.25	5.1			7207	06-27-027
N 4173	1209.8	197.21	85.59	7B	6.9	0.23	11.97	1127.	205	1	9.94	22.4	9.50	10.29	6.3	6.1			
	2928	81.14	-1.36		1.00	83.	1.08	1113.	20	1.12	0.99		-18.26	9.09				7204	05-29-033
U 7209	1210.0	269.76	101.85	4A	3.8	0.71	13.17	2235.	283	1	4.15	11.9	8.98	10.57	5.1	38.7		7209	02-31-047
	1224	72.44	-6.70		1.00	46.	0.12	2144.	50	1.05	2.00	V	-16.98	9.28	2.00			7209	02-31-047
N 4178	1210.2	271.84	103.07	8B	7.3	0.42	11.44	381.	286	1	17.26	22.8	9.67	10.64	0.3	9.3		7215	02-31-050 2
	1109	71.37	-7.03		1.00	68.	0.46	285.	15	1.15	1.54	V	-18.71	8.15	0.03			7215	02-31-050 2
1210-20	1210.4	290.86	133.93	10	2.7	0.52		1550.	127	6	2.45	10.8		9.67	9.5			UGCA 274	
U 7218	1210.4	136.37	63.71	10 P	2.3	0.55	0.47	1340.	15	1.04	0.62	5.9	8.31	9.32	4.5	10.2			-3-31-024
	5233	63.84	6.05		1.00	58.	0.25	791.	112	1	1.20		-15.29	7.97	0.46			7218	09-20-113
N 4183	1210.8	145.40	71.92	6A	7.4	0.19	11.84	934.	253	1	11.71	21.3	9.44	10.44	4.1	9.9			
	4358	71.74	3.48		1.00	90.	1.08	987.	10	1.13	1.25		-18.13	9.06	0.41			7222	07-25-051 2
N 4192	1211.2	265.42	99.29	2X	11.6	0.28	9.91	-142.	458	1	19.47	36.2	10.29	11.20	0.1	8.3		M 98	
N 4190	1211.2	160.62	78.63	10	2.9	0.95	13.24	234.	80	1.32	2.05	V	-20.24	7.97	0.1			7231	03-31-079 2
N 4189	1211.2	268.32	100.68	6X	3.4	0.85	12.47	2123.	301	1.04	0.50	2.2	7.71					VV 104	
	1343	73.72	-6.02		1.00	33.	0.45	2039.	7	6	0.74	10.6	-13.79	7.49	0.60			7232	06-27-030 2
U 7239	1211.6	276.69	106.16	10	3.8	0.93	13.82	1234.	112	1	1.11	12.5	8.77	9.00	1.5	36.7		IC 3050	
U 7249	1212.1	270.12	101.35	10	2.3	0.42	14.48	627.	130	6	1.21	7.2	-16.44	8.15	0.24			7239	01-31-028
	1305	73.29	-6.00		1.00	68.	0.46	541.	15	1.02	0.47	V	-15.67	7.55	9.9			DDO 114	
1212-35	1212.1	294.57	149.51	5B	5.2	0.66		2689.	317	2	5.07	37.4		11.11	2.4	0.12		7249	02-31-056 2
	-3515	26.75	-17.10		1.07	50.	0.52	2445.	25	1.02	1.23			9.48					-6-27-009
U 7257	1212.5	161.95	79.37	9	2.6	0.66	13.90	948.	100	1	3.69	7.3	8.60	9.40	13.8	6.3		KAR 91	
N 4204	1212.7	249.66	93.90	8B	6.5	1.00	12.78	861.	110	1.02	0.51	15.4	-16.03	8.54	0.87			7257	06-27-039 2
N 4206	1212.7	270.18	101.19	4A	6.6	0.24	11.73	701.	307	1.20	0.69	20.6	-16.76	8.72	0.67			7261	04-29-051 2
	1318	73.55	-5.80		1.00	82.	1.06	616.	25	1.03	1.38	V	-18.42	8.55	0.9	11.0		IC 3064	
U 7267	1212.9	136.22	64.69	9	3.1	0.45	13.99	473.	134	6	2.72	5.1	8.09	9.35	3.8	17.9		7267	09-20-128
U 7271	1213.0	144.66	72.30	7B	3.5	0.41	13.90	566.	15	1.04	0.64	6.1	-14.75	7.93	0.69			7267	09-20-128
N 4214	1213.1	160.30	79.06	10X	10.6	1.00	10.21	288.	4	1.05	0.56	9.6	-14.99	7.80	0.40			7271	07-25-052
	3636	78.07	1.57		1.00		-0.01	309.		1.13			-17.24					7278	06-27-042 2
U 7279	1213.2	274.17	103.47	9	3.4	0.17	13.70	1978.	248	6	4.44	10.6	8.77	10.12	12.0	22.1		IC 3074	
N 4217	1213.3	139.53	68.82	3	7.4	0.35	11.25	1028.	421	1.05	0.99	V	-16.45	9.20	2.68			7279	02-31-071 2
	4722	68.85	4.95		1.00	73.	0.65	1098.	20	1.14	12.23	23.7	9.77	10.97	1.6	15.7			
N 4216	1213.4	270.48	101.11	3X	10.4	0.36	10.28	139.	580	1	1.71	32.5	-18.95	9.17	0.25			7282	08-22-087 2
	1326	73.75	-5.60		1.00	72.	0.61	55.	25	1.27	2.14	V	-19.87	6.60	17.7			7284	02-31-072 2
1213-11	1213.8	289.39	125.21	10	2.4	0.27		1165.	140	6	1.94	6.9		9.45	6.6			DDO 116	
	-1116	50.40	-12.26		1.01	79.	1.09	985.	15	1.02	0.50			8.27					-2-31-026 2
N 4219	1213.8	296.21	157.68	4A	7.5	0.40	11.03	1993.	385	2	20.68	37.9	10.26	11.12	4.8	7.1			
	-4303	19.09	-17.62		1.17	69.	1.06	1739.	15	1.04	2.00		-20.17	9.80	0.34				-7-25-005 2

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	b_H	r_H	$B_T^{j,i}$	V	W_{20}	tel.	F_c	A_H^b	log L	log M_T	% M_H/M_T	M_T/L	Alternate Names
(1)	(2)	(3)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
U 7300	1214.1	199.20	86.34	10	2.7	1.00	1.00	-0.01	1215.	97	1	3.07	9.5		8.65			DDO 117
	2900	82.15	-0.62						1202.	15	1.04	0.50						7300 05-29-048 2
N 4236	1214.3	127.42	47.13	88	26.0	0.33	0.33	9.22	2.	177	2	112.23	12.4	8.93	9.93	3.5	10.0	
	6945	47.35	11.35			1.00	0.74	0.75	163.	30	1.39	4.29		-16.84	8.47			7306 12-12-004 2
1214-11	1214.6	285.74	125.41	10	1.7	0.50	0.50	0.43	1278.	115	6	1.44	5.5	-16.84	9.27	9.3	0.35	UGCA 277, DDO 118
	-1125	50.30	-12.10			1.01	62.		1098.	86	1	0.42			8.24			-12-31-028 2
U 7307	1214.6	276.04	104.22	10	3.1	1.00	1.00		1188.	86	1	1.44	9.7					7307 02-31-000
	1017	71.06	-6.25			1.00			1091.	10	1.05	0.30	V		8.24			
N 4242	1214.9	140.82	70.30	8X	7.6	0.95	0.95	11.59	516.	142	1	11.46	12.5	9.08				
	4554	70.31	4.77			1.00	19.	0.01	580.	10	1.26	1.00		-17.23	8.59			7323 08-22-098 2
U 7321	1215.0	241.82	92.28	6	7.4	0.14	0.14	12.77	403.	234	2	9.49	7.8	8.20	9.93	1.5		
	2249	81.04	2.56			1.00	90.	1.08	362.	10	1.03	1.18		-15.02	8.09			7321 04-29-060
N 4244	1215.0	154.56	77.76	6A	18.0	0.16	0.16	9.42	247.	220	4	98.77	14.5	9.31	10.15	5.3		
	3805	77.16	2.39			1.00	90.	1.08	276.	5	1.18	4.39		-17.79	8.68			7322 06-27-045 2
U 7332	1215.4	284.80	113.53	10	3.5	0.68	0.68	13.91	941.	100	1	6.10	8.2	8.44	9.47	13.4	10.8	
	43	62.13	-8.79			1.00	48.	0.19	805.	15	1.04	0.66		-15.62	8.60			7332 00-31-045
U 7352	1216.5	278.69	105.47	8	3.3	0.57	0.57	13.84	2464.	205	6	2.86	10.3	8.71	10.10	12.7	24.0	IC 776
	908	70.19	-6.14			1.00	57.	0.24	2363.	40	1.06	0.77	V	-16.31	9.20			7352 02-31-088
N 4258	1216.5	138.31	68.77	4X	24.0	0.40	0.40	8.45	449.	440	4	119.51	36.5	10.25	11.21	2.0	9.3	
	4735	68.84	5.53			1.00	69.	0.50	521.	7	1.36	9.50		-20.13	9.51			7353 08-22-104 2
N 4288	1218.2	138.53	69.82	7B	4.4	0.64	0.64	12.81	534.	230	1	9.08	7.7	8.63	10.13	2.4	31.7	DDO 119
	4635	5.52	-15.29			1.00	52.	0.17	602.	15	1.07	1.00		-16.09	8.52			7399 08-23-006 2
U 7408	1218.8	138.73	70.31	10A	4.0	0.63	0.63	13.55	464.	59	1	2.53	6.2	8.22	8.84	10.3	4.2	DDO 120
	4606	70.37	5.47			1.00	52.	0.18	530.	10	1.05	0.34		-15.07	7.85			7408 08-23-013 2
N 4299	1219.2	277.44	103.12	7B	2.7	1.00	1.00	12.88	238.	86	6	4.24	8.4	9.10			0.43	7408 08-23-013 2
	1147	72.89	-4.73			1.00		-0.01	150.	15	1.06	0.72	V	-17.27	6.98			7408 08-23-013 2
N 4304	1219.6	295.58	147.68	3B	3.8	1.00	1.00	12.43	2631.	260	2	8.04	26.6	9.98	9.66		0.48	7414 02-32-010 2
	-3315	28.95	-15.29			1.05	64.	0.32	2395.	15	1.02	1.21		-19.47	10.07			7414 02-32-010 2
N 4331	1220.3	125.21	40.34	10 P	3.4	0.34	0.34	13.77	1570.	176	6	2.73	17.5	9.17	8.93	7.1	8.0	5-29-034 2
1220-13	1220.6	292.58	127.97	10	2.0	0.92	0.92	0.76	1756.	15	1.05	0.80		-17.45	8.93		0.57	7449 13-09-026
	-1339	48.38	-11.21			1.01	24.	0.15	974.	15	1.03	0.40			8.06			UGCA 278
1221-34	1221.0	296.46	148.85	5A	4.7	0.47	0.47	11.67	2724.	395	2	7.19	33.8	10.32	11.12	3.4	6.4	-2-32-000
	-3421	27.90	-15.17			1.06	64.	0.71	2487.	30	1.02	1.53		-20.31	9.65			IC 3253
N 4359	1221.6	174.89	84.16	5B	5.2	0.34	0.34	12.50	1253.	220	6	5.26	19.1	9.39	10.31	4.1	8.2	6-27-021 2
1221+00	1221.7	288.02	113.85	10	2.0	0.82	0.82	0.68	1256.	10	1.11	0.98		-18.00	8.92		0.34	7483 05-29-079 2
	50	62.64	-7.25			1.00	36.	0.11	1928.	88	1	1.72	11.3		9.71	12.4		DDO 121
U 7490	1222.1	126.24	46.43	9A	5.6	1.00	1.00	12.89	470.	83	1	4.36	10.4	8.64				00-32-004 2
	7037	46.62	12.20			1.00		0.03	636.	8	1.15	0.56		-16.13	8.25		0.40	DDO 122
N 4389	1223.1	136.74	70.65	6BP	3.9	0.72	0.72	12.37	718.	220	6	1.80	8.9	9.03	10.24	0.6	16.1	7490 12-12-008 2
	4558	70.74	6.15			1.00	45.	0.11	786.	40	1.09	0.55		-17.11	8.05		0.10	7514 08-23-028 2
U 7513	1223.2	284.74	107.52	5	5.0	0.19	0.19	13.11	1001.	292	1	6.29	15.6	9.01	10.43	1.9	26.4	IC 3322A
	730	65.18	-5.03			1.00	90.	1.10	898.	10	1.06	1.26	V	-17.04	8.71		0.50	7513 01-32-054 2
U 7512	1223.2	288.01	112.41	10	1.9	0.42	0.42	14.77	1503.	95	1	2.98	7.7	8.56	9.21	34.9	4.4	
	226	64.28	-6.45			1.00	68.	0.50	1379.	20	1.01	0.46		-15.93	8.75		1.56	7512 00-32-008
N 4393	1223.3	207.16	88.06	7X	5.0	0.87	0.87	12.50	755.	137	1	8.79	10.8	8.93	10.21	3.0	19.0	IC 3323
	2750	84.29	0.95			1.00	30.	0.04	741.	8	1.11	0.83		-16.85	8.68		0.57	7521 05-29-083 2
N 4395	1223.4	162.05	82.35	9A	15.0	0.73	0.73	10.59	318.	135	2	78.66	14.6	9.00	10.04	7.9	11.0	7521 05-29-083 2
	3349	81.55	2.73			1.00	44.	0.11	332.	5	1.20	3.50		-17.02	8.94		0.87	7524 06-27-053 2
U 7534	1223.8	129.29	58.35	10B	5.0	0.61	0.61	13.84	724.	86	1	7.56	12.3	8.51	9.45	19.2	8.7	DDO 123
	5835	58.51	9.58			1.00	54.	0.19	845.	10	1.08	0.63		-15.79	8.73		1.67	7534 10-18-045 2
N 4411	1224.0	283.51	105.99	7X	3.3	1.00	1.00	13.55	1282.				10.3	8.83				NGC 4411A
	909	70.82	-4.37			1.00		10.82	1180.	418	1	1.05		-16.60	10.97		24.2	7537 02-32-048 2
N 4414	1224.0	174.50	84.60	5A	6.6	0.70	0.70	10.82	720.	20	1.16	1.72	13.9	9.58	10.97	0.9	0.21	7539 05-29-085 2
	3130	83.19	2.17			1.00	47.	0.13	723.					-18.47	8.90			

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	b	SGL	T	d_H^b	f_a	i	r_H	$B_T^{b,i}$	V	σ	W_{20}	tel.	f_H	F_c	A_H^b	flag	$M_B^{b,i}$	log L	log M_T	log M_H	$\%M_H/M_T$	M_T/L	Alternate Names
(1)	(2)	(3)	(3)	(4)	(4)	(5)	(6)	(6)	(7)	(7)	(8)	(9)	(10)	(10)	(11)	(12)	(12)	(13)	(13)	(14)	(15)	(15)	(16)	(17)	(18)	
U 7547	1224.3	281.37	103.42	10	103.42	10	2.6	0.72	0.72	14.99	1100.	87	1	1.02	4.63	8.1	8.25	9.39	13.8	IC 3356, KAR 130						
	1151	73.41	-3.52				1.00	45.	0.11	0.11	1016.	10	1	1.06	0.57	11.2	-15.16	8.68	2.69	7547 02-32-000						
U 7546	1224.3	284.12	106.01	7A	106.01	7A	3.6	1.00	13.02	13.02	1265.						9.04			NGC 44118						
	909	70.84	-4.30				1.00				1170.						-17.13			7546 02-32-055 2						
N 4423	1224.6	286.64	108.92	9	108.92	9	3.4	0.23	13.12	13.12	1092.	187	6	1.05	3.83	9.8	8.93	9.84	8.2	7556 01-32-065						
	609	67.57	-5.08				1.00	83.	1.10	0.83	984.	25	1	1.05	1.22	4.6	-16.84	8.57	0.44							
U 7559	1224.6	148.62	78.97	108	78.97	108	6.2	0.70	13.25	13.25	222.	76	1	1.14	5.83	4.6	7.70	9.00	20.2	DDO 126						
	3725	78.74	4.01				1.00	47.	0.13	0.13	252.	8	1	1.04	0.54	10.3	-13.76	7.57	0.74	7559 06-27-055 2						
U 7563	1224.6	275.01	99.29	10	99.29	10	3.3	0.61	13.96	13.96	2336.	131	1	1.04	1.66	9.8	8.67	9.74	11.8	IC 3365						
	1611	77.44	-2.19				1.00	54.	0.19	0.19	2271.	10	1	1.04	0.38	14.7	-16.19	8.93	1.83	7563 03-32-041						
U 7557	1224.7	285.72	107.59	9	107.59	9	4.7	0.83	13.17	13.17	935.	164	1	1.09	0.85	4.6	7.87	10.59	25.6	7557 01-32-066						
	732	69.32	-4.66				1.00	35.	0.07	0.07	833.	10	1	1.05	0.43	2.8	-13.22	7.40	0.84	7599 06-27-057 2						
U 7577	1225.2	137.79	72.88	10	72.88	10	6.2	0.70	12.83	12.83	195.	49	4	1.03	0.48	4.6	7.87	8.62	5.7	DDO 125						
	4346	72.95	5.90				1.00	47.	0.13	0.13	254.	5	2	1.01	1.51	21.7	-14.20	7.57	0.50	7577 07-26-006 2						
N 4444	1225.9	298.52	157.85	3	157.85	3	2.8	1.00	0.54	0.54	2666.	30	1	1.01	1.51	2.8	7.48	9.60	18.9	DDO 127						
	4259	19.42	-15.42				1.16		14.25	14.25	280.	86	6	1.05	0.43	2.8	-13.22	7.40	0.84	7599 06-27-057 2						
U 7599	1226.0	147.15	78.97	9	78.97	9	3.1	0.54	14.25	14.25	280.	86	6	1.05	0.43	2.8	7.48	9.60	18.9	DDO 127						
	3730	78.80	4.30				1.00	59.	0.27	0.27	312.	10	1	1.05	0.43	2.8	-13.22	7.40	0.84	7599 06-27-057 2						
U 7605	1226.2	150.96	80.42	10	80.42	10	2.6	0.72	14.83	14.83	304.	47	6	1.04	0.31	2.5	7.30	8.35	11.3	7605 06-27-058						
	3600	80.13	3.91				1.00	45.	0.11	0.11	329.	10	1	1.04	0.31	2.5	-12.76	7.27	0.93	7605 06-27-058						
N 4455	1226.2	251.59	92.78	7	92.78	7	4.0	0.43	12.51	12.51	644.	157	1	1.05	0.79	7.1	8.76	9.62	7.3	7603 04-30-001 2						
	2306	83.29	0.18				1.00	61.	0.44	0.44	611.	10	1	1.05	0.85	7.1	-16.42	8.46	0.51	7603 04-30-001 2						
U 7608	1226.3	137.42	73.19	10	73.19	10	5.6	0.89	13.07	13.07	543.	74	1	1.04	0.57	9.8	8.52	10.42	4.0	DDO 129						
	4330	73.26	6.02				1.00	60.	0.03	0.03	601.	8	1	1.24	0.57	9.8	-15.82	8.39	0.74	7608 07-26-010 2						
U 7612	1226.5	289.60	112.09	98	112.09	98	3.4	0.55	13.97	13.97	1571.	193	1	1.04	0.81	14.4	8.93	10.17	17.6	DDO 128						
	300	65.01	-5.50				1.00	58.	0.29	0.29	1452.	15	1	1.04	0.81	14.4	-16.84	8.99	1.14	7612 01-32-077 2						
U 7639	1227.5	135.19	69.08	10	69.08	10	5.2	0.52	13.50	13.50	384.	50	1	1.08	0.71	7.0	8.12	8.67	3.5	7612 01-32-077 2						
	4748	69.17	7.37				1.00	61.	0.29	0.29	462.	10	1	1.08	0.71	7.0	-14.83	7.18	0.12	7639 08-23-043						
N 4490	1228.3	137.91	74.83	78P	74.83	78P	8.9	0.53	9.92	9.92	577.	245	1	1.24	0.57	16.3	9.82	10.42	4.0	ARP 269, VV 30, TURN 698						
	4155	74.88	5.94				1.00	60.	0.28	0.28	629.	10	1	1.24	0.57	16.3	-19.07	9.52	0.51	7651 07-26-014 2						
N 4487	1228.4	294.20	122.70	6X	122.70	6X	5.8	0.75	11.30	11.30	1037.	235	1	1.13	0.94	15.0	9.56	10.56	10.1							
	748	54.45	-7.92				1.00	42.	0.19	0.19	878.	30	1	1.13	1.22	15.0	-18.42	8.85	0.19	-1-32-021 2						
N 4496	1229.1	290.57	111.11	98	111.11	98	5.2	1.00	11.62	11.62	1738.	179	1	1.075	1.04	24.7	9.97	9.97	0.19	VV 76						
	412	66.32	-6.54				1.00		0.03	0.03	1625.	10	1	1.13	1.04	24.7	-19.43	9.45	0.30	7668 01-32-090 2						
N 4498	1229.1	277.86	98.69	78	98.69	78	5.0	0.53	12.21	12.21	1506.	190	1	1.08	0.50	15.6	9.37	10.18	0.30	7668 01-32-090 2						
	1708	77.75	-0.89				1.00		0.28	0.28	1448.	20	1	1.08	0.50	15.6	-17.94	8.78	0.26	7669 03-32-056 2						
N 4501	1229.4	282.27	101.04	3A	101.04	3A	9.4	0.59	10.05	10.05	2285.	542	1	1.28	0.79	29.4	10.23	11.41	15.1	M 88						
	1442	76.51	-1.51				1.00	56.	0.21	0.21	2217.	15	1	1.28	0.79	29.4	-20.10	9.64	0.25	7675 03-32-059 2						
U 7673	1229.5	180.54	86.38	10	86.38	10	3.1	0.82	12.98	12.98	639.	73	1	1.04	0.40	5.8	9.26	9.26	0.25	DDO 131						
	3000	84.99	2.87				1.00	36.	0.06	0.06	639.	10	1	1.04	0.40	5.8	-15.90	8.23	0.48	7690 07-26-021						
N 4504	1229.7	294.64	122.28	6A	122.28	6A	5.1	0.71	11.48	11.48	1003.	250	1	1.09	2.02	12.6	9.46	10.49	10.8	7673 05-30-014 2						
	717	55.00	-7.47				1.00	46.	0.21	0.21	847.	8	1	1.09	2.02	12.6	-18.16	9.20	0.56	-1-32-022 2						
U 7685	1229.9	292.49	114.61	8B	114.61	8B	5.4	0.91	12.58	12.58	1532.	177	1	1.13	1.10	22.2	9.46	9.34	0.76	NGC 4517A, REINHUTH 80						
	38	62.84	-5.33				1.00	23.	0.07	0.07	1405.	10	1	1.13	1.10	22.2	-18.16	9.34	0.76	7685 00-32-019 2						
U 7690	1230.0	135.65	73.88	10	73.88	10	3.5	0.80	12.98	12.98	540.	103	1	1.05	0.59	6.1	8.55	9.54	9.8	7690 07-26-021						
	4259	73.95	6.53				1.00	38.	0.07	0.07	598.	10	1	1.05	0.59	6.1	-15.90	8.23	0.48	7690 07-26-021						
N 4517	1230.2	292.74	114.87	6A	114.87	6A	12.7	0.28	10.10	10.10	1131.	317	4	1.10	3.09	37.2	10.16	10.90	5.5	7699 06-28-008 2						
	23	62.61	-5.32				1.00	79.	0.98	0.98	1004.	7	1	1.10	3.09	37.2	-19.91	9.49	0.21	7694 00-32-020 2						
U 7698	1230.4	164.34	84.69	10	84.69	10	9.1	0.74	13.28	13.28	335.	83	2	1.04	1.04	9.1	7.95	9.43	30.1	DDO 133						
	3149	84.01	3.57				1.00	43.	0.10	0.10	543.	7	1	1.07	0.76	9.1	-14.40	8.08	1.34	DDO 133						
U 7699	1230.4	142.22	78.82	5B	78.82	5B	5.6	0.34	12.18	12.18	503.	209	1	1.08	0.96	8.8	8.78	9.93	13.9	7698 05-30-016 2						
	3754	78.80	5.24				1.00	14.	0.68	0.68	539.	10	1	1.08	0.96	8.8	-16.48	8.27	0.31	7699 06-28-008 2						
1230-04	1230.9	294.54	119.75	8	119.75	8	3.9	0.23	10.10	10.10	1131.	317	4	1.10	3.09	37.2	10.16	10.90	5.5	7699 06-28-008 2						
	436	57.70	-6.49				1.00	83.	1.15	1.15	1151.	20	1	1.04	0.73	13.1	-16.27	7.23	7.6	UGCA 286						
N 4522	1231.1	288.93	106.21	4	106.21	4	5.9	0.33	12.25	12.25	2331.	316	6	1.14	1.62	18.4	9.35	10.60	17.9	-1-32-023						
	926	71.54	-2.61				1.00	74.	0.73	0.73	2241.	30	1	1.14	1.62	18.4	-17.90	8.91	0.36							

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	d_H^b	r_H	B_p^i	V	W_{20}	tel.	F_C	flag	A_p^b	$\log L$	$\log M_H$	$\log M_T$	% M_H/M_T	M_T/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)
U 7719	1231.5	138.52	77.54	8	3.0	0.38	14.46	686.	89	1	1.02	2.23	6.4	8.13	9.06	10.3	8.4	7719 07-26-025		
	3917	77.57	5.82		1.00	71.	0.55	728.	10			0.45		-14.85	8.07		0.88			
N 4534	1231.7	145.57	80.92	8	6.2	0.76	12.16	803.	143	1	1.15	15.51	15.0	9.17	10.15	7.8	9.6	7723 06-28-010 2		
	3548	80.83	4.92		1.00	42.	0.09	830.	8			1.07		-17.44	9.04		0.74			
N 4532	1231.8	291.04	108.84	108	4.0	0.65	12.14	2010.	251	2	1.09	15.19	12.5	9.39	10.42	21.0	10.7	7726 01-32-103 2		
	645	68.95	-3.19		1.00	51.	0.18	1509.	20	1	1.01	22.55	30.9	-18.01	9.74		2.25			
N 4535	1231.8	290.08	107.19	5X	9.9	0.50	10.62	1966.	291	1	1.43	1.25	V	19.53	9.90		0.79	7727 01-32-104 2		
	828	70.63	-2.71		1.00	26.	0.04	1873.	8					-10.00						
U 7739	1232.2	291.40	109.05	10	2.5	1.00	14.71	2032.		1			14.1	8.88				A 1232 HOLMBERG VII, DDO 137		
	634	68.79	-3.15		1.00		0.02	1931.		1	1.03	2.49	6.2	-16.72	9.65	2.0		7739 01-32-107 2		
U 7737	1232.3	284.11	100.47	10	2.0	0.55	0.25	661.	160	1		0.62	V	10.12	7.95			IC 3522, DDO 136		
	1930	77.48	-0.62		1.00	58.	12.46	598.	20	1	1.01	5.14	35.9	-19.47	10.97	4.5	7.0	7737 03-32-072 2		
N 4545	1232.3	126.10	53.45	68	4.3	0.59	0.21	2716.	295	1	1.06	1.16		-19.82	9.62		0.32	7747 11-15-064 2		
	6348	53.50	11.75		1.00	56.		2860.	10											
1233-07	1233.0	296.12	122.82	9	6.0	0.49	13.19	993.	182	1	1.11	5.71	14.8	8.43	10.09	3.2		UGCA 289		
	-737	54.77	-6.77		1.00	63.	0.42	838.	15	1		0.96		-15.60	8.60			-1-32-028		
N 4559	1233.5	198.44	88.32	6X	11.6	0.57	10.07	816.	255	4		68.42	27.4	9.98	10.71	8.8	5.4	7766 05-30-030 2		
	2814	86.47	3.22		1.00	57.	0.23	810.	10	1	1.10	3.51		-19.47	9.65		0.47			
N 4565	1233.8	230.88	90.25	3A	20.0	0.18	9.22	1228.	524	1	1.76		70.8	10.67	11.59		8.3	7772 04-30-006 2		
	2615	86.42	2.74		1.00	90.	0.17	1213.	15					-21.20						
U 7774	1233.9	135.65	76.69	7	5.3	0.21	13.19	526.	203	6		6.02	8.9	8.43	9.87	2.7	27.4	7774 07-26-031		
	4017	76.74	6.53		1.00	86.	13.18	574.	10	1	1.11	0.74	12.6	8.90	8.30		0.74			
U 7781	1234.1	292.54	108.86	9	4.4	1.00	0.01	1076.	67	1	1.09	0.52	V	-16.77	8.67		0.58	IC 3576, DDO 138		
	654	69.20	-2.60		1.00		13.68	978.	10			1.91	11.9	8.78	10.00	2.1	16.6	7781 01-32-112 2		
U 7784	1234.2	288.28	102.49	108	3.8	0.64	0.17	1125.	160	6	1.08	0.54	V	-16.47	8.33		0.35	IC 3583		
	1332	75.71	-0.73		1.00	52.		1055.	15									7784 02-32-154 2		
N 4571	1234.4	287.53	101.59	6A	5.4	0.96	11.83	348.	199	1	1.14	2.82	16.9	9.52	7.35		0.01	7788 02-32-156 2		
	1429	76.64	-0.42		1.00	17.		282.	25	1		0.76	V	-18.32	8.25			CWNI DW A		
1236+33	1236.3	148.24	83.87	10	1.7	0.73	0.11	312.	51	1	1.01	3.21	1.6		7.54	19.6				
N 4592	1236.7	330.1	5.09	8A	6.9	0.36	11.30	326.	7			35.45	19.2	9.63	10.27	17.3	4.3	06-28-000		
	-16	62.18	-3.94		1.00	72.	0.67	954.	208	1	1.13	2.43		-18.60	9.51		0.76	7819 00-32-032 2		
U 7822	1236.9	293.95	107.77	10	2.0	0.62	14.34	2086.	187	1	1.76	1.76	6.2	8.51	9.84	10.1	21.0	IC 3617, DDO 140, KAR 173?		
	814	70.62	-1.56		1.00	53.	0.20	1995.	40	1	1.01	0.35	V	-15.81	8.85			7822 01-32-127 2		
N 4597	1237.5	297.75	121.09	98	5.1	0.50	11.99	1049.	171	1	1.18	11.81	13.5	9.31	10.01	9.4	5.0			
	-532	56.95	-5.15		1.00	62.	0.40	904.	8			1.22	7.4	-17.79	8.98		0.47	-1-32-034 2		
N 4605	1237.8	125.33	55.50	58P	9.1	0.41	10.49	140.	199	1	1.08	12.84		8.89	9.84	1.4	8.9			
	6153	55.47	12.00		1.00	69.	0.48	279.	30	1	1.22	2.50		-16.74	8.00		0.13	7831 10-18-074 2		
N 4602	1238.0	297.88	120.47	4X	4.5	0.39	11.58	2559.	422	1	2.88	31.9		10.33	11.11	1.3	6.1			
	-452	57.62	-4.85		1.00	70.	0.60	2417.	50	1	1.06	1.70	33.3	-20.34	9.23		0.08	-1-32-036 2		
N 4603	1238.3	300.82	155.88	5A	4.9	0.65	11.36	2562.	495	2	8.55	3.21		10.38	11.44	1.7	11.4			
	-4042	21.86	-12.80		1.12	51.	0.64	2323.	60	1	1.02	1.81		-20.47	9.66		0.19	-7-26-028 2		
N 4618	1239.2	130.53	75.84	98	6.0	0.93	11.26	546.	157	1	20.37	10.5		9.25				ARP 23, VV 73		
	4125	75.84	7.78		1.00	22.	0.01	602.	8	1	1.16	2.50		-17.64	8.87		0.42	7853 07-26-037 2		
N 4625	1239.5	130.22	75.72	9XP	3.5	0.71	12.78	610.	86	6		6.95	6.8	8.73	9.30	15.5	3.7	IC 3675		
	4133	75.72	7.87		1.00	46.	0.12	667.	10	1	1.07	1.24		-16.34	8.49		0.58	7861 07-26-038 2		
U 7866	1239.7	132.10	78.45	10	5.6	0.66	13.18	352.	71	1		5.20	6.5	8.12	9.05	7.3	8.6	IC 3687, DDO 141		
	3846	78.47	7.23		1.00	50.	0.15	396.	8	1	1.11	0.49		-14.81	7.91		0.62	7866 07-26-039 2		
N 4631	1239.8	142.59	84.26	7B	19.0	0.23	8.68	613.	325	4	142.29	35.0		10.32	10.88	7.5	3.6	ARP 281, TURN 768		
	3249	84.23	5.75		1.00	83.	1.08	631.	7	1	1.20	6.26		-20.32	9.75		0.27	7865 06-28-020 2		
U 7872	1240.0	123.75	41.63	10	3.1	0.77	0.16	1887.	98	6		1.75	18.8		9.93	8.8				
	7535	41.80	14.32		1.00	41.	13.30	2073.	15	1	1.06	0.46		8.82	10.29	0.9	29.2	7872 13-09-030		
N 4635	1240.2	286.90	96.46	7A	2.9	0.80	0.07	981.	212	6		1.86	8.0	-16.58	8.22		0.25	7876 03-32-087 2		
	2013	82.54	2.50		1.00	38.	12.17	944.	30	1	1.05	0.60		9.38			0.17			
N 4639	1240.4	294.34	102.91	3X	4.0	0.88	0.03	983.	313	6	1.11	0.61		-17.98	8.60			7884 02-32-189 2		
	1332	75.99	0.72		1.00	29.		917.	20				V							

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	d_H^b	r_H	$B_T^{b,i}$	V	W_{20}	tel.	F_C	A_H^b	flag	$\log L$	$\log M_T$	$\log M_H$	$\%M_H/M_T$	M_T/L	M_H/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)	(22)
N 4651	1241.2	293.08	99.96	5A	6.1	0.74	11.20	800.	403	1	16.08	19.1	9.77	11.12	0.7	22.5	ARP 189, VV 56				
N 4653	1241.3	298.86	116.25	6X	4.4	0.89	12.73	748.	25	1.14	1.79	V	-18.95	8.95	0.15	0.15	7901 03-33-001 2				
N 4654	1241.4	295.41	103.12	6X	7.0	0.70	10.97	2506.	10	1.08	0.93		-19.26	9.55	0.45	0.45	7900 00-33-006 2				
	1323	75.87	0.91		1.00	47.	0.13	978.	10	1.17	1.52	V	-19.18	9.12	0.18	0.18	7902 02-33-004 2				
1241-05	1241.5	299.56	121.22	9	5.1	0.71		1429.	142	1	8.49	19.3		10.18	9.3		DDO 142				
N 4656	1241.6	300.25	84.73	98P	14.5	0.28	9.84	1287.	10	1.09	0.94		9.15	9.32	16.4	2.6	-1-33-001 2				
U 7911	1241.9	299.05	115.31	98	4.3	0.75	13.64	667.	7	1.13	3.66	28.3	9.90	9.53	0.43	0.43	7907 05-30-066 2				
	45	63.29	-2.41		1.00	42.	0.15	1066.	119	1	3.06	13.4	-19.28	8.79	13.6	0.56	DDO 144				
U 7916	1242.1	134.05	82.58	10	3.9	0.79		612.	82	1	5.91	7.3	9.40	9.40	9.6		7911 00-33-007 2				
1242-08	1242.4	300.25	-4.84	10	1.6	0.90	0.07	1378.	126	6	2.40	5.7	8.38	8.38			I Zw 42, VV 127, DDO 143				
1243-05	1243.1	300.32	121.73	10	5.1	0.88	0.12	1479.	148	1	2.92	20.0	8.56	8.56			7916 06-28-024 2				
	-549	56.75	-3.88		1.00	29.	0.12	1337.	20	1.11	0.68		8.72	8.72			UGCA 295				
U 7941	1244.0	123.87	52.64	7	6.5	0.24	12.80	2294.	263	1	4.18	46.4	9.85	10.82	3.8	9.4	DDO 146				
U 7943	1244.2	299.70	110.19	5	3.8	0.82	13.58	837.	133	1	2.22	8.2	-19.14	9.40	1.4	0.35	7941 11-16-006				
U 7949	1244.6	128.39	80.65	10	3.3	0.61	0.09	743.	15	1.06	1.04		-15.78	8.09	0.39	0.39	7943 01-33-007				
	3646	80.59	7.68		1.00	54.	0.19	371.	8	1.04	0.42		7.79	7.79	20.6		DDO 147, KAR 200				
U 7950	1244.6	124.63	65.66	10	2.9	0.75	15.00	510.	104	1	1.93	5.2	7.77	9.40	2.9	42.7	7949 06-28-030 2				
N 4688	1245.3	300.62	111.83	68	6.1	1.00	12.84	991.	70	1	9.14	15.9	-13.93	7.86		1.23	HARO 36				
N 4707	1246.1	124.11	66.19	9	3.8	0.89	13.94	468.	83	1	0.70	6.3	-16.91	8.86		0.80	7950 09-21-047 2				
	5126	65.96	11.13		1.00	28.	0.03	569.	10	1.06	0.49		8.13	8.10		0.92	7961 01-33-013 2				
1246-04	1246.1	301.65	121.12	10	2.9	1.00		1343.	65	1	1.03	10.2	-14.83	8.10			I Zw 43, DDO 150				
N 4700	1246.5	302.02	127.09	78	4.8	0.25	11.22	1206.	10	1.04	0.29		9.90	10.00	10.6	1.3	7971 09-21-050 2				
N 4701	1246.7	301.58	112.83	6A	5.2	0.85	12.69	727.	185	1	13.11	9.5	-19.26	9.03	2.2	44.6	DDO 148, KAR 205				
	340	66.26	-0.47		1.00	33.	0.08	624.	10	1.11	1.22		8.71	10.36		1.00	-1-33-011 2				
1246-09	1246.8	302.11	125.87	98	7.1	0.75	11.88	1318.	161	1	8.70	24.2	-16.29	8.71		1.00	-2-33-013 2				
N 4713	1247.5	302.00	111.03	7X	4.7	0.66	12.02	655.	196	1	14.61	7.7	9.57	10.44	4.3	7.4	A 1247				
1247-10	1247.9	302.56	126.67	8	5.6	0.50	0.18	2407.	285	1	8.95	38.3	-18.45	9.07		0.32	-2-33-015 2				
	-1036	52.00	-3.99		1.01	62.	0.43	2251.	15	1.10	1.35		-16.72	10.90		0.60	7985 01-33-018 2				
N 4725	1248.1	295.56	91.57	2XP	12.1	0.83	9.89	1207.	410	2	23.61	42.4	10.39	11.65	0.8	17.9	DDO 151				
N 4731	1248.4	302.73	122.38	68	8.9	0.49	10.88	1457.	244	6	27.23	35.4	-20.50	9.53		0.14	-2-33-020 2				
N 4736	1248.6	123.31	76.28	2A	15.0	0.89	8.82	307.	232	2	14.13	16.1	-19.79	9.70	9.3	4.2	7989 04-30-022 2				
	4123	76.02	9.49		1.00	28.	0.03	368.	15	1.23	1.66		-19.01	8.28		0.39	M 94				
N 4747	1249.3	305.66	91.38	58P	4.5	0.58	12.79	1189.	197	1	6.21	15.5	9.22	10.25	4.9	0.03	7996 07-26-058 2				
1249-09	1249.8	303.33	125.69	6	3.9	0.18	0.22	2258.	10	1.06	1.46	24.1	-17.57	8.94		10.6	ARP 159				
1250-06	1250.0	303.45	122.39	10	3.2	1.00	1.18	1536.	105	1	0.97	13.1	8.81	8.81		0.52	8005 04-30-023 2				
	-602	56.57	-2.28		1.00		0.08	1398.	10	1.05	0.47		2.77	8.73			UGCA 304				

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	σ_H	b	r_H	B_T^i	V	W_{20}	tel.	F_C	A_H^b	$\log L$	$\log M_T$	$\log M_H$	$\%M_H/M_T$	M_T/L	M_H/L	Alternate Names
(1)	(2)	(3)	(3)	(4)	(5)	(6)	(7)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(18)	
U 8011	1250.0	305.44	95.42	10	2.5	0.82	0.06	770.	143	1	1.91	5.5	9.82	8.03	1.6	9.1	8011 04-30-000				
N 2155	84.51	5.15	5.15	38P	4.4	0.33	12.90	1244.	205	1	2.70	15.4	10.15	8.59	2.7	0.25	8014 03-33-015 2				
N 4758	1250.3	304.60	101.06		1.00	0.74	0.72	1196.	10	6	0.96	6.3	8.20				UGCA 305, KAR 213				
1250-04	1250.8	303.85	121.16	10	1.7	1.00	0.07	1410.	80	6	0.96	6.3	8.20				-1-33-000				
	-442	57.90	-1.73		1.00			1278.	20	1.02	0.31										
1251-11	1251.4	303.93	128.07	10	3.5	0.45	0.51	824.	103	1	6.47	6.8	9.25	8.46	16.1		UGCA 307, DDO 153				
	-1149	50.78	-3.48		1.01	66.	0.51	667.	8	1.04	0.78						-2-33-047 2				
U 8024	1251.6	304.76	90.16	10	3.8	0.89	13.76	378.	103	1	17.48	4.2	8.40				NGC 4789A, DDO 154				
N 4781	1251.8	304.13	126.60	78	5.8	0.45	11.28	1265.	272	1	10.37	19.0	10.53	9.11	3.8	5.7	8024 05-30-120 2				
	-1016	52.33	-2.97		1.01	66.	0.51	1113.	20	1.10	1.44						-2-33-049 2				
N 4790	1252.3	304.34	126.34	58	2.9	0.71	12.35	1354.	255	1	4.64	10.3	10.41		2.6	10.1	UGCA 307, DDO 153				
	-958	52.62	-2.78		1.01	46.	0.23	1204.	20	1.03	1.40						-2-33-056 2				
N 4809	1252.3	304.99	113.91	10 P	2.9	0.39	14.06	945.	173	1	5.21	7.1	8.42	9.69	7.6	18.6	VV313, WITH NGC4810=ARP277				
U 8036	1252.3	308.61	97.95	58	5.6	0.29	12.43	926.	216	1	7.27	14.6	10.16	8.57	4.0	10.9	8034 01-33-023 2				
	1927	82.01	5.04		1.00	78.	0.88	893.	10	1.08	1.04						IC 3881				
U 8041	1252.6	304.98	116.38	78	5.3	0.63	12.21	1330.	202	1	5.10	18.8	10.39	8.76	3.1	8.2	8036 03-33-016				
1252-44	1252.7	303.65	160.65	10	1.00	52.	0.23	1218.	20	1.09	1.40						A 1253				
1252-10	1252.9	304.58	126.51	10	2.2	0.58	0.61	1985.	20	5.10	0.60						8041 00-33-021 2				
	-1006	52.49	-2.67		1.01	56.	0.33	1171.	15	1.02	0.80						UGCA 308				
U 8053	1253.3	305.73	112.67	8X	2.7	0.79	14.04	717.	131	1	3.62	4.9	9.64		3.2	29.9	UGCA 308				
N 4808	1253.3	305.76	112.39	6A	3.9	0.44	12.20	762.	284	1	20.60	7.6	8.16	8.14	6.2	0.97	8053 01-33-027				
1253+34	1253.9	115.36	82.90	10	1.6	0.90	0.45	730.	67	1	1.66	3.6	8.96		1.01		8054 01-33-028 2				
	3455	82.41	9.09		1.00	26.	0.03	766.	10	1.01	0.38						UGCA 309, CVNII DW 8				
N 4826	1254.3	315.75	95.64	2A	12.3	0.67	9.21	414.	311	4	13.29	14.1	10.68		0.4	9.6	M 64				
1254-03	1254.6	305.69	120.64	10	2.7	0.73	0.15	394.	20	1.13	3.50						8062 04-31-001 2				
U 8074	1255.2	306.74	114.07	9	2.6	0.94	0.18	1411.	134	6	0.69	11.1	8.91		9.9	0.04	UGCA 310				
	258	65.52	1.39		1.00	20.	0.05	811.	10	1.05	0.66						-1-33-000				
1255-09	1255.2	305.55	125.95	5	5.2	0.18	1.18	1487.	269	6	5.22	20.5	10.47		3.2		DDO 156				
	-922	53.20	-1.93		1.01	90.	11.08	1341.	15	1.11	0.79						8074 01-33-031 2				
N 4835	1255.3	304.14	161.76	5X	6.2	0.32	11.08	2185.	380	2	11.36	35.2	8.97		3.9	5.1	UGCA 311				
U 8084	1255.8	307.14	114.01	88	2.7	0.89	14.08	2769.	160	1	2.21	21.1	8.91				-1-33-060				
	304	65.61	1.56		1.00	28.	0.07	2670.	30	1.03	0.48						DDO 158				
U 8091	1256.2	310.76	103.01	10	1.9	0.83	14.45	216.	46	3	2.03	0.9	10.47		4.6	17.2	8084 01-33-032 2				
1256-11	1256.5	305.89	128.53	10	1.6	0.60	0.06	165.	7	1.01	0.26						DDO 155, GR 8				
N 4861	1256.7	111.47	82.82	98	6.2	0.43	12.37	847.	116	1	9.57	16.0	8.08		22.5	0.78	8091 02-33-041 2				
	3508	82.09	9.70		1.00	67.	0.44	885.	7	1.11	0.74						UGCA 312				
1257-12	1257.7	306.34	128.72	108	3.1	0.54	0.39	1582.	200	1	4.85	13.0	10.15		7.0		-2-33-000				
	-1204	50.48	-2.06		1.01	59.	0.39	1428.	12	1.03	0.74						IC 3961, ARP 266, MARK 59				
1258-15	1258.1	306.22	132.01	10	2.9	1.00	0.13	1385.	103	6	1.13	10.4	8.23				8098 06-29-003 2				
N 4900	1258.2	308.50	114.46	58	3.8	1.00	12.06	968.	130	1	4.05	9.7	8.49				UGCA 314				
	246	65.27	2.06		1.00		0.04	870.	20	1.07	0.59						DDO 159, KAR 217				
N 4899	1258.3	306.44	130.30	5X	4.1	0.62	12.07	2656.	277	1	5.57	30.2	10.16		4.8	5.0	8116 01-33-035 2				
	-1340	48.87	-2.35		1.01	53.	0.32	2497.	15	1.06	0.91						-2-33-085				
N 4891	1258.3	306.48	129.82	3 P	4.2	0.94	0.32	2546.	236	1	8.02	29.5	10.86			0.24	UGCA 316				
	-1310	49.37	-2.21		1.01	20.	0.14	2389.	10	1.08	1.28						-2-33-089 2				

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	q_H	r_H	B_{I}^{I}	V	W_{20}	tel.	F_c	A_H^b	flag	$\log M_T$	$\%M_H/M_T$	M_T/L	Alternate Names
(1)	(2)	(3)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
1258-04	1258.9	-429	307.66	121.50	10	2.4	0.34	0.76	2981.	160	1	1.14	20.1		10.05	8.2		DDO 160
			58.03	0.27		1.00	74.		2855.	30	1.02	0.49			8.97			-1-33-070 2
1259-16	1259.5	306.59	133.55	10	2.3	1.01	0.74	0.25	738.	49	1	0.83	3.8		8.60	6.8		UGCA 319
			-2.94			1.01	43.	12.83	569.	10	1.02	0.31			7.43			-3-33-027
U 8146	1300.0	120.29	58.88	6	5.4	0.21	0.21	12.83	669.	176	1	0.94	12.7		9.90	6.1	10.7	8146 10-13-015
			58.38			1.00	86.	13.94	805.	10	1.07	0.94			8.69			
U 8153	1300.6	310.33	113.18	6	2.9	1.00	1.00	13.94	2869.	143	1	2.09	23.5		9.50		0.51	8153 01-33-039
			66.70			1.00		0.03	2779.	15	1.04	0.45			9.21			
1300-17	1300.7	306.58	133.80	10 P	9.2	0.23	0.23	1.23	746.	129	1	27.64	15.6		8.73	17.4		UGCA 320, DDO 161
			-2.72			1.01	83.	0.16	578.	7	1.20	2.12			8.97			-3-33-030 2
N 4930	1301.3	305.49	157.20	58	5.7	0.71	0.71	0.61	2591.	277	2	9.59	39.6		11.07	4.5		
			-8.63			1.13	46.	10.89	2364.	15	1.03	1.32			9.73			-7-27-029
N 4939	1301.7	308.13	127.06	4A	8.1	0.45	0.45	0.51	3117.	446	1	14.84	70.7		11.53	3.8	5.6	
			-0.57			1.01	66.	0.11	2973.	10	1.19	2.17			10.78		0.22	-2-33-104 2
N 4942	1301.7	308.50	124.49	6A	2.5	0.80	0.80	0.16	1751.	166	1	2.46	11.9		10.24	3.7		
			55.06			1.00	38.	0.13	1417.	20	1.02	0.54			8.81			-1-33-078 2
1301-03	1301.9	309.29	120.56	9	5.3	0.83	0.83	0.13	1368.	134	1	10.58	19.3		10.34	7.5		UGCA 322, A 1302
			-318			1.00	35.	12.55	2591.	8	1.11	1.01			9.22			08-33-028 2
1302-07	1302.4	308.73	125.00	78	2.2	0.92	0.92	0.11	1449.	103	1	1.94	9.1		8.59			NGC 4948A, DDO 162
			54.57			1.00	24.	0.04	1417.	15	1.02	0.44			8.59			-1-33-080 2
1302-07	1302.5	308.82	124.75	98	2.5	0.46	0.46	0.47	1123.	218	1	3.39	7.2		9.93	3.9		DDO 163
			-737			1.00	65.	11.81	988.	15	1.02	0.87			8.52			-1-33-082 2
N 4947	1302.6	306.14	151.30	38	4.2	0.59	0.59	0.57	2409.	380	2	3.34	26.6		11.06	1.4	8.1	
			-6.94			1.06	56.	12.55	2194.	70	1.01	0.79			9.21		0.11	-6-29-006 2
U 8188	1303.5	107.69	80.37	9	5.1	0.87	0.87	0.04	326.	59	1	16.51	10.1		9.45	8.5	13.5	IC 4182
			79.10			1.00	30.	0.04	380.	7	1.35	0.80			8.32		1.14	8188 06-29-031 2
1303-17	1303.7	307.99	134.09	10	2.5	1.00	1.00	0.15	1463.	115	1	3.66	11.1		8.79			DDO 164
			-2.05			1.01	47.	0.14	1296.	10	1.04	0.66			8.79			-3-33-032 2
1304-28	1304.1	307.02	144.78	78	3.2	0.95	0.95	0.27	2217.	115	2	3.58	18.9		9.16			UGCA 324
			-2817			1.03	19.	0.27	2019.	15	1.01	0.72			9.16			-5-31-035
N 4965	1304.5	307.16	144.45	9A	3.9	0.89	0.89	0.29	2265.	190	2	4.55	23.7		9.29			UGCA 326
			-4.74			1.03	28.	0.06	2068.	15	1.02	0.89			9.29			-5-31-036 2
U 8201	1304.5	120.77	49.65	10	5.3	0.70	0.70	12.54	33.	68	1	6.64	3.1		8.74	4.9	9.0	VII 7M 499, DDO 165
			49.37			1.00	47.	0.14	201.	8	1.10	0.69			7.43		0.44	8201 11-16-010 2
1305-22	1305.1	307.84	139.53	9	4.5	0.74	0.74	0.93	2616.	253	6	4.33	31.9		10.62	6.2		UGCA 327
			-3.18			1.02	82.	1.26	2434.	15	1.08	1.06			9.41			-4-31-035
U 8215	1305.8	114.61	71.10	10	1.7	0.82	0.82	0.06	221.	59	1	1.18	1.6		8.51	3.6		
			70.01			1.00	36.	0.06	314.	10	1.01	0.26			7.07			8215 08-24-048
N 4981	1306.2	310.62	123.95	4X	4.4	0.75	0.75	11.80	1677.	283	1	7.87	20.0		10.85	2.7	9.9	
			-631			1.00	42.	0.18	1549.	15	1.07	1.31			9.28		0.27	-1-34-003 2
1306-24	1306.7	308.15	140.91	10	2.0	0.70	0.70	0.34	2872.	119	6	1.81	16.1		9.94	15.0		UGCA 328
			-3.24			1.02	47.	0.34	2687.	20	1.02	0.60			9.12			-4-31-037
1307-10	1307.2	310.34	127.41	5	5.0	0.69	0.69	0.24	1213.	190	1	3.52	15.8		10.32	1.9		UGCA 330
			52.29			1.01	48.	0.24	1073.	15	1.09	0.88			8.61			-2-34-006
1307-23	1307.3	308.34	140.81	10 P	3.3	0.33	0.33	0.93	2667.		2	2.85	26.6					
			-3.07			1.02	74.	0.93	2763.		1.01	0.70			9.34			-4-31-040
U 8246	1307.7	94.53	83.96	68	4.8	0.31	0.31	13.42	813.	170	1	4.64	12.0		9.87	4.6	15.2	8246 06-29-048 2
			11.77			1.00	76.	0.80	855.	20	1.06	0.72			8.53		0.69	UGCA 331
1308-23	1308.0	308.50	140.50	58	3.5	1.00	1.00	0.20	2855.	188	2	3.71	27.1		9.42			-4-31-041
			-2.81			1.02		0.20	2672.	15	1.01	0.65			9.42			
U 8261	1308.7	97.67	82.66	10	1.7	0.54	0.54	0.27	855.	127	1	2.38	4.5		9.30	9.7		8261 06-29-053
			12.22			1.00	59.	0.27	903.	10	1.01	0.59			8.29			
N 5012	1309.1	351.35	95.23	5X	4.3	0.62	0.62	12.80	2625.	407	1	4.95	32.9		11.23	2.0	21.2	
			9.74			1.00	53.	0.19	2620.	25	1.06	1.70			9.52		0.41	8270 04-31-012 2
1309-11	1309.4	310.86	129.26	68	2.7	0.68	0.68	0.26	2107.	125	1	1.87	15.6		9.94	8.2		UGCA 332
			50.47			1.01	48.	0.26	1963.	15	1.03	0.49			8.86			-2-34-008
1309-06	1309.4	311.57	124.37	88	5.4	0.59	0.59	0.30	1485.	173	1	10.92	21.5		10.28	10.5		UGCA 333
			55.51			1.00	56.	0.30	1359.	8	1.09	1.17			9.30			-1-34-011

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	d_H^b	r_H	B_p^i	V	W_{20}	tel.	F_C	A_H^b	log L	log M_T	% M_H/M_T	M_T/L	Alternate Names
(1)	(2)	(3)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
N 5016	1309.7	1.07	94.11	5X	5X	3.0	0.76	13.64	2613.	247	1	2.70	22.9	9.57	10.81	2.9	17.2	8279 04-31-013 2
U 8280	1309.8	96.91	82.55	5	5	4.0	0.26	12.96	815.	194	1	2.65	10.1	8.88	9.27	2.5	10.4	IC 4213
	3556	80.39	12.47			1.00	80.	1.01	865.	15	1.04	0.52		-16.73	8.30		0.26	8280 06-29-057
U 8285	1310.0	317.97	110.71	9	9	3.1	0.32	14.07	896.	142	1	1.67	7.5	8.40	9.51	3.5	13.1	
	727	69.44	6.13			1.00	75.	0.78	825.	15	1.03	0.46		-15.51	8.06		0.45	8285 01-34-008
N 5023	1310.0	110.36	74.08	5	5	9.6	0.19	11.17	400.	193	1	14.31	13.6	9.09	10.01	3.3	8.2	
	4418	72.58	13.88			1.00	90.	1.08	484.	10	1.21	1.09		-17.25	8.53		0.27	8286 07-27-043 2
U 8290	1310.2	352.27	95.39	9 P	9 P	2.5	0.76	14.45	2604.	190	1	2.12	19.0	9.24	10.50	4.5	18.0	
	2306	83.56	9.96			1.00	42.	0.09	2599.	40	1.02	0.43		-17.62	9.16		0.82	8290 04-31-014
1310-32	1310.2	308.16	149.15	8B	8B	4.6	0.33		2382.	261	2	4.78	29.4		10.64	5.2		UGCA 334
	-3226	29.95	-4.73			1.05	74.	1.03	2178.	15	1.01	1.12			9.36			-5-31-039 2
1310-15	1310.9	310.77	132.59	EA	EA	4.2	0.94		2503.	85	1	3.13	29.1		9.24			UGCA 338
	-1511	47.09	0.17			1.01	20.	0.15	2348.	8	1.08	0.56						-2-34-010
U 8303	1311.0	97.17	82.06	10	10	3.2	0.97	13.60	949.	106	1	3.55	9.4	8.75			0.63	A 1311, HC VIII, DDO 166
	3628	79.81	12.80			1.00	14.		1002.	10	1.05	0.55		-16.40	8.55			8303 06-29-061 2
N 5033	1311.2	97.59	81.68	5A	5A	12.3	0.47	10.24	877.	452	4	42.12	33.4	10.03	11.23	2.1	15.7	
	3651	79.45	12.91			1.00	64.	0.36	931.	10	1.11	3.85		-19.60	9.56		0.34	8307 06-29-062 2
U 8308	1311.2	111.61	71.78	10	10	2.2	0.65		165.	50	1	1.09	1.7		8.15	5.2		DDO 167
	4635	70.32	14.40			1.00	51.	0.16	259.	7	1.02	0.25			8.66			8308 08-24-090 2
U 8313	1311.6	107.48	75.99	5B	5B	2.9	0.34	13.95	621.	127	1	1.30	5.9	8.30		10.5		
	4228	74.25	13.89			1.00	74.	0.68	699.	15	1.02	0.38		-15.27	7.80		0.32	8313 07-27-048 2
1312-22	1312.2	309.92	140.06	10	10	3.4	0.35		1508.	137	2	2.85	13.1		9.74	9.2		UGCA 339
	-2252	39.42	-1.68			1.02	73.	0.85	1330.	20	1.01	0.70			8.70			-4-31-000
U 8320	1312.2	110.80	72.21	10B	10B	6.0	0.45	12.23	198.	68	1	18.07	5.1	8.23		5.7		DDO 168
	4411	70.66	14.52			1.00	68.	0.40	291.	7	1.10	1.05		-15.09	8.18		0.90	8320 08-24-093 2
N 5042	1312.8	308.57	140.94	5X	5X	6.5	0.60		1390.	233	6	11.70	22.4		10.57	4.6		UGCA 340
	-2345	39.53	-1.80			1.02	55.	0.42	1210.	15	1.21	1.94			9.23			-4-31-043 2
U 8331	1313.3	111.50	70.61	10A	10A	4.4	0.39	13.99	258.	74	1	3.57	4.6	7.70	8.76	8.0		DDO 169
	4746	69.09	14.91			1.00	70.	0.53	358.	8	1.05	0.45		-13.78	7.66		0.91	8331 08-24-097 2
U 8333	1313.5	17.15	92.97	10	10	2.2	0.37		941.	132	1	2.13	6.1		9.38	8.0		DDO 170
	2542	84.26	11.26			1.00	72.	0.58	950.	15	1.01	0.58			8.28			8333 04-31-016 2
N 5055	1313.5	106.03	76.23	4A	4A	16.0	0.63	5.12	497.	406	4	87.83	26.9	10.06	11.15	2.1	12.3	M 63
	4217	74.30	14.21			1.00	52.	0.18	575.	5	1.20	4.23		-19.68	9.46		0.25	8334 07-27-054 2
N 5054	1314.4	311.76	133.97	3A	3A	6.9	0.62	10.95	1743.	347	1	7.00	31.9	10.21	11.08	1.5	7.4	UGCA 344
	-1622	45.80	0.65			1.01	53.	0.34	1587.	25	1.16	1.04		-20.05	9.25		0.11	-3-34-039 2
1316-08	1316.0	314.37	126.22	10	10	2.4	0.71		1310.	67	1	1.43	8.3		9.16	13.8		DDO 171
	-811	53.82	3.34			1.01	46.	0.22	1183.	15	1.02	0.32			8.30			-1-34-014 2
N 5068	1316.3	311.51	138.33	6X	6X	10.4	0.94	10.61	679.	113	2	38.25	15.5	9.36			0.43	UGCA 345
	-2047	41.37	-0.18			1.02	20.	0.20	510.	8	1.12	2.02		-17.93	9.00			-3-34-046 2
U 8365	1316.5	104.02	76.40	7B	7B	3.8	0.54	13.99	1215.	195	1	2.22	14.4	8.82	10.25	2.1	27.2	DDO 172
	4212	74.17	14.75			1.00	52.	0.17	1294.	160	1.05	0.55		-16.57	8.57		0.56	8365 07-27-058 2
1317-35	1317.4	309.43	152.81	8	8	4.4	0.34		1455.	162	2	5.85	16.0		9.96	10.0		
	-3548	26.45	-4.22			1.07	74.	1.05	1248.	15	1.01	0.86			8.96			-6-29-028
N 5085	1317.6	311.29	141.64	5A	5A	5.7	0.95	11.67	1958.	254	6	12.17	29.8	10.02			0.37	UGCA 349
	-2409	37.99	-0.86			1.02	15.	0.23	1780.	15	1.24	1.26		-19.58	9.59			-4-32-005 2
U 8385	1318.2	326.02	108.70	9X	9X	3.9	0.48	13.54	1133.	217	1	3.99	12.3	8.84	10.16	3.2	21.0	DDO 173
	1003	71.34	8.75			1.00	64.	0.37	1079.	20	1.04	0.82		-16.63	8.67		0.67	8385 02-34-008 2
N 5101	1319.0	311.14	144.64	0B	0B	7.3	1.00	11.45	1864.	200	2	5.14	35.9	10.06			0.13	UGCA 351
	-2711	34.54	-1.44			1.03		0.25	1679.	10	1.06	0.63		-19.68	9.16			-4-32-008 2
N 5112	1319.6	96.13	79.76	6B	6B	5.6	0.73	11.82	978.	225	1	11.80	17.1	9.50	10.56	3.6	11.3	
	3900	76.76	14.89			1.00	44.	0.11	1046.	10	1.12	1.12		-18.28	9.11		0.41	8403 07-28-003 2
U 8409	1320.6	6.49	95.44	8A	8A	3.9	0.48	14.04	2812.	197	1	1.83	32.1	9.48	10.50	4.6	10.5	
	2334	81.90	12.39			1.00	64.	0.35	2817.	20	1.04	0.70		-18.21	9.16		0.48	8409 04-32-009
1321-24	1321.3	312.30	142.05	10	10	3.0	0.90		2056.	113	2	2.38	16.3		8.93			UGCA 352, DDO 241
	-2422	37.65	-0.12			1.02	26.	0.25	1880.	25	1.01	0.59			10.54			-4-32-000 2
1322-19	1322.0	313.57	137.44	6X	6X	5.1	0.58		1975.	209	6	5.48	26.9		10.54	5.2		UGCA 353
	-1927	42.47	1.49			1.02	56.	0.40	1815.	30	1.13	0.87			9.26			-3-34-069

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	a_H	r_H	B_T^i	V	W_{20}	tel.	F_c	A_H^b	$\log L$	$\log M_T$	$\%M_H/M_T$	M_T/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	
N 5145	1323.0	102.13	75.20	12	3.5	0.80	12.91	1225.	233	1	1.05	3.46	13.4	9.26	10.59	1.5	21.3	8439 07-28-009
U 8441	1323.5	114.21	60.04	10	5.0	0.74	13.28	1519.	131	1	1.09	3.78	24.2	9.32	10.75	5.9	8.5	000 175
1323-21	1323.9	313.57	139.96	10	2.7	0.54	0.10	1661.	104	2	1.04	1.54	9.9	-17.82	9.40	8.5	0.50	8441 10-19-070 2
1323-21	-2157	39.93	1.17		1.02	59.	0.47	1273.	30	1.01	0.47	0.47		8.40	8.40			UGCA 356, DDO 174
1324+38	1324.0	90.59	80.88	10	1.4	0.77	0.08	1170.	170	1	1.01	3.31	5.1	9.84	9.84	7.3		UGCA 357
1324+38	3802	77.08	15.60		1.00	41.	0.08	1237.	20	1.01	0.47	0.47		8.71	8.71			06-30-000
1324-29	1324.2	312.02	147.49	10	3.5	0.50	0.60	1894.	140	6	1.06	3.50	17.6	9.95	9.95	11.5		UGCA 358
U 8449	-2945	32.17	-1.12		1.04	62.	0.46	1705.	15	1.06	0.71	0.71		9.01	9.01			-5-32-000
1324+4	1324.4	100.64	75.73	9	2.3	0.42	0.46	1237.	193	1	1.01	2.16	8.9	9.89	9.89	4.9		8449 07-28-010
1324+4	4302	72.80	16.30		1.00	68.	0.46	1324.	25	1.01	0.65	0.65		8.58	8.58			
1324-37	1324.6	310.69	155.25	7	4.8	0.30	1.26	1443.	215	2	1.01	16.88	17.4	10.23	10.23	15.2		UGCA 357
1324-37	-3755	24.15	-3.45		1.09	77.	1.26	1235.	15	2.01	2.01	9.41		9.41	9.41			06-30-000
1324-41	1324.7	310.18	158.42	10	1.09	77.	0.50	525.	112	2	1.08	16.88		8.05	8.05			UGCA 358
N 5169	-4113	20.89	-4.40		1.09	70.	0.50	311.	10	1.03	0.46	0.46		10.81	10.81	4.1	23.2	-5-32-000
1326.0	1326.0	105.03	71.71	38	3.5	0.39	13.94	2482.	335	1	1.03	3.96	24.9	9.44	10.81			8449 07-28-010
1326.0	4656	69.16	16.96		1.00	70.	0.53	2585.	40	1.03	0.46	0.46		-18.12	9.42	0.96		8465 08-25-004 2
N 5161	1326.3	311.95	150.60	6X	8.0	0.46	11.39	2391.	356	2	1.04	1.86	51.4	10.32	11.20	5.5	7.7	UGCA 359
N 5170	-3256	29.02	-1.63		1.06	65.	0.71	2196.	15	1.04	1.86	1.86		-20.32	9.94	0.42		UGCA 359
U 8489	1327.1	315.65	136.13	3A	10.4	0.19	10.54	1498.	629	1	1.25	20.57	41.1	10.24	11.52	1.1	19.1	-5-32-031 2
U 8489	-1742	43.96	3.16		1.01	90.	1.25	1347.	10	1.25	3.05	3.05		-20.11	9.57	0.21		UGCA 360
1327.6	1327.6	102.75	73.07	8X	3.5	0.37	14.27	1302.	154	1	1.03	3.08	14.3	8.78	9.88	8.0	12.8	-3-34-084 2
4539	4539	70.21	17.13		1.00	72.	0.58	1401.	10	1.03	0.63	0.63		-16.46	8.78	1.00		DDO 176
N 5204	1327.7	113.50	59.44	9A	8.0	0.52	11.47	200.	130	3	1.19	29.43	8.1	8.68	9.56	9.7	7.5	8489 08-25-011 2
N 5194	1327.8	104.83	71.19	4AP	14.2	0.67	8.80	467.	195	4	1.19	1.44	23.7	-16.23	8.55	5.0	0.74	8490 10-19-078 2
N 5205	4727	68.56	17.31		1.00	49.	0.15	573.	10	1.17	3.34	3.34		-19.99	10.50	2.1		M 51, ARP 85, VV 1, TURN 85A
1328.2	1328.2	115.37	55.13	12	5.0	0.61	12.73	1781.	253	1	1.08	0.59	28.3	-19.99	10.50	2.4	11.8	8493 08-25-012 2
6246	6246	54.05	17.89		1.00	54.	0.19	1940.	15	1.08	0.59	0.59		-18.71	9.13	2.0	13.9	8501 11-17-003
U 8507	1328.6	354.77	99.72	13	2.6	0.60	13.89	1020.	163	1	1.02	0.38	7.7	8.65	9.79	2.0	0.27	VV 88
U 8508	1328.8	111.13	63.12	10A	2.7	0.63	14.36	68.	73	1	1.02	0.46	1.6	-16.14	8.09	5.7	0.27	8507 03-34-044
1331-45	1331.7	310.82	162.70	10	6.7	0.33	0.18	829.	158	2	1.03	2.79	12.0	-12.17	7.20	26.0	1.37	I ZW 60
1331-45	-4317	16.67	-4.40		1.24	74.	1.37	612.	8	1.03	0.46	0.46		-12.17	7.20			8508 09-22-075
1331+60	1331.8	113.64	57.35	10	1.6	0.80	0.07	2072.	56	1	0.95	0.95	10.4	9.24	9.24	27.1		FOURCADE-FIGUERO
N 5229	1332.0	103.93	70.50	58	5.3	0.24	12.84	365.	157	1	1.01	6.44	7.4	8.41	9.57	3.9	14.5	-7-28-004
N 5238	1332.7	107.40	66.61	8X	3.1	0.82	13.29	243.	59	1	1.07	0.78	3.3	-15.55	8.16	3.6	0.57	UGCA 363
U 8575	5152	64.19	18.35		1.00	36.	0.06	368.	8	1.04	0.34	0.34		-14.54	7.39			10-19-089
U 8575	1332.3	335.01	110.43	10	3.9	0.26	14.09	1167.	146	1	1.04	3.59	12.8	8.66	9.75	8.0	12.5	8550 08-25-019 2
U 8588	1333.7	100.75	72.60	9	2.3	1.00	14.34	1447.	53	1	1.03	0.26	10.4	-16.16	8.66	0.99		I ZW 64
U 8597	1334.2	100.92	72.31	78	2.9	0.85	14.22	2434.	119	1	1.03	0.56	21.5	-16.61	8.42	10.3	0.57	8565 09-22-082
1334-11	4428	68.45	18.33		1.00	33.	0.05	2540.	15	1.03	0.56	0.56		-17.80	9.34	1.08		8575 02-35-010
1334+11	1334.4	320.27	130.81	7X	3.0	0.86	0.17	2474.	117	1	1.04	2.34	20.8	-16.16	8.66	6.1	1.08	DDC 178
U 8611	-1135	49.49	6.65		1.01	31.	0.17	2349.	15	1.04	0.58	0.58		9.29	9.29			8588 08-25-023 2
U 8614	1334.8	98.78	73.70	7X	2.6	0.94	14.44	2640.	185	1	1.04	2.20	20.8	-16.61	8.42	10.3	0.38	DDO 177
U 8614	4509	70.04	18.35		1.00	20.	0.01	2741.	20	1.03	0.47	0.47		9.31	10.33	2.8	0.85	8597 08-25-025 2
1334+9	1334.9	334.25	111.86	10	5.6	0.54	13.00	1053.	227	1	1.03	0.47	16.4	-17.75	9.22	2.8	0.64	8611 08-25-029
754	754	67.68	12.21		1.00	59.	0.30	1004.	15	1.10	0.39	0.39		-17.01	8.81	0.90	0.64	DDO 178
N 5248	1335.1	335.96	110.65	4X	7.9	0.77	10.69	1156.	291	4	1.06	20.96	25.7	-17.01	8.81	2.5	10.2	8614 01-35-020 2
N 5247	1335.4	318.54	136.67	5A	6.9	0.91	10.91	1360.	160	1	1.21	15.75	24.4	-19.54	9.41	0.25	0.23	8616 02-35-015 2
1335-45	-11738	43.58	5.06		1.01	25.	0.19	1216.	10	1.21	1.42	1.42		-19.51	9.37	0.23		UGCA 368

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	d_H	r_H	B_{H}^{J}	V	W_{20}	tel.	F_C	A_H^b	$\log L$	$\log M_T$	$\%M_H/M_T$	M_T/L	Alternate Names
(1)	(2)	(3)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
1335-09	1335.5	321.56	51.37	128.54	9	3.6	1.00	0.11	1300.	110	1	4.44	12.5		8.79		DDO 180	
	-953			7.55		1.01			1184.	8	1.06	0.62					-2-35-010 2	
N 5254	1336.9	321.32		130.66	5A	4.5	0.59		2315.	346	1	5.87	29.0		11.01	2.7		
	-1114	49.66		7.38		1.01	56.	0.34	2194.	20	1.07	1.51			9.45		-2-35-012 2	
U 8639	1337.0	105.84		66.82	10	2.6	0.77	14.37	1708.	134	1	0.93	13.9	8.97	10.08	2.6	12.7	
	5141	64.09		19.01		1.00	41.	0.08	1854.	15	1.03	0.54		-16.95	8.50	0.34	8639 09-22-089	
N 5253	1337.1	314.86		149.86	108P	6.7	0.51	10.37	417.	100	2	10.48	4.5	8.78	9.08	4.7	2.0	UGCA 369
	-3124	30.09		1.02		1.05	61.	0.62	233.	10	1.03	0.99		-16.46	7.76	0.09	-5-32-069 2	
U 8651	1337.8	89.72		78.10	10	4.4	0.54	13.78	200.	56	3	3.23	3.7	7.60	8.50	8.4	8.0	DDO 181
	4100	73.10		18.58		1.00	59.	0.27	287.	5	1.06	0.31		-13.51	7.43	0.67	8651 07-28-046 2	
U 8658	1338.7	107.93		63.76	4X	3.5	0.74	13.25	2035.	246	1	5.27	22.2	9.57	10.76	4.3	15.7	A1339,HOLMBERG V, SCI 132
	5435	61.34		19.30		1.00	43.	0.10	2172.	10	1.05	0.97		-18.43	9.40	0.67	8658 09-22-091 2	
N 5264	1338.8	315.72		148.34	10	3.0	0.90	0.32	478.	55	2	2.74	2.6				UGCA 370, DDC 242	
	-2940	31.70		1.94		1.04	26.	0.32	300.	8	1.01	0.38			7.39		-5-32-066 2	
U 8683	1340.4	85.50		79.29	10	3.5	1.00	14.29	663.	44	1	1.62	7.6	8.22			DDO 182	
	3955	73.57		18.98		1.00	70.	-0.01	748.	7	1.06	0.31		-15.08	7.96	0.55	8683 07-28-055 2	
N 5290	1343.1	89.32		77.16	48P	5.2	0.32	11.85	2579.	479	1	2.89	40.6	10.31	11.30	1.0	9.9	
	4158	71.72		19.64		1.00	75.	0.76	2673.	30	1.07	1.59		-20.28	9.31	0.10	8700 07-28-061 2	
N 5297	1344.3	93.00		74.89	3X	7.7	0.25	11.13	2404.	422	1	12.25	56.4	10.54	11.32	3.7	6.0	TURN 908
	4407	69.93		19.97		1.00	81.	1.04	2507.	20	1.14	1.64		-20.87	9.89	0.22	8709 07-28-063 2	
U 8716	1344.8	110.97		57.31	13 P	2.0	0.39	0.48	2063.	128	1	1.22	13.0		9.69	12.3		
	6038	55.45		19.93		1.00	70.	12.27	2222.	15	1.01	0.39		8.78			8716 10-20-000	
N 5300	1345.7	335.73		116.23	5A	5.4	0.64	0.22	1179.	232	1	4.13	17.7	9.38	10.50	1.6	12.9	
	412	63.15		13.87		1.00	52.	0.22	1123.	10	1.10	0.99		-17.98	8.72	0.22	8727 01-35-038 2	
1346-35	1346.2	315.81		154.66	10	7.0	0.78	0.48	330.	59	2	7.16	2.9		8.70	2.8		
	-3549	25.36		1.32		1.08	40.	0.48	141.	10	1.05	0.58			7.15		-6-30-025	
U 8733	1346.5	91.24		75.41	58	3.9	0.61	13.41	2345.	215	1	4.62	27.9	9.61	10.60	6.9	9.9	
	4339	70.04		20.35		1.00	54.	0.19	2447.	30	1.05	0.80		-18.53	9.44	0.68	8733 07-28-070	
U 8742	1347.4	80.74		80.21	10	2.6	0.89	0.03	2266.	95	1	1.09	17.9					
	3909	73.10		20.27		1.00	28.	0.03	2352.	15	1.03	0.40		8.78		8.6	8742 07-28-000	
N 5320	1348.2	86.38		77.59	5	5.2	0.54	12.41	2613.	308	1	5.95	41.1	10.09	11.03	4.1	0.35	
	4137	71.33		20.57		1.00	59.	0.27	2709.	15	1.08	1.18		-19.75	9.64		8749 07-28-076 2	
1348+62	1348.5	111.80		54.78	10	1.6	1.00		2132.	48	1	0.68	10.7				UGCA 374	
	6259	53.11		20.15		1.00		-0.01	2299.	10	1.01	0.24			8.55		11-17-000	
U 8760	1348.7	77.78		81.17	10	3.5	0.33	14.30	189.	45	3	2.44	2.8	7.34	8.09	14.8	5.6	DDO 183
	3816	73.45		20.46		1.00	74.	0.72	273.	7	1.03	0.29		-12.88	7.26	0.83	8760 06-30-105 2	
N 5324	1349.4	328.98		126.35	4A	3.9	1.00	12.19	3045.	232	1	6.04	33.8	10.26				
	-548	53.73		11.96		1.01		0.09	2954.	15	1.07	0.81		-20.16	9.72	0.29	-1-35-016 2	
N 5334	1350.4	333.06		121.59	58	6.2	0.80	12.34	1383.	223	1	6.90	23.8	9.49	10.80	1.9	20.6	
	-53	58.10		13.62		1.00	38.	0.15	1311.	15	1.15	1.04		-18.25	9.07	0.38	8790 00-35-024 2	
U 8798	1350.7	90.99		74.95	8	2.6	0.54	0.27	2282.	203	1	2.50	18.1	10.31	10.31	7.0		
	4404	69.23		21.12		1.00	59.	0.27	2388.	20	1.02	0.50		9.15			8798 07-29-006	
N 5350	1351.3	82.79		78.71	48	4.9	0.81	12.14	2316.	293	1	7.11	34.5	10.10	11.22	2.5	13.3	
	4036	71.59		21.10		1.00	37.	0.06	2410.	15	1.10	1.16		-19.77	9.62	0.33	8810 07-29-009 2	
N 5348	1351.7	340.05		115.34	3	5.0	0.25	12.75	1457.	193	1	3.12	20.6	9.39	10.20	3.9	6.5	
	529	72.55		15.64		1.00	81.	1.09	1411.	15	1.06	0.59		-18.00	8.79	0.25	8821 01-35-051 2	
U 8833	1352.7	65.49		83.56	10 P	1.9	0.83	0.05	225.	38	3	1.27	1.7		8.18	7.7		
	3605	73.94		21.09		1.00	35.	0.05	305.	5	1.01	0.23			7.07			
U 8837	1352.9	103.71		64.17	108	6.5	0.42	12.63	141.	102	1	5.78	5.4	8.04	9.12	3.5	11.9	8833 06-31-023
	5405	60.80		21.38		1.00	68.	0.46	283.	8	1.12	0.59		-14.63	7.67	0.42	A1353,HOLMBERG1V, DDC 185	
U 8839	1353.0	3.91		102.61	10	4.8	0.78	13.35	965.	115	1	5.88	13.6	8.83	9.95	6.2	13.3	DDC 184
	1802	72.55		18.74		1.00	40.	0.08	571.	10	1.09	0.68		-16.59	8.74	0.82	8839 03-36-001 2	
N 5452	1354.5	118.87		38.48	7X	3.5	0.80	13.18	2066.	190	1	2.54	23.3	9.63	10.65	2.9	10.6	
	7828	38.41		18.36		1.01	38.	0.17	2262.	15	1.05	0.57		-18.60	9.12	0.31	8867 13-10-014	
N 5375	1354.6	44.76		90.72	28	5.3	0.79	12.18	2391.	302	1	2.39	37.8	10.10	11.25	0.8	14.3	
	2924	75.45		20.85		1.00	39.	0.07	2444.	30	1.11	0.60		-19.76	9.15	0.11	8865 05-33-027 2	

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	d_H	r_H	B_T^i	V	W_{20}	tel.	F_C	A_H	flag	$\log L$	$\log M_T$	$\log M_H$	$\%M_H/M_T$	M_T/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)			
1355-29	1355.1	319.93	149.01	3A	9.5	0.21	10.82	2661.	523	6	1.33	12.51	69.3		10.66	11.59		2.0	8.6	IC 4351, UGCA 376
U 8892	-2904	31.36	5.48		1.04	86.	1.38	2456.	30	1	1.33	2.01	20.5		-21.17	9.89		7.8	0.17	-5-33-034 2
U 8892	1356.0	105.95	60.81	10	3.7	0.77	14.14	1748.	116	1	1.45	2.85	20.5		9.09	10.12		0.84	10.6	8892 10-20-052
U 8894	5715	57.88	21.61		1.00	41.	0.08	1901.	15	1	1.05	0.50	19.3		-17.26	9.01		4.6	0.84	8894 11-17-011
U 8894	1356.4	110.90	53.97	9	3.4	0.67	1771.	144	1	1.04	0.62	0.62	19.3		10.15	10.15				8894 11-17-011
U 8894	6339	52.14	21.00		1.00	49.	0.15	1943.	20	1	1.04	0.62	19.3		8.82	8.82				8894 11-17-011
1357-45	1357.7	315.49	164.16	5B	4.1	0.90	0.73	1502.	155	2	1.02	3.12	15.5		10.66	11.59		2.0	8.6	IC 4351, UGCA 376
U 8892	-4510	15.76	-0.06		1.27	26.	0.73	1300.	20	1	1.02	0.70	15.5		-21.17	9.89		7.8	0.17	-5-33-034 2
1358-30	1358.3	320.34	150.22	7X	4.6	1.00	0.31	2594.	187	2	1.02	5.56	32.8		9.09	10.12		4.6	0.84	8892 10-20-052
N 5398	-3003	30.18	5.75		1.05	50.	0.31	2428.	15	1	1.02	0.69	14.1		-17.26	9.01				8894 11-17-011
N 5398	1358.5	319.44	152.78	8BP	4.6	0.50	12.10	1226.	137	2	1.02	5.99	14.1		9.40	9.52		9.7	2.8	UGCA 379
N 5408	-3249	27.56	4.77		1.06	62.	0.67	1053.	15	1	1.02	0.72	14.1		-18.01	8.82		0.26		-5-33-037 2
N 5408	1400.3	317.15	160.63	10	4.5	0.60	0.75	510.	114	2	1.02	15.23	4.2		9.21	9.21		9.4		-7-29-006 2
N 5408	-4109	19.49	1.92		1.16	55.	0.75	318.	8	1	1.02	1.01	31.0		10.07	8.19				M 101, ARP 26, VV 344
N 5457	1401.5	102.03	63.55	6X	28.0	1.00	-0.01	231.	200	2	1.91	10.22	31.0		-19.68	9.73		0.45		8981 09-23-028 2
1402-24	1402.1	323.39	145.40	6B	3.5	0.88	0.28	2337.	195	6	1.08	8.83	22.5		9.63	9.63				UGCA 383
1402-24	-2436	35.10	8.56		1.03	29.	0.28	2191.	15	1	1.08	1.03	22.5		9.63	9.63				-4-33-040
U 8995	1402.4	349.82	112.40	8X	3.5	0.56	13.81	1233.	164	1	1.04	2.27	12.4		8.83	9.97		3.6	13.8	8995 02-36-031 2
N 5474	903	64.76	19.08		1.00	58.	0.28	1210.	15	1	1.04	0.49	8.9		-16.60	8.52		0.49		VV 344
N 5474	1403.3	100.82	64.33	6AP	7.2	0.94	11.34	277.	68	1	1.24	34.13	8.9		-16.79	8.79		0.75		9013 09-23-032 2
N 5468	5354	60.19	22.92		1.00	20.	0.01	423.	7	1	1.24	1.90	28.4		-10.28	9.77		0.31		UGCA 384
N 5468	1404.0	334.88	126.90	6X	3.5	1.00	11.99	2840.	152	1	1.06	0.92	28.4		-20.22	9.77				-1-36-007 2
N 5468	-513	52.69	15.60		1.01	70.	0.10	2763.	10	1	1.06	0.92	28.4		-20.22	9.77				-1-36-007 2
N 5486	1405.7	101.85	62.74	5 P	2.5	0.64	13.72	1407.	203	1	1.02	3.66	11.4		9.09	10.19		5.7	12.5	9036 09-23-038 2
N 5486	-55	55.77	18.07		1.00	52.	0.17	1559.	20	1	1.02	0.69	28.6		-17.24	8.95		10.7		8995 02-36-031 2
N 5483	1407.4	317.86	162.93	5A	6.2	0.85	11.33	1770.	185	2	1.04	29.54	28.6		-10.06	10.84		0.64		VV 125
U 9057	-4305	17.25	2.36		1.22	33.	0.68	1578.	10	1	1.04	1.83	19.5		-19.66	9.87		14.0		9083 08-26-009
U 9057	1407.6	338.61	124.32	8B	4.4	0.39	13.18	1573.	244	1	1.05	0.70	19.5		-17.72	10.42		5.3	0.74	9057 00-36-023
U 9057	-220	54.75	17.32		1.00	70.	0.62	1510.	15	1	1.05	0.70	19.5		-17.72	10.42				9057 00-36-023
N 5496	1409.0	340.44	123.00	7	6.2	0.25	11.74	1544.	260	1	1.10	13.65	27.0		9.84	10.58		7.9	5.4	9079 00-36-026 2
N 5496	-55	55.77	18.07		1.00	81.	1.13	1488.	145	1	1.10	1.46	10.1		-19.12	9.48		4.3	0.44	VV 125
U 9083	1409.6	94.82	67.99	8	1.7	0.82	14.72	1905.	145	1	1.31	1.31	10.1		-16.83	8.74		0.66		9083 08-26-009
1412-43	1412.0	318.48	163.85	5B	3.6	1.00	0.06	2044.	30	2	1.01	0.40	17.9		-16.83	8.74				IC 4386
1412-43	-4343	16.38	2.86		1.25	1.00	0.66	1691.	10	1	1.02	0.99	20.9		9.37	10.58		2.9	16.0	9119 04-34-008 2
N 5523	1412.6	32.12	95.36	6A	6.5	0.36	12.25	1048.	285	1	1.11	9.24	20.9		-17.95	9.05		0.48		DDO 188
U 9126	2533	71.22	24.38		1.00	72.	0.61	1093.	10	1	1.11	1.27	19.4		9.37	10.58		1.7	14.0	9126 03-36-098 2
U 9126	1413.3	8.79	104.87	10	2.9	0.90	0.04	2277.	92	1	1.28	0.72	71.1		10.55	11.70		0.24		9127 06-31-085 2
N 5529	1413.4	67.82	23.28	5	8.2	0.19	11.47	2878.	590	1	1.16	1.10	71.1		-20.89	9.93				DDO 187
N 5529	3627	70.00	25.27		1.00	90.	1.08	2971.	15	1	1.16	1.10	71.1		-20.89	9.93				9128 04-34-009 2
U 9128	1413.6	25.55	97.86	10	2.9	0.90	14.30	153.	54	3	1.04	3.13	1.7		7.06	7.08		1.05		9128 04-34-009 2
N 5530	2317	70.47	24.33		1.00	26.	0.03	196.	7	2	1.04	0.31	20.2		-12.16	10.69		2.6	7.9	9128 04-34-009 2
N 5530	1415.4	315.28	163.60	4A	6.8	0.57	11.02	1200.	292	2	1.04	12.71	20.2		-19.01	9.12		8.0		9169 02-37-001 2
U 9169	-4309	16.71	3.66		1.24	57.	0.89	1013.	25	1	1.04	6.06	23.1		-17.94	8.99				UGCA 389, DDO 243
U 9169	1417.3	356.68	112.73	10	6.2	0.25	12.58	1281.	161	1	1.10	0.63	16.7		9.62	9.24		0.41		-5-34-009 2
U 9169	936	62.62	22.79		1.00	81.	1.09	1273.	10	1	1.10	0.63	16.7		-18.58	9.24		6.5		9179 10-20-094 2
N 5556	1417.6	325.31	160.88	7X	4.6	1.00	11.88	1384.	181	6	1.17	11.30	16.7		-19.10	9.33		0.31		9201 00-37-001 2
N 5556	-2901	29.73	10.03		1.05	36.	0.31	1236.	10	1	1.17	1.05	11.8		-18.58	9.24		5.5	33.3	DDO 189
N 5585	1418.2	100.99	60.74	7X	8.7	0.66	11.24	303.	162	3	1.26	31.89	11.8		-17.10	10.69		2.5	16.0	9211 08-26-029 2
N 5585	5657	56.48	24.64		1.00	50.	0.15	466.	5	1	1.26	1.48	23.4		-17.10	10.69				9211 08-26-029 2
N 5584	1419.8	345.11	123.05	6X	5.0	0.82	11.92	1641.	229	1	1.10	1.06	23.4		-19.10	9.33		0.31		9201 00-37-001 2
N 5584	-9	54.87	20.88		1.00	36.	0.15	1597.	15	1	1.10	1.06	23.4		-19.10	9.33		5.5	33.3	DDO 189
U 9211	1420.6	84.12	73.18	10	3.8	0.82	14.22	690.	115	1	1.06	5.78	9.1		-18.58	9.24		2.5	16.0	9211 08-26-029 2
N 5608	4536	64.25	26.38		1.00	36.	0.06	819.	159	1	1.06	0.66	10.0		-18.58	9.24		0.39		9219 07-30-009
N 5608	1421.3	76.81	77.18	10 P	4.4	0.61	13.22	662.	159	1	1.06	0.66	10.0		-18.58	9.24				9219 07-30-009
N 5608	4200	66.19	26.73		1.00	54.	0.15	780.	15	1	1.06	0.59	10.0		-18.58	9.24				9219 07-30-009

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	q_H	r_H	B_{p}^{I}	V	W_{20}	tel.	F_c	A_H	$\log L$	$\log M_T$	$\log M_H$	$\log M_T$	$\log M_H$	M_T/L	M_H/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)	(22)
U 9240	1422.8	81.97	74.11	10A	3.1	1.00	13.18	153.	62	3	1.05	5.65	2.5	7.82	7.65	7.65	7.65	7.65	0.68	0.68	I 2M 87, DDC 190 9240 08-26-030 2
U 9242	1423.3	71.36	79.69	6	7.3	0.14	12.95	1440.	205	1	1.12	4.53	33.1	9.39	10.44	10.44	10.44	10.44	11.1	11.1	I 2M 88 9242 07-30-011
U 9249	1424.5	358.15	113.91	7	3.5	0.21	13.65	1366.	175	1	1.03	2.24	13.9	9.00	9.94	9.94	9.94	9.94	8.6	8.6	9249 02-37-000
N 5630	1425.6	74.74	77.72	9	3.8	0.34	12.90	2258.	230	1	1.04	3.01	30.8	9.92	10.55	10.55	10.55	10.55	4.3	4.3	9270 07-30-014
U 9275	1425.9	7.20	108.48	8X	4.2	0.67	13.12	1294.	220	1	1.06	7.53	16.1	9.18	10.44	10.44	10.44	10.44	18.1	18.1	IC 1014 9275 02-37-012
U 9291	1426.6	69.87	80.26	6	4.2	0.58	13.01	2895.	262	1	1.06	1.02	36.9	9.94	10.87	10.87	10.87	10.87	8.4	8.4	9291 07-30-015
U 9310	1427.5	351.78	119.91	88	3.4	0.34	14.18	1853.	160	1	1.03	1.60	18.3	9.04	10.01	10.01	10.01	10.01	9.2	9.2	9310 01-37-000
U 9324	1428.0	80.67	74.10	98	3.5	0.61	14.09	2746.	163	1	1.05	3.23	32.8	9.47	10.43	10.43	10.43	10.43	9.0	9.0	DOO 192 9324 08-26-000 2
N 5660	1428.0	89.56	68.31	5X	4.7	0.89	12.27	2336.	158	1	1.10	0.56	34.1	10.07	9.56	9.56	9.56	9.56	0.31	0.31	9325 08-26-039 2
N 5645	1428.2	357.35	115.64	78	4.7	0.57	12.51	1378.	193	1	1.07	4.29	18.8	9.46	10.50	10.50	10.50	10.50	6.9	6.9	9328 01-37-019 2
1428-43	1428.5	321.58	164.72	5A	3.8	0.86	11.55	1949.	190	2	1.01	5.03	19.7	10.07	10.72	10.72	10.72	10.72	4.6	4.6	IC 4444 -4312 15.79 5.77 1200. 1429.4 321.42 165.49 5X -4355 15.01 5.55 112.97 6X 1430.3 1.92 112.97 6X 1006 60.55 26.02
U 9380	1432.1	354.59	119.13	10	3.3	0.57	14.02	1708.	142	1	1.03	1.50	16.3	9.04	9.98	9.98	9.98	9.98	8.6	8.6	9380 01-37-000
U 9385	1432.8	356.10	118.11	10	2.6	0.94	16.44	1644.	106	1	1.03	0.40	12.4	10.72	8.63	8.63	8.63	8.63	0.13	0.13	9385 01-37-037 DOO 193 9391 10-21-011 2
U 9391	1433.2	101.19	57.46	88	2.9	0.65	14.28	1921.	140	1	1.03	2.15	17.8	9.12	10.07	10.07	10.07	10.07	8.8	8.8	DOO 194 9405 10-21-013 2
U 9405	1433.9	98.72	59.70	10	3.8	0.64	14.29	222.	101	1	1.05	2.67	4.4	9.16	9.16	9.16	9.16	9.16	2.9	2.9	9405 10-21-013 2
N 5690	1435.2	353.12	121.51	5	5.2	0.37	11.82	1750.	310	1	1.07	0.51	26.4	9.94	10.75	10.75	10.75	10.75	6.5	6.5	9416 00-37-019 2
U 9426	1435.8	86.39	69.20	10	3.1	0.54	13.15	2315.	62	1	1.03	1.28	22.3	9.27	9.37	9.37	9.37	9.37	0.21	0.21	9426 08-27-008
N 5688	1436.2	322.23	166.82	5	9.0	0.63	0.99	2806.	445	2	1.07	12.57	69.2	11.64	11.64	11.64	11.64	11.64	2.0	2.0	-7-30-004 DOO 195 -1-37-010 2
1436-08	1436.3	342.78	132.89	10	4.4	0.26	1.16	1761.	113	1	1.05	0.49	30.6	9.76	10.88	10.88	10.88	10.88	13.2	13.2	9431 08-27-011
N 5714	1436.4	82.90	71.44	5	4.4	0.20	12.97	2239.	350	1	1.05	1.27	11.8	8.86	8.86	8.86	8.86	8.86	0.54	0.54	9432 01-37-040
U 9432	1436.6	354.39	120.87	10	2.6	0.94	14.29	1573.	112	1	1.03	0.44	28.1	9.85	9.85	9.85	9.85	9.85	0.65	0.65	9432 01-37-040
N 5701	1436.7	357.46	118.28	08	6.4	1.00	11.72	1505.	140	1	1.20	12.77	28.1	10.16	10.16	10.16	10.16	10.16	0.40	0.40	9436 01-37-042 2
N 5707	1437.2	350.40	124.84	78	4.3	0.65	13.28	1768.	235	1	1.06	5.99	21.9	9.36	10.61	10.61	10.61	10.61	17.8	17.8	9447 00-37-021 2
N 5713	1437.6	351.01	124.40	4XP	4.8	0.78	11.82	1900.	195	1	1.09	12.93	26.3	10.01	10.69	10.69	10.69	10.69	9.2	9.2	9451 00-37-022 2
N 5727	1438.4	55.95	85.92	8X	3.5	0.56	13.67	1451.	191	1	1.04	3.22	16.3	9.13	10.23	10.23	10.23	10.23	4.8	4.8	9465 06-32-083
U 9477	1439.9	100.07	57.29	10	2.0	1.00	0.24	2331.	100	1	1.02	1.01	14.7	8.91	8.91	8.91	8.91	8.91	0.61	0.61	9477 10-21-023
	5930	52.69	26.89					2510.	20			0.34			8.80	8.80	8.80	8.80			

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	a_H^b	r_H	B_T^i	V	W_{20}	tel.	F_C	A_H^b	$\log L$	$\log M_T$	$\log M_H$	$\%M_H/M_T$	M_T/L	M_H/L	Alternate Names	
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)				
J 9483	1440.4	357.95	119.07	12	3.8	0.38	12.92	1633.	317	1	3.86	18.2	9.45	10.61	2.5	14.7	10.61	2.5	14.7	10.61	IC 1048
	506	55.36	27.27		1.00	71.	0.63	1627.	15	1.04	0.90			-18.14	9.01	9.01	0.36	9483	01-37-051 2		
N 5740	1441.9	354.51	122.64	3X	4.8	0.54	12.24	1575.	325	1	7.90	21.9	9.68	10.80	3.0	13.3	9.68	3.0	13.3	10.80	
	154	52.85	26.76		1.00	55.	0.36	1558.	20	1.07	2.53			-18.72	9.28	9.28	0.40	9493	00-38-003 2		
U 9500	1442.9	358.85	125.57	98	4.4	1.00		1698.	37	3	2.28	21.9			8.82			9500	01-38-000 2		
	805	56.86	28.60		1.00		0.06		5	1.09	0.27										
1442-20	1442.9	335.89	145.47	10	5.8	0.32		2360.	218	2	4.82	38.1			10.59	6.3		UGCA	393		
	-2033	34.69	18.81		1.03	75.	1.01		2259.	20	1.02	0.97			9.39					-3-38-005	
1444-17	1444.6	338.46	142.47	5	4.9	0.20		2210.	257	1	11.15	30.4			10.61	12.3		UGCA	394		
	-1715	37.29	20.58		1.03	90.	1.31		2122.	20	1.06	1.58			9.70					-3-38-008	
1446-09	1446.8	344.46	135.47	108P	5.2	0.65		1849.	200	1	5.31	27.1			10.56	4.7		ARP	261, VV 140, DDO 197		
	-957	43.00	23.97		1.01	51.	0.33	1790.	30	1.09	0.74			9.23						-2-38-016 2	
1450-03	1450.0	351.26	128.94	8X	4.2	0.80		1955.	175	1	6.86	23.8			10.59	6.5		UGCA	396		
	-321	47.62	27.06		1.01	38.	0.20		1924.	8	1.07	0.77			9.40					00-38-010	
N 5783	1451.9	88.82	64.74	5X	4.2	0.61	13.04	2330.	260	1	4.78	30.6	9.77	10.81	4.6	10.8	0.51	9586	09-24-050 2		
	5217	56.19	30.37		1.00	54.	0.19		2497.	10	1.06	0.40		-18.95	9.47		0.42				
N 5792	1455.8	355.36	126.83	38	10.3	0.32	11.51	1930.	467	1	16.61	57.4		10.15	11.43	2.2	19.0	9649	12-14-015 2		
	-53	48.43	29.23		1.01	75.	0.88	1914.	20	1.26	1.98			-19.90	9.78		0.43	9631	00-38-012 2		
U 9638	1456.9	97.11	57.03	10	3.1	0.68	14.30	2275.	127	1	2.72	22.3		9.25	10.11	12.8		7.2			
	5904	51.43	29.09		1.00	48.	0.16		2461.	15	1.03	0.53		-17.66	9.22		0.93	9638	10-21-040		
N 5832	1457.6	110.10	43.73	38P	5.3	0.70	12.10	451.	172	1	9.40	10.2		8.99	10.06	3.6	11.7	9649	12-14-015 2		
	7153	42.15	24.27		1.00	47.	0.20		650.	10	1.10	1.06		-17.00	8.61		0.42				
1457-13	1457.7	344.58	140.06	10	3.2	1.00		2788.	89	1	2.55	25.2			9.28			UGCA	397		
	-1321	38.67	25.07		1.02		0.20		2726.	10	1.05	0.53								-2-38-024	
U 9663	1459.7	88.39	63.80	10	2.5	0.88	14.23	2422.	133	1	1.89	18.5		9.33				DDO	198		
	5248	54.92	31.38		1.00	29.	0.04		2594.	15	1.03	0.51		-17.84	9.10	2.8	0.59	9663	09-25-005 2		
N 5861	1506.5	348.51	138.81	5X	4.9	0.59	11.77	1867.	358	1	8.49	26.0		10.00	11.00		9.8				
	-1108	39.06	27.95		1.02	56.	0.41		1821.	20	1.08	1.30		-19.53	9.45		0.28			-2-39-003 2	
N 5879	1508.4	93.25	58.45	4A	6.6	0.41	11.61	775.	283	4	8.86	18.5		10.6	10.54	2.4	10.6	9753	10-22-001 2		
	5712	51.40	31.15		1.00	65.	0.50	962.	15	1.03	1.50			-18.31	8.91		0.25				
U 9760	1509.5	1.87	125.01	7	4.2	0.15	13.41	2016.	163	1	2.61	25.0		9.44	10.12	8.0	4.7				
	152	47.79	33.34		1.01	90.	1.21		2016.	15	1.04	0.68		-18.12	9.03		0.39	9760	00-39-011		
U 9762	1509.7	51.85	87.14	9	1.9	0.92		2275.	146	1	1.41	13.3									
	3250	59.24	36.96		1.00	28.	0.03	2396.	20	1.02	1.16			8.91	10.72	6.0	24.4	9762	06-33-000		
U 9764	1509.8	102.42	50.04	8B	3.9	0.65	14.08	2248.	238	1	5.28	27.9		9.34	10.72		1.45	9764	11-18-029		
	6505	46.30	28.20		1.00	51.	0.21	2448.	10	1.05	0.98			-17.86	9.50						
1510-17	1510.4	344.11	146.13	8B	3.4	0.96		2279.	205	1	3.63	22.1						IC	4536, UGCA 401		
	-1757	33.17	25.77		1.04	17.	0.27		2210.	15	1.05	0.91		9.25						-3-39-002	
N 5894	1510.6	96.51	55.31	98	4.8	0.23	11.96	2485.	463	1	3.90	37.6		11.22	9.45	1.7	9.0	9768	10-22-004		
1510-20	1510.7	49.50	30.37	9	5.4	0.24	1.11	2678.	352	2	7.56	34.9		-20.18	10.95	4.1	0.15	9768	10-22-004		
	-2030	31.10	24.61		1.04	82.	1.36	2199.	20	1.02	2.60			9.56				UGCA	402		
U 9769	1510.7	91.35	59.66	8A	4.4	0.79	14.19	844.	208	1	5.35	13.2		8.54	10.47	1.9	84.9	NGC	58668		
	5559	51.83	31.88		1.00	39.	0.09	1029.	30	1.08	0.75			-15.87	8.75		1.63	9769	09-25-034 2		
1511-15	1511.0	346.24	143.57	7A	5.3	0.82	11.88	2287.	169	1	6.42	34.2		10.14	10.76	5.5	4.2	A	1511, FATH 703		
	-1518	35.15	27.13		1.03	36.	0.30	2229.	20	1.11	0.93			-19.86	9.50		0.23			-2-39-007 2	
U 9776	1511.7	92.80	58.30	10	1.7	0.54		830.	75	1	0.99	5.1			8.89	13.2		9776	10-22-005		
	5710	51.05	31.58		1.00	59.	0.29	1018.	10	1.01	0.40			8.01							
N 5885	1512.4	350.98	138.19	5X	6.6	0.82	11.94	2005.	214	1	10.77	38.2		10.00	11.02	4.0	10.2				
	-953	39.05	29.79		1.02	36.	0.26	1968.	491	4	62.39	39.2		-15.53	9.62		0.42			-2-39-013 2	
N 5907	1514.6	91.59	58.84	5A	15.7	0.13	0.90	854.	7	1.14	5.64			10.10	11.27	2.4	15.0	9801	09-25-040 2		
	5631	51.08	32.19		1.00	90.	1.10	1334.	178	2	4.67	16.1		-19.76	9.66		0.36				
1516-41	1516.0	330.65	167.62	3B	4.6	0.90	1.10	1334.	178	2	4.67	16.1									
	-4103	13.55	14.37		1.40	26.	0.85	1191.	25	1.02	0.85			8.80						-7-31-011	
U 9837	1522.6	92.93	56.46	5X	3.1	0.91	13.55	2661.	178	1	2.17	25.9		9.68	9.25	3.4	0.37	SCI	149		
	5814	49.25	32.50		1.00	25.	0.06	2857.	15	1.04	0.49			-18.73	10.85		0.37	9837	10-22-013 2		
1523-22	1523.2	343.86	151.80	4X	4.5	0.61		2325.	277	2	4.67	29.3			9.37			UGCA	408		
	-2206	28.05	26.32		1.06	54.	0.54	2251.	30	1.02	1.16									-4-36-014	

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	q_H	r_H	B_T^i	V	W_{20}	tel.	F_c	A_H^b	$\log L$	$\log M_T$	$\%M_H/M_T$	M_T/L	Alternate Names
(1)	(2)	(3)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
U 9857	1524.7 4155	67.94 55.22	75.20 38.38	108	3.0 1.00	0.38 71.	0.57	2332. 2491.	140 20	1.02	1.15 0.38	21.8	9.99 8.85	7.3	9.99 8.85	7.3	9857 07-32-009	
U 9858	1524.8 4044	65.90 55.44	76.66 38.69	4X	6.2 1.00	0.25 81.	12.17 1.06	2619. 2774.	376 10	1.10	11.80 1.56	50.2	11.17 9.96	6.1	11.17 9.96	6.1	9.1 0.56	9858 07-32-010
1525-42	1525.6 -4237	331.28 11.25	170.02 14.84	10	1.00	0.27	1.01	1195. 1764.	160 15	2	11.80 1.14	27.2	8.93	4.0	8.93	4.0	7.0	-7-32-000
N 5951	1531.4 1510	23.51 50.44	110.15 41.58	5	5.0 1.00	0.79 79.	12.58 1.06	1860. 657.	272 15	1.06	4.80 1.07	27.2	10.62 9.22	0.28	10.62 9.22	0.28	0.58	9895 03-40-003 2
N 5963	1532.3 5645	89.98 48.87	57.39 34.32	12 P	5.6 1.00	0.77 41.	12.04 0.12	657. 854.	265 15	1	11.74 1.29	14.0	10.67 8.93	1.8	10.67 8.93	1.8	26.9	9906 09-25-058 2
U 9912	1532.8 1643	25.96 50.77	108.14 42.10	88	2.7 1.00	0.89 28.	14.04 0.12	1034. 1117.	63 7	1.03	2.59 0.32	8.8	8.67 8.51	0.69	8.67 8.51	0.69	0.69	VV 132 9912 03-40-007
U 9936	1535.1 4424	71.37 52.83	71.44 39.50	9	2.7 1.00	0.57 57.	14.85 0.26	2628. 2800.	188 15	1.02	2.18 0.69	22.1	10.35 9.23	7.6	10.35 9.23	7.6	1.21	DDO 200 5936 07-32-039 2
N 5964	1535.1 609	12.42 45.25	122.13 40.68	78	6.2 1.01	0.79 39.	12.52 0.21	1447. 1492.	215 10	1	9.94 1.75	26.8	10.80 9.34	3.5	10.80 9.34	3.5	18.8	9935 01-40-008 2
U 9941	1536.0 1307	21.42 48.55	113.10 42.39	10	2.5 1.01	0.88 29.	14.43 0.14	1856. 1929.	184 20	1.03	2.24 0.42	14.2	8.99 8.92	0.85	8.92 8.92	0.85	0.85	9941 02-40-005
U 9977	1539.5 52	7.35 41.31	129.18 40.13	5	5.6 1.01	0.19 90.	12.72 1.25	1915. 1944.	291 20	1.08	4.82 0.75	31.7	10.74 9.26	3.3	10.74 9.26	3.3	0.38	9977 00-40-007
U 9979	1539.8 37	7.14 41.10	129.52 40.11	10	2.5 1.01	0.39 70.	14.58 0.70	1978. 2006.	140 30	1	2.32 0.61	14.8	9.83 8.97	13.9	9.83 8.97	13.9	7.2	DDO 201 9979 00-40-008 2
U 9992	1541.4 6725	102.20 42.37	45.91 29.79	10	2.9 1.00	0.70 47.	14.36 0.20	429. 646.	52 7	1.03	2.64 0.34	5.5	8.07 8.04	19.5	8.07 8.04	19.5	4.8	9992 11-19-011
U10014	1543.4 1239	22.00 46.73	114.14 44.09	10	2.2 1.01	0.86 31.	15.11 0.16	1126. 1203.	137 10	1.02	6.31 0.76	7.8	8.31 8.96	8.5	8.31 8.96	8.5	53.5	10014 02-40-013
U10020	1543.6 2044	33.26 49.79	102.85 44.93	7A	3.5 1.00	0.96 17.	13.45 0.09	2089. 2195.	85 15	1	2.10 0.37	22.5	9.50 -18.26	13.9	9.50 -18.26	13.9	0.32	10020 04-37-031
U10031	1545.0 2605	95.22 45.06	51.23 33.27	98	2.7 1.00	0.89 28.	0.49 0.09	888. 1099.	71 10	1.03	1.85 0.40	8.7	8.35	15.5	8.35	15.5	0.94	10031 10-22-000
U10041	1546.5 520	13.62 42.42	124.23 43.18	8X	4.5 1.01	0.61 54.	13.50 0.35	2172. 2224.	224 20	1.07	6.01 0.57	28.9	10.66 9.47	6.6	10.66 9.47	6.6	14.7	10041 01-40-015
U10054	1548.0 8159	116.28 32.93	32.96 21.07	88	4.8 1.01	0.49 63.	13.29 0.50	1499. 1725.	193 20	1	3.71 0.89	24.0	10.36 9.04	4.9	10.36 9.04	4.9	10.2	DDO 203 10054 14-07-029 2
U10058	1548.3 2605	41.73 50.17	95.20 45.89	98	2.0 1.00	0.77 41.	0.16	2154. 2282.	129 10	1.02	1.42 0.36	13.3	10.02 8.87	7.1	10.02 8.87	7.1	0.49	10058 04-37-000 DDO 202
U10061	1548.8 1628	27.88 47.14	109.03 45.89	10	3.5 1.01	0.88 29.	0.14	2087. 2182.	98 10	1.05	2.12 0.56	22.4	9.00	8.5	9.00	8.5	0.96	10061 03-40-000 2
N 6015	1550.7 6228	95.70 44.12	50.04 33.41	6A	6.3 1.00	0.46 65.	11.20 0.45	834. 1048.	319 10	4	20.74 1.82	19.3	10.68 9.36	4.7	10.68 9.36	4.7	8.5	10075 10-23-003 2
U10095	1553.8 4534	72.12 49.36	68.42 42.16	10	2.3 1.00	0.48 64.	0.40 0.40	1869. 2055.	133 25	1.02	2.00 0.52	13.8	9.79 8.93	13.7	9.79 8.93	13.7	0.41	10095 08-29-022
U10288	1611.8 -5	12.28 34.17	134.52 47.29	5	7.4 1.03	0.19 90.	12.34 1.32	2046. 2099.	370 10	1.13	9.62 1.58	45.4	11.09 9.63	3.4	11.09 9.63	3.4	15.7	10095 08-29-022
U10290	1612.0 56	13.34 34.69	133.17 47.73	9	3.2 1.03	0.95 19.	13.61 0.24	1582. 2039.	142 20	1	2.64 0.64	19.0	9.37 9.04	4.5	9.37 9.04	4.5	0.53	10288 00-41-009
U10310	1618.8 4710	73.62 45.53	64.19 44.65	108	4.7 1.00	0.77 41.	12.89 0.16	715. 917.	130 8	1.05	4.94 0.59	12.6	10.01 8.62	4.0	10.01 8.62	4.0	0.47	10290 00-41-010 ARP 2, DDO 204
N 6118	1619.3 -210	11.47 31.45	138.51 48.11	6A	7.1 1.04	0.45 66.	11.59 0.67	1578. 1629.	361 15	1.14	9.45 1.57	33.6	9.98 9.40	2.4	9.98 9.40	2.4	11.1	10310 08-30-002 2
N 6140	1620.5 6530	97.48 39.86	44.73 34.01	5A	10.3 1.01	0.75 42.	11.77 0.20	919. 1147.	239 10	1	29.88 1.76	34.4	10.94 9.59	4.5	10.94 9.59	4.5	0.26	10350 00-42-002 2
U10419	1628.1 2750	46.98 41.89	90.50 54.42	10	2.5 1.01	0.88 29.	0.16	2623. 2786.	98 15	1.39	1.76 0.33	20.5	10.24 8.98	0.99	10.24 8.98	0.99	21.7	10359 11-20-012 2
N 6207	1641.3 3656	59.55 40.68	74.23 53.94	5A	4.8 1.01	0.42 68.	11.57 0.58	852. 1048.	225 10	1.03	7.49 1.08	14.8	10.24 8.92	4.7	10.24 8.92	4.7	4.3	10419 05-39-000
										1.02							0.20	10521 06-37-007 2

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	c_H	b_H	r_H	$B_T^{b,i}$	V	W_{20}	tel.	F_C	A_H^b	$\log L$	$\log M_T$	$\%M_H/M_T$	M_T/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)		
N 6236	1645.0	102.74	38.50	6X	4.4	0.64	12.11	1288.	196	1	5.79	19.8	9.71	10.39	5.4	4.8	10546	12-16-008 2	
	7052	35.78	31.48		1.01	52.	0.31	1525.	15	1.07	0.70	19.3	-18.81	9.13		0.26			
N 6248	1646.8	102.19	38.65	68	4.8	0.42	12.70	1126.	206	1	9.19	19.3	9.38	10.28	8.9	8.0	10564	12-16-009	
	7027	35.78	31.90		1.01	68.	0.60	1364.	20	1.07	1.03	16.6	-17.97	9.23		0.71	ZW COMPACT		
N 6255	1652.9	59.48	72.81	58	5.1	0.45	12.57	921.	220	1	7.16	16.6	9.27	10.29	4.6	10.6	10606	06-37-014 2	
	3635	38.33	56.14		1.01	66.	0.55	1124.	15	1.07	0.99		-17.68	8.96		0.49			
U10608	1653.2	80.75	52.08	88	2.2	0.72	10.94.		116	1	2.97	8.6	9.66	9.66	11.3		DDO 206		
	5311	38.75	45.72		1.01	45.	0.24	1325.	8	1.02	0.44	4.7	8.72				10608 09-28-007 2		
U10669	1701.0	101.65	37.54	10	2.3	1.00	0.40	440.	52	3	0.86						KAR 235		
	7022	34.67	32.64		1.01		0.15	682.	8	1.03	0.26		7.60				10669 12-16-000		
U10736	1708.4	100.48	37.41	8X	5.1	0.40	13.19	491.	159	1	5.27	10.8	8.65	9.81	4.5	14.3			
	6932	34.27	33.69		1.01	69.	0.66	735.	10	1.07	0.84		-16.14	8.45		0.64	10736 12-16-020		
N 6339	1715.5	65.57	61.72	68	4.9	0.59	12.64	2111.	245	1	3.20	33.3	9.87	10.78	2.9	7.9			
	4054	34.58	57.10		1.02	56.	0.40	2336.	20	1.08	0.56		-19.20	9.24		0.24	10790 07-35-059		
U10792	1715.6	106.98	33.62	10	3.1	1.00	0.17	1239.	60	1	1.74	13.6							
	7517	32.31	28.91		1.02		0.17	1481.	8	1.05	0.37		8.58				10792 13-12-000		
U10805	1717.6	36.11	116.50	98	3.1	0.90	13.97	1557.	59	3	1.94	15.3	9.07	8.76		0.48	DDO 207		
	1427	26.66	67.01		1.05	26.	0.35	1715.	8	1.04	0.28		-17.20				10805 02-44-002 2		
U10806	1717.6	76.56	50.95	88	3.8	0.47	12.96	936.	167	1	5.69	12.9	9.15	10.05	7.1	8.0			
	4955	35.04	50.66		1.01	64.	0.53	1175.	15	1.04	0.82		-17.39	8.90		0.56	10806 08-31-040		
N 6368	1724.8	34.02	124.70	3	6.0	0.29	11.80	2767.	403	1	5.06	51.5	10.40	11.25	2.4	7.0			
	1135	23.88	68.26		1.08	78.	1.27	2920.	10	1.09	1.47		-20.53	9.63		0.17	10856 02-44-004 2		
U10862	1725.8	30.12	135.25	58	5.3	0.92	12.64	1694.	157	1	4.33	28.3	9.66	9.16		0.32			
	728	21.86	67.22		1.10	24.	0.46	1834.	10	1.12	0.70		-18.68				10862 01-44-007		
N 6395	1727.1	101.97	34.86	5 P	4.1	0.36	12.04	1167.	218	1	4.37	16.8	9.68	10.25	4.9	3.8			
	7108	32.41	33.00		1.02	72.	0.79	1415.	15	1.04	0.67		-18.71	8.94		0.18	10876 12-16-039 2		
U10951	1746.5	97.33	34.68	10	2.7	0.77		1457.	56	1	1.17	13.3		9.30	17.2				
	6721	31.12	37.15		1.02	41.	0.29	1712.	8	1.03	0.33		8.54				10991 11-22-001		
N 6503	1749.9	100.58	33.17	6A	11.4	0.36	10.07	51.	4	1.08	35.37	10.2	9.13	8.52		0.24			
	7010	30.65	34.60		1.02	72.	0.82	305.			2.57		-17.35				11012 12-17-009 2		
U11074	1756.7	33.43	146.86	7	5.1	0.46	13.19	1899.	215	1	3.88	30.7	9.54	10.55	4.7	10.0			
	709	14.87	73.87		1.28	65.	1.09	2059.	15	1.08	0.61		-18.38	9.22		0.47	11074 01-46-001		
N 6509	1757.0	32.66	149.56	6	3.4	0.83	12.40	1817.	308	1	8.94	19.6	9.82	11.07	3.0	17.3			
	617	14.41	73.45		1.30	35.	0.79	1974.	20	1.05	0.92		-19.08	9.54		0.53	11075 01-46-002		
U11093	1759.5	33.58	148.83	5	6.5	0.22	12.08	1961.	329	1	14.59	40.1	10.01	10.95	7.4	8.6			
	658	14.16	74.35		1.32	85.	1.83	2122.	10	1.10	1.16		-19.55	9.82		0.64	11093 01-46-003 2		
U11105	1802.4	47.82	88.08	8	4.3	0.75	13.70	2226.	195	1	3.00	30.4	9.49	10.71	3.5	16.8			
	2138	19.65	76.64		1.13	42.	0.58	2435.	15	1.07	0.79		-18.23	9.25		0.58	11105 04-42-024		
U11113	1803.4	49.52	81.50	6X	3.0	1.00	14.10	2353.	122	1	2.39	22.5	9.36						
	2316	20.06	76.08		1.12		0.47	2547.	10	1.04	0.41		-17.93	9.19		0.68	11113 04-43-003		
U11124	1805.7	62.16	52.41	68	4.2	0.89	12.78	1609.	175	1	5.15	22.5	9.62	9.25		0.42			
	3533	23.78	67.46		1.07	28.	0.59	1852.	30	1.07	0.72		-18.56				11124 06-40-005 2		
U11141	1805.5	39.42	134.09	8	4.1	1.00	13.37	2241.	112	1	3.08	28.8	9.61	9.26		0.44			
	1204	14.19	78.92		1.31		0.73	2426.	15	1.08	0.50		-18.55	9.26		0.44	11141 02-46-009		
U11152	1810.3	45.64	98.94	88	3.9	0.57	13.31	2730.	175	1	2.91	33.8	9.80	10.48	8.3	4.7			
	1835	16.74	79.43		1.20	57.	0.83	2935.	25	1.05	0.48		-19.03	9.40		0.40	11152 03-46-018		
U11193	1815.7	101.50	30.40	10	2.7	0.66	14.39	1528.	130	1	1.31	14.0	8.94	9.91	5.1	9.3			
	7100	28.49	34.33		1.03	50.	0.39	1786.	25	1.02	0.35		-16.87	8.62		0.48	11193 12-17-020		
U11220	1821.8	68.76	40.10	10	2.5	1.00		1447.	94	1	2.87	12.4							
	4055	22.39	63.82		1.08		0.38	1706.	10	1.03	0.42		8.92				11220 07-38-000		
N 6667	1830.8	98.16	29.36	2XP	5.2	0.74	12.12	2582.	400	1	6.11	43.1	10.25	11.48	1.7	16.5			
	6756	26.93	37.56		1.04	43.	0.37	2847.	30	1.10	1.46		-20.15	9.70		0.28	11269 11-22-053 2		
U11283	1832.6	77.98	32.67	88P	3.7	0.88	13.20	1560.	209	1	4.72	24.4	9.61				IC 1291		
	4914	22.95	56.13		1.07	29.	0.40	2230.	15	1.06	0.82		-18.54	9.37		0.58	11283 08-34-004 2		
N 6689	1835.4	101.05	28.53	7A	6.1	0.41	11.63	487.	238	1	9.51	13.4	9.29	10.25	3.0	9.1	NGC 6690		
	7029	26.83	35.07		1.04	69.	0.75	750.	15	1.10	1.19		-17.74	8.73		0.27	11300 12-17-026 2		
U11332	1840.3	104.51	27.80	78P	3.9	0.42		1565.		1		20.9					NGC 6654A		
	7333	26.80	32.04		1.04	68.	0.72	1824.									11332 12-17-029 2		

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	α_{H}	r_{H}	B_{H}^{I}	V	W_{20}	tel.	F_{C}	A_{H}^{b}	$\log L$	$\log M_{\text{H}}$	$\%M_{\text{H}}/M_{\text{T}}$	M_{T}/L	Alternate Names
(1)	(2)	(3)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
N 6764	1907.0 5051	81.49 18.23	22.88 54.65	48	4.0	0.64 52.	12.06 0.68	2409. 2691.	292 10	1 1.05	4.18 0.66	31.2	10.23 -20.09	10.95 9.48	3.4	5.2 0.18	11407 08-35-003 2	
1945-18	1945.4 -1813	22.48 -20.44	228.23 53.77	98	3.9	0.60 55.	0.65 0.65	1735. 1842.	190 30	1 1.05	3.01 0.88	20.7	10.35 9.01	10.35 9.01	4.5	UGCA 416		
2006-06	2006.6 -627	36.18 -20.16	247.77 61.34	10	4.9	0.58 56.	0.67 0.67	1422. 1588.	98 8	1 1.08	6.90 0.76	22.6	9.80 9.24	9.80 9.24	27.3	UGCA 417	-1-51-000	
U11557	2023.0 6002	94.98 12.82	11.66 42.64	8X	5.0	0.92 24.	12.74 0.80	1393. 1684.	115 10	1 1.11	5.15 0.60	24.6	9.55 -18.39	9.16	0.41	11557 10-29-005		
N 6925	2031.2 -3209	11.27 -34.69	232.86 36.73	4A	6.3	0.43 67.	11.44 0.65	2799. 2847.	517 15	2 1.03	11.64 2.09	52.7	10.52 -20.83	11.53 9.97	2.8	10.0	-5-48-022 2	
2044-13	2044.2 -1302	34.06 -31.36	252.16 50.25	10	3.7	0.56 58.	0.65 0.49	-132. 11.	46 7	1 1.04	3.03 4.45	1.1	7.81 4.56	7.81 4.56	0.1	0.28	DDO 210	
U11651	2055.1 2346	71.13 -12.59	321.38 59.73	8	6.9	0.32 75.	12.56 1.56	1527. 1804.	290 25	1 1.12	4.93 1.05	36.1	9.68 -18.72	10.82 9.21	2.4	13.7 0.34	11651 04-49-005	
2059-17	2059.7 -1700	31.44 -36.36	251.91 44.80	4A	5.7	0.34 74.	0.88 0.88	1479. 1605.	284 20	1 1.09	8.84 1.48	26.7	10.68 9.36	10.68 9.36	4.8	IC 5078, UGCA 419	-3-53-021 2	
U11707	2112.3 74.31	321.21 74.31	321.21 74.31	8A	6.4	0.60 55.	13.37 0.85	908. 1112.	202 10	1 1.13	13.90 1.18	22.2	8.99 -17.00	10.44 9.29	7.1	28.0	11707 04-50-001	
U11782	2135.7 84.5	63.65 -30.89	291.88 49.66	98	3.9	0.60 55.	13.58 0.46	1112. 1343.	146 15	1 1.05	3.40 0.61	15.4	9.02 -17.06	9.99 8.79	6.2	0.59	11782 01-55-006	
N 7107	2139.2 -4502	354.90 -48.58	236.44 18.57	88	2.3	0.92 24.	12.61 0.15	2158. 2180.	107 50	2 1.01	2.63 0.50	21.2	9.82 -19.08	9.82 10.55		0.19 6.7	2	
N 7137	2145.9 2156	76.43 -15.03	312.40 55.80	5XP	2.8	0.83 35.	12.63 0.42	1685. 1952.	190 45	1 1.03	2.49 0.55	15.8	9.72 -18.82	10.55 8.98	2.7	0.18	11815 04-51-005 2	
U11820	2147.0 1401	70.34 -29.49	300.53 47.93	9	2.6	0.70 47.	0.40 0.40	1108. 1354.	128 10	1 1.02	5.12 0.72	10.3	9.81 8.97	9.81 8.97	14.7		11820 02-55-015	
U11861	2155.7 7301	111.05 14.56	13.19 26.99	8X	6.7	0.76 42.	12.45 0.75	1489. 1760.	275 10	1 1.17	14.27 1.14	34.4	9.70 -18.78	11.07 9.65	3.7	23.6 0.88	11861 12-20-000	
U11868	2156.7 1756	75.39 -28.28	306.60 46.02	98	4.1	0.89 28.	0.75 0.32	1102. 1357.	155 15	1 1.07	3.75 0.68	16.1	16.1 16.6	10.71 10.41	5.8		II ZW 158	
2157-43	2157.5 -4322	356.62 -52.69	240.12 17.45	9X	2.5	0.80 38.	0.32 0.18	1357. 2264.	124 15	2 1.01	0.68 0.67	16.6	9.74 -18.87	8.84 9.38	17.1	2.5 0.43	11868 03-56-001	
2159-12	2159.4 -1225	45.08 -37.60	268.15 35.99	88	3.1	0.82 36.	0.18 0.19	2264. 2725.	15 182	1 1.04	0.67 0.66	16.6	9.74 10.71	10.41 9.48	0.43		UGCA 424	
N 7184	2159.9 2159.9	32.90 -42.96	259.47 47.66	58	8.2	0.33 91.	0.19 0.83	2625. 2727.	20 20	2 1.04	0.66 2.24	26.2	10.58 -20.97	9.48 10.01	2.6	10.7 0.27	-2-56-007	
U11891	2201.5 4330	93.61 -9.37	341.66 41.31	10	10.5	0.77 41.	12.13 1.21	461. 756.	154 7	1 1.42	29.04 1.39	23.2	9.10 -17.26	10.41 9.22	6.4	20.9 1.32	-4-52-009 2	
U11909	2204.3 4700	96.11 -6.85	345.73 -39.59	12 P	9.4	0.29 78.	10.65 2.47	1108. 1404.	247 10	1 1.22	8.17 0.71	38.6	10.23 -20.09	10.70 9.21	3.2	3.0 0.09	11909 08-40-001 2	
N 7218	2207.5 -1655	50.09 -51.35	264.69 32.00	68	3.9	0.54 59.	12.16 0.38	1662. 1783.	277 15	1 1.05	6.20 1.34	20.4	9.83 -19.10	10.63 9.29	4.6	6.3 0.29	-3-56-008 2	
22207-19	2207.5 -1906	36.81 -52.16	262.52 30.85	10	3.1	0.41 69.	0.59 0.59	1738. 1848.	151 30	6 1.04	2.21 0.76	16.8	9.95 8.88	9.95 8.88	8.4	UGCA 426, DDO 211	-3-56-009 2	
U11944	2209.6 1739	77.77 -30.66	306.55 42.93	10	3.6	0.41 69.	0.74 0.74	1848. 1985.	176 15	1 1.04	3.64 4.89	21.0	10.18 9.16	10.18 9.16	9.4		11944 03-56-018	
2212-45	2212.9 -4356	351.37 -54.13	240.04 13.70	98	3.2	0.81 37.	0.17 0.17	2042. 2016.	15 170	2 1.01	4.89 1.30	18.9	9.30	9.30			NGC 7232B	
2213-21	2213.7 -2141	33.50 -54.36	260.93 28.23	38	3.9	1.00 1.01	0.10 0.10	2712. 2712.	30 30	1 1.02	1.30 0.92	31.1	9.30	9.30			IC 1438	
22214-21	2214.1 -2130	33.85 -54.40	261.16 28.25	10 P	3.5	0.37 72.	0.69 10.87	1848. 915.	160 20	2 1.01	3.57 1.40	27.5	10.20 9.40	10.20 9.40	15.9	UGCA 427, DDO 212	-4-52-029	
22218-46	2218.3 -4619	350.23 -54.90	240.56 12.74	68	12.1	0.49 63.	0.69 0.44	2668. 886.	20 206	2 1.10	1.40 1.92	31.2	9.40 -18.87	9.40 10.14	7.4	6.1 0.46	11944 03-56-018	
22221-03	2221.6 -344	54.90 -67.36	280.68 34.84	58	3.3	0.78 40.	0.44 0.21	2836. 3012.	98 10	1 1.04	1.93 0.42	29.2	10.14 9.24	10.14 9.24	12.6	UGCA 428	-1-57-007	
22224+15	2224.4 1555	79.64 -34.28	304.78 39.22	10	1.6	0.70 47.	14.92 0.34	1914. 2158.	125 20	1 1.01	0.91 0.52	10.3	8.89 -16.75	9.79 8.63	6.9	7.9 0.55	UGCA 429	03-57-006

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	σ_H	f_0	r_H	B_T^i	V	σ	tel.	F_C	flag	M_B^i	log L	log M_T	% M_H/M_T	M_T/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	(19)	(20)	(21)
N 7292	2226.1	89.65	323.06	108	3.8	0.80	12.50	993.	100	1	5.23	14.0	9.40	9.87	11.3	3.0				
	2231.7	23.17	39.24		1.07	38.	0.45	1269.	10	1.06	6.59	11.7	-18.02	8.93		0.34				12048 05-53-003 2
U12060	2228.2	92.15	327.50	108	3.4	1.00	13.73	1687.	128	1	6.59	11.7	-16.61	8.95		1.33				12060 06-49-025 2
	5334	-20.49	38.47		1.10		0.43	1168.	10	1.06	0.73									
U12069	2230.0	114.90	14.63	8X	3.7	0.68	13.85	2369.	155	1	2.86	28.2	9.49	10.38	8.2	7.8				
	7615	15.88	23.27		1.18	48.	0.72	2631.	15	1.05	0.71					0.64				12069 13-16-000
N 7307	2231.0	357.94	245.97	5XP	5.1	0.38	11.92	2083.	274	2	7.80	31.0	10.66	10.72	6.4	4.6				
	-4111	-58.61	14.07		1.00	71.	0.65	2077.	20	1.02	1.18					0.29				-7-46-003 2
U12082	2232.0	92.32	326.20	9	5.4	0.87	12.93	803.	87	5	6.67	17.2	9.09	10.02	7.5	8.5				DDO 213
	3237	-21.72	37.78		1.09	30.	0.45	1081.	5	1.20	0.56					0.63				12082 05-53-006 2
N 7314	2233.0	27.15	259.21	4X	6.2	0.52	11.17	1430.	317	2	9.71	27.2	10.08	10.86	3.0	6.1				
	22618	-59.14	22.04		1.00	61.	0.58	1499.	10	1.03	1.47					0.18				-4-53-018 2
N 7320	2233.7	93.24	327.47	7A	3.3	0.57	12.77	786.	187	1	1.87	10.2	9.14	10.01	2.1	7.4				ARP 319, VV 288
	3340	-21.02	37.32		1.10	57.	0.66	1066.	20	1.03	0.45					0.15				12101 06-49-042 2
2233-03	2233.9	63.97	282.67	9	3.6	0.87	13.34	1692.	136	1	3.77	19.7	9.30	10.46	4.5	11.7				ARP 3, DDO 214
	-309	-49.65	32.20		1.01	30.	0.16	1867.	10	1.06	0.67					0.52				-1-57-016 2
N 7331	2234.8	93.73	328.07	4A	14.8	0.52	9.62	819.	531	4	51.41	47.6	10.43	11.55	1.7	13.4				
	3410	-20.72	37.04		1.10	61.	0.73	1099.	10	1.16	6.30					0.23				12113 06-49-045 2
2236-05	2236.5	62.34	280.89	10	2.7	0.30	10.99	829.	82	1	1.87	7.9	-20.59	9.79	16.3	0.50				UGCA 433, DDO 215
	-502	-51.35	30.91		1.01	77.	0.96	995.	10	1.02	0.45									-1-57-019 2
U12151	2236.0	68.99	286.83	10	4.4	0.70	0.25	1753.	193	1	5.00	25.1	10.55	9.27	5.3					12151 00-57-007
	8	-48.59	32.10		1.01	47.	0.25	1939.	25	1.07	0.84									
N 7361	2236.6	19.27	256.37	5	4.7	0.35	12.21	1259.	233	2	10.17	18.0	9.54	10.33	8.1	6.2				
	-3020	-61.61	18.68		1.00	73.	0.75	1306.	10	1.01	1.23					0.50				UGCA 434
2240-40	2240.5	359.03	247.93	9	2.4	0.78	13.15	2057.	272	1	4.30	27.5	9.66	10.66	4.9	10.3				-5-53-027 2
	-4007	-60.63	13.20		1.00	40.	0.95	2302.	25	1.05	0.79									
U12178	2242.6	75.96	294.00	8X	4.9	0.56	12.96	1935.	242	1	7.51	30.3	9.67	10.70	7.2	10.7				-7-46-008
	610	-44.62	32.95		1.01	58.	0.39	2142.	10	1.07	0.83					0.78				12178 01-58-004 2
U12212	2248.1	93.42	321.35	9	4.0	0.75	896.	106	1	1.06	3.86	13.5	9.83	9.83	7.7					
	2852	-26.72	34.50		1.05	42.	0.41	1163.	8	1.06	0.58									12212 05-53-019
U12221	2250.0	119.09	20.05	7A	4.1	0.38	13.15	2057.	272	1	4.30	27.5	9.66	10.66	4.9	10.3				
	8238	20.95	19.27		1.08	71.	0.95	2302.	25	1.05	0.79					0.50				12221 14-01-001
N 7412	2252.9	351.91	246.83	3B	4.4	0.82	11.76	1726.	184	2	7.21	22.0	9.95	10.64	4.8	4.9				
	-4255	-61.87	9.73		1.00	36.	0.15	1706.	20	1.02	1.56					0.24				-7-47-004 2
N 7418	2253.8	3.49	251.81	6X	6.5	0.78	11.84	1445.	248	2	7.73	27.7	9.78	10.92	2.0	13.9				
	-3717	-63.87	12.54		1.00	40.	0.16	1453.	20	1.04	1.94	21.6	-18.57	9.21	0.27					-6-50-013 2
2253-36	2253.8	5.23	252.50	5	4.4	0.33	0.80	1659.	256	2	4.54	21.6	9.10	10.49	4.1	0.27				
	-3650	-64.04	12.94		1.00	74.	0.80	1671.	20	1.01	1.07									IC 5269B
2254-43	2254.3	351.37	246.83	7B	5.3	1.00	0.08	938.	134	2	4.14	14.3	8.54	9.10						
	-4305	-62.04	9.42		1.00		0.08	917.	20	1.03	0.71									NGC 7412A
N 7424	2254.5	354.77	248.34	6X	10.5	0.94	10.77	951.	177	2	61.40	28.9	9.83	9.73	2.5	0.80				
	-4121	-62.75	10.30		1.00	20.	0.10	938.	8	1.12	3.14									-7-47-008 2
U12263	2255.0	114.53	10.08	10	6.3	0.70	11.70	1304.	200	2	4.46	54.3	11.19	9.59						
	7225	11.71	23.55		1.44	47.	0.98	2938.	20	1.14	1.06									12263 12-21-000
N 7437	2255.7	85.88	303.89	7X	2.9	1.00	13.31	2117.	125	1	1.65	20.2	9.61	8.96	0.22	0.22				
	1402	-40.28	31.47		1.01		0.16	2345.	30	1.04	0.52									12270 02-58-041
U12281	2256.7	85.63	303.12	8	5.1	0.14	13.61	2567.	305	1	7.05	41.4	9.64	10.89	7.1	17.4				
	1319	-41.02	31.10		1.01	90.	1.25	2793.	20	1.06	1.16					1.26				12281 02-58-043
2256-37	2256.7	1.65	251.52	5X	5.1	0.71	11.70	1304.	200	2	4.10	19.6	9.74	10.48	2.3	5.5				
	-3758	-64.25	11.69		1.00	46.	0.20	1308.	20	1.02	1.90					0.13				-6-50-020 2
N 7456	2259.4	357.16	250.14	6A	8.4	0.34	11.11	1211.	236	2	11.23	29.7	9.91	10.56	4.5	4.5				
	-3951	-64.16	10.28		1.00	74.	0.76	1205.	15	1.05	2.06					0.20				-7-47-011 2
2259-37	2259.5	2.72	252.36	9				1378.	127	2	11.23									
	-3720	-64.95	11.53		1.00		0.08	1384.	15		0.64									-6-50-000
N 7462	2300.0	354.38	249.09	5B	5.8	0.27	11.61	1074.	199	2	8.08	18.1	9.60	10.17	6.1	3.7				
	-4107	-63.80	9.54		1.00	79.	1.05	1061.	10	1.02	1.02					0.23				-7-47-013 2
U12344	2302.5	90.65	309.28	7B	3.6	0.45	1633.	164	1	1.04	4.27	19.5	10.11	9.17	11.7					
	1827	-37.39	30.53		1.02	66.	0.59	1871.	10		0.71									12344 03-58-029

TABLE 1—Continued

NGC/UGC	α	δ	ℓ	SGL	T	σ_H	r_H	$B_{\perp}^{i,j}$	V	W_{20}	tel.	F_C	A_H^b	$\log L$	$\log M_T$	$\%M_H/M_T$	M_T/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	
U12350	2302.8	89.53	307.15	9	4.5	0.39	13.51	2138.	223	1	3.53	31.0	9.54	10.55	5.6	10.2	12350 03-58-032 2	
N 7497	2306.7	91.40	308.81	58	6.2	0.40	12.11	1710.	310	1	1.05	0.58	18.36	9.30	6.4	9.3		
N 7496	2307.0	347.83	247.45	38	5.0	0.80	11.45	1657.	169	2	1.10	0.69	19.53	10.90	3.5	0.59	12392 03-59-002 2	
	-4342	-63.80	7.13		1.00	38.	0.15	1629.	15	1.02	0.81	23.9	10.04	10.56	3.5	3.4	-7-47-020 2	
2307+18	2307.6	91.81	309.14	10	1.6	1.00		1785.	88	1	1.24	9.6					UGCA 436	
N 7531	2312.0	346.40	247.77	4A	6.1	0.56	11.69	1598.	341	2	0.25	28.0	9.91	10.96	5.4	11.4	03-59-005	
N 7552	2313.5	348.07	248.78	28	5.9	0.71	11.20	1609.	280	2	1.88	27.4	9.91	10.92	2.9	6.5	IC 5294	
	-4253	-65.24	6.49		1.00	46.	0.20	1583.	50	1.03	1.72		10.11	10.92	0.19	0.19	-7-47-028 2	
U12578	2321.8	81.61	289.93	12 P	2.6	0.72	14.56	2696.	127	1	2.58	21.8	9.28	10.15	14.9	7.4		
U12588	2322.3	105.91	335.32	8	3.3	1.00	12.74	425.	116	1	0.44	6.7	8.78	9.33	1.11	1.11	12578 00-59-038	
2324-37	2324.2	357.81	254.44	10	3.4	0.41	0.49	690.	103	2	0.54	6.8	8.21	9.23	8.6	0.27	12588 07-48-005	
	-3737	-69.48	7.08		1.00	69.	0.55	686.	25	1.01	0.74		16.48	8.16			-6-51-005	
U12613	2326.0	94.75	305.87	10A	7.8	0.60	12.27	-178.	49	1	5.98	2.2	7.28	8.21	0.6	8.6	PEG IRR, DDO 216	
2326-41	2326.0	347.71	250.99	4A	3.8	1.00	12.12	1512.	142	2	0.52	1	-12.73	5.96	0.05	0.05	12613 02-59-046 2	
U12632	2327.6	106.78	334.88	9	7.6	0.82	12.89	1488.	15	1.02	0.68	15.5	9.69	8.73	0.11	0.11	IC 5325	
	4043	-19.31	26.14		1.12	36.	0.54	695.	7	1.23	1.05	15.4	8.72	10.20	5.5	29.9	-7-48-004 2	
2331-36	2331.8	359.42	256.23	7A	9.3	0.78	11.19	707.	119	2	41.33	19.2	9.41	10.13	15.2	5.2	000 217	
U12682	2332.4	98.57	309.92	10	2.6	0.83	13.78	1397.	125	1	2.22	2.2	-18.05	9.31	0.80	0.80	IC 5332	
U12690	2332.2	87.16	292.15	10	3.1	1.00	0.22	1621.	116	1	3.08	12.5	9.10	10.09	6.7	9.6	000 218	
	56	-56.31	19.39		1.00		0.09	2779.	15	1.05	0.54	25.3	-17.27	8.91	0.64	12682 03-60-007 2		
N 7713	2333.6	353.84	254.70	68	5.5	0.60	11.31	698.	236	2	12.33	11.0	9.34	10.27	3.1	8.5	12690 00-60-015	
N 7716	2334.0	86.62	291.25	38	3.5	0.80	12.78	687.	40	1.02	1.76	28.0	-17.87	8.76	0.27	8.5	-6-51-013 2	
U12709	2334.9	87.07	291.46	9	4.4	0.64	14.08	2677.	155	1	1.98	36.7	9.47	10.46	5.5	9.8	12702 00-60-019 2	
	8	-57.22	18.76		1.00	52.	0.27	2839.	10	1.07	0.63	20.3	-18.19	9.20	0.54	0.54	000 219	
U12710	2335.0	99.22	309.78	10 P	2.5	0.64	14.12	2521.	155	1	2.93	20.3	9.42	10.21	13.7	6.1	12709 00-60-022 2	
U12713	2335.7	104.84	323.57	0	2.5	0.55	14.48	2743.	15	1.02	0.61	19.7	-18.07	9.34	0.84	6.1	12710 03-60-015	
N 7721	2336.2	79.69	284.63	5A	4.5	0.46	11.83	2015.	325	1	13.57	28.3	10.12	10.87	8.3	5.5	82 2335+30	
	-648	-63.12	16.36		1.00	65.	0.46	2148.	20	1.06	1.72		-14.19	7.84	0.93	12713 05-55-044 2		
U12732	2338.1	103.72	318.75	9	4.5	1.00	12.65	756.	140	1	17.51	13.1	9.13	9.24	1.29	0.47	-1-60-017 2	
N 7741	2341.4	104.51	318.69	68	7.4	0.56	11.48	998.	8	1.10	1.17	21.3	-17.35	9.24	4.5	7.0	12732 04-55-042	
2341-32	2341.4	104.51	318.69	9	5.3	0.21	0.46	990.	10	1.04	1.20	4.4	9.59	10.44	0.32	0.32	12754 04-55-050 2	
	-3215	-74.58	6.08		1.00	86.	1.15	282.	8	1.02	0.51	7.96	-18.50	9.05	8.1	5.5	UGCA 442	
N 7755	2345.4	15.38	262.48	58	5.4	0.71	11.60	2868.	299	2	7.38	47.2	10.50	11.22	4.0	5.2	-5-56-001	
U12791	2346.3	105.84	319.00	10	2.8	0.41	14.17	799.	118	1	2.31	8.4	-20.78	9.82	0.21	0.21	UGCA 443	
N 7764	2348.4	341.55	253.25	10	2.5	0.80	12.56	1706.	190	2	2.62	12.2	8.56	9.82	9.1	7.6	000 220	
	-4101	-71.55	1.42		1.00	38.	0.14	1676.	60	1.01	1.08		-15.91	8.39	0.67	0.67	12791 04-56-011 2	
													-18.56	8.87	0.18		-7-48-027 2	

TABLE 1—Continued

NCG/UGC	α	δ	ℓ	SGL	T	ϕ_H^b	r_H	$B_{T,i}^b$	V	W_{20}	tel.	F_c	A_H^b	$\log L$	$\log M_T$	$\%M_H/M_T$	M_T/L	Alternate Names
(1)	(2)	(3)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
U12843	2353.0	104.64	310.55	8X	8X	4.5	0.48	12.98	1777.	208	1	5.17	25.9	9.60	10.46	7.2	7.1	
	1739	-42.95	18.55			1.01	64.	0.50	1989.	20	1.06	0.59		-18.51	9.31		0.51	12843 03-30-039
U12846	2353.3	104.92	311.06	9	9	3.1	0.91		1744.	110	1	1.85	17.9					
	1808	-42.51	18.58			1.01	25.	0.18	1958.	10	1.04	0.39			8.85			12846 03-01-002
U12856	2354.2	104.57	309.47	108	108	3.9	0.40	13.21	1781.	182	1	4.12	23.0	9.51	10.24	9.3	5.5	ARP 262, VV 255
	1633	-44.09	18.06			1.01	69.	0.65	1990.	25	1.04	0.69		-18.28	9.21		0.50	12856 03-01-004
N 7793	2355.3	4.59	261.36	8A	8A	12.0	0.72	9.52	231.	194	4	63.96	8.3	9.13	10.10	2.8	9.3	
	-3251	-77.19	3.14			1.00	45.	0.18	236.	7	1.13	3.15		-17.35	8.55		0.26	-6-01-009 2
N 7798	2356.9	106.88	313.66	12	12	2.3	0.94	12.59	2403.	92	1	1.08	17.9	9.59				MARK 332
	2029	-40.48	18.17			1.01	20.	0.18	2521.	15	1.02	0.40		-19.50	8.87		0.08	12884 03-01-010 2
N 7800	2357.0	104.66	307.54	13	13	3.9	0.72	12.72	1748.	232	1	8.57	22.4	9.68	10.68	6.7	10.1	
	1432	-46.21	16.99			1.01	45.	0.14	1949.	15	1.06	1.00		-18.73	9.51		0.68	12885 02-01-007 2
2359-15	2359.2	75.70	277.82	10	10	14.4	0.47	10.97	-124.		1	75.12	4.2	7.80	7.12		0.21	UGCA 444, DDO 221, MLM
	-1545	-73.60	8.14			1.00	64.	0.43	-42.		1.56	4.00	L	-14.03				-3-01-015 2

TABLE 2
GALAXIES WITH VELOCITIES GREATER THAN 3000 km s⁻¹

NGC/UGC	α	δ	ℓ	SGL	T	$b_{\rm H}$	$r_{\rm H}$	$B_{\rm T}^{\rm i}$	V	W_{20}	tel.	$F_{\rm C}$	$A_{\rm H}^b$	log L	log $M_{\rm H}$	% $M_{\rm H}/M_{\rm T}$	$M_{\rm T}/L$	Alternate Names
(1)	(2)	(3)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)
N 151	31.6	108.95	285.74	48	5.9	0.46	11.84	3748.	472	1	5.25	66.3	10.62	11.56	2.1	8.6		-2-02-054 2
N 173	34.6	-72.09	2.34	5A	1.00	0.65	0.45	3835.	15	1.10	1.78	0.89	-21.08	9.89		0.19		
N 309	54.2	-60.73	4.81	5X	1.00	0.89	12.75	4367.	304	1	5.60	73.9	10.40	10.08		0.45	369 00-02-092 2	
	140	-44.99	0.12			28.	0.12	4499.	15	1.14	1.25	5.66	-20.52	10.05	5.5	5.7		
	54.2	127.33	287.04		5.1	0.85	12.34	5657.	238	1	1.79	85.5	-21.45	10.27		0.32	-2-03-050 2	
	-1011	-72.74	-3.08		1.00	0.33	0.11	5728.	20	1.11								
U 1192	139.5	141.77	311.91	5	5.0	0.53	12.58	2988.	322	1	6.79	45.8	10.15	11.10	5.2	9.2	1192 02-05-009 2	
U 1313	148.3	-48.42	-7.65	58P	1.01	0.60	0.41	3111.	15	1.08	0.81	40.2	-19.88	9.82	0.47		IC 167, ARP 31	
U 1313	148.3	321.50	321.50		4.5	0.61	12.85	2934.	172	1	5.44	40.2	10.03	10.57	14.0	3.5		1313 04-05-021 2
N 697	214.0	-38.88	-6.63	4	1.02	0.54	0.38	3082.	10	1.07	0.74	67.1	-19.59	9.71	0.48	0.48		
N 697	148.5	140.69	321.93		7.0	0.39	11.32	3126.	463	6	13.71	24.1	10.69	11.52	4.5	6.6		
	2206	-38.45	-6.53		1.02	0.70	0.71	3275.	20	1.21	1.23		-21.26	10.17		0.30	1317 04-05-022 2	
U 1678	208.5	-57.82	305.67	5X	3.9	0.82	13.37	3266.	225	1	5.18	38.2	9.89	11.06	5.0	14.8	IC 211, TURN 154A	
U 1678	337	-53.53	-17.16		1.01	0.36	0.17	3333.	15	1.06	0.96	26.6	-19.24	9.76	0.74	0.74	1678 01-03-053 2	
N 922	222.8	211.82	276.23	68P	3.0	0.90	12.45	3086.	268	2	5.24	26.6	10.17	9.68		0.32	UGCA 30	
N 922	-2500	-68.85	-26.62		1.00	0.26	0.10	3029.	25	1.01	0.76	24.1	-19.96	9.68		0.32	-4-06-037 2	
U 80	334.0	193.09	301.11	98	2.7	0.57	0.37	3081.	187	6	1.96	24.1	10.38	9.26	7.5		UGCA 80	
U 80	-653	-45.87	-40.61		1.01	0.57	0.37	3034.	40	1.04	0.52						-1-10-009	
U 2885	349.8	159.57	347.42	5A	9.5	0.50	11.80	5803.	541	1	8.19	163.2	11.01	12.09	2.3	11.9	2885 06-09-012	
U 3090	431.2	138.86	16.14	10	3.1	0.77	1.02	5905.	20	1.26	1.89	27.7	-22.06	10.46	7.0	0.28		
U 3090	7126	16.04	0.30		1.18	0.41	0.66	2916.	155	1	2.29	36.3	10.50	9.34			3090 12-05-000	
U 99	503.9	209.14	307.17	7X	3.9	0.77	0.38	3339.	251	1	4.06	36.3	11.04	11.04	3.8		IC 402, UGCA 99	
U 99	-910	-27.47	-62.68		1.05	0.41	0.38	3209.	25	1.06	1.06		9.62	9.62			-2-13-043	
U 3294	518.4	198.49	334.84	3A	5.6	0.54	12.76	4138.	389	1	5.60	66.2	10.30	11.44	3.3	13.7		
U 3294	358	-18.01	-59.53		1.14	0.59	0.79	4048.	20	1.10	1.54	51.1	-20.28	9.96		0.46	3294 01-14-029	
U 111	529.7	211.06	315.02	3B	5.1	0.80	0.49	3557.	323	1	10.44	51.1	11.46	11.46	4.2		UGCA 111	
U 111	758	-21.22	-68.30		1.09	0.38	0.49	3413.	20	1.10	1.55	79.1	10.09	10.09			-1-15-001	
U 3420	609.1	138.19	24.13	3	5.1	0.33	12.46	5092.	487	1	0.76	79.1	10.65	11.61	0.5	9.1		
U 3420	7557	24.15	1.81		1.05	0.74	1.03	5274.	20	1.07	0.82		-21.15	9.32		0.05	3420 13-05-019	
U 3644	659.9	144.19	27.34	7X	3.5	0.63	13.65	3242.	245	1	3.21	34.8	9.79	10.82	5.6	10.9		
U 3644	7108	26.69	-3.24		1.03	0.52	0.43	3359.	10	1.04	0.64	18.8	-19.01	9.57		0.60	3644 12-07-024	
U 3690	705.1	163.48	28.73	10	2.0	1.00	0.43	3145.	62	1	0.94	47.9	10.50	10.91	6.1	2.6	3690 09-12-040 2	
U 3697	5332	24.03	-20.80		1.05	0.15	0.31	3223.	7	1.02	0.24	47.9	10.50	10.91			3697 12-07-028 2	
U 3697	705.6	143.37	27.76	3 P	4.9	0.15	11.83	3157.	293	1	0.75	47.9	10.50	10.91				
U 3697	7155	27.22	-2.44		1.03	0.50	1.33	3316.	30	1.06	0.75		-20.77	9.70		0.16		
U 4316	815.1	218.82	73.38	8X	2.8	0.94	13.95	4227.	67	1	1.35	33.7	9.83	8.99				
U 4316	446	-61.17	13.17		1.09	0.20	0.44	4052.	12	1.04	0.31	27.3	-19.09	9.34		0.33	4316 01-21-020	
U 4363	819.3	139.86	32.39	7B	2.5	1.00	13.93	3522.	115	1	2.37	27.3	9.75	9.51		0.57	DDO 51	
U 4363	7436	32.29	1.25		1.01	0.89	0.16	3685.	30	1.03	0.45	59.6	-18.90	9.51			4363 12-08-039 2	
N 2595	824.8	202.73	58.58	4X	4.8	0.89	12.32	4335.	385	1	0.69	47.2	-20.81	9.75		0.17	111 2M 59	
N 2595	2139	30.32	-46.43		1.03	0.28	0.26	4255.	40	1.10	0.69						4422 04-20-062 2	
N 2614	837.4	141.11	34.11	5A	4.2	0.87	13.04	3460.	277	1	1.83	44.8	10.09	11.43	0.9	22.1		
N 2614	7309	33.90	0.40		1.01	0.30	0.19	3616.	20	1.08	0.61	47.1	-19.75	9.38		0.19	4523 12-09-005 2	
U 4640	849.2	229.78	94.21	5	5.2	0.41	12.54	3316.	329	1	5.76	47.1	10.16	11.07	4.7	8.2		
U 4640	-158	25.38	-58.23		1.06	0.69	0.82	3109.	15	1.07	0.88	47.2	-19.92	9.75		0.39	4640 00-23-007	
U 4658	851.2	191.47	56.75	5A	3.7	0.92	13.65	4385.	170	1	3.63	47.2	10.01	9.83		0.67	IC 2421	
U 4658	3252	38.96	-33.86		1.01	0.24	0.14	4339.	20	1.06	0.56		-19.54	9.83			4658 06-20-013 2	
N 2718	856.2	222.44	83.17	2X	4.0	1.00	12.57	3849.	133	1	3.90	43.1	10.29	9.72		0.27	4707 01-23-015 2	
N 2718	856.2	31.13	-52.27		1.03	0.63	0.23	3676.	15	1.08	0.67	34.3	-20.26	9.72		0.33	NGC 3218	
N 3183	1017.5	135.27	38.89	3B	3.6	0.69	12.48	3076.	350	1	5.19	34.3	10.22	11.19	3.5	9.3	5582 12-10-028 2	
N 3183	7426	39.15	5.58		1.00	0.48	0.23	3240.	20	1.05	0.84	35.1	-20.07	9.74		0.33	MARK 185	
N 3811	1138.6	151.97	66.17	58P	3.8	0.75	12.51	3104.	307	1	4.72	35.1	10.19	11.17	3.2	9.5	6650 08-21-091 2	
N 3811	4758	65.29	-0.29		1.00	0.42	0.10	3163.	35	1.05	1.14		-19.99	9.67		0.31		
N 4512	1230.3	126.39	53.06	88	3.4	0.75	13.57	2979.	177	6	2.27	31.0	9.75	10.63	5.2	7.6	7700 11-15-060	
N 4512	6409	53.13	11.61		1.00	0.42	0.10	3124.	20	1.07	0.57	126.0	-18.90	9.35		0.39	IC 983, ARP 117	
U 9061	1407.7	9.64	103.35	28	7.9	0.92	12.75	5442.	189	1	7.46		10.57	10.35		0.60	9061 03-36-068 2	
U 9061	1758	69.58	22.17		1.00	24.	0.03	5460.	10	1.28	0.85		-20.94	10.35				

TABLE 2—Continued

NGC/UGC	α	δ	ℓ	SGL	T	σ_H	r_H	B_T^i	V	σ	tel.	F_C	Δ_B^b	$\log L$	$\log M_T$	$\%M_H/M_T$	M_T/L	Alternate Names
(1)	(2)	(3)	(4)	(5)	(6)	(7)	(8)	(9)	(10)	(11)	(12)	(13)	(14)	(15)	(16)	(17)	(18)	
U 9291	1426.6	69.47	80.26	6	4.2	0.58	13.01	2895.	262	1	1.06	2.86	36.9	9.94	10.87	3.5	8.4	9291 07-30-015
	3913	66.54	27.86		1.00	56.	0.22	3007.	10			0.97		-19.38	9.41		0.30	
U 9614	1454.3	8.07	114.89	10	2.6	0.89		3063.				0.95	23.5					
	941	55.59	31.70		1.00	28.	0.10	3087.				0.57						
N 5965	1532.8	90.06	57.24	3	8.0	0.23	11.74	3416.	620	1	1.03	10.98	84.5	10.61	8.96	2.2	16.2	9614 02-38-000
	5651	48.76	34.33		1.00	83.	1.12	3614.	15	1.15		1.17		-21.05	10.16	0.35		9914 10-22-020 2
U 9971	1538.8	91.35	55.29	2	7.0	0.41	11.78	3018.	565	1	1.13	3.61	65.9	10.50	11.69	0.8	15.6	
	5815	47.40	34.39		1.00	69.	0.53	3221.	25			0.92		-20.76	9.57		0.12	9971 10-22-032 2
U10294	1613.1	97.93	45.33	9	3.1	0.68		3516.	185	1	1.03	1.60	34.1		10.62	5.4		
	6532	40.55	33.43		1.00	48.	0.24	3742.	20	1.03		0.69		9.35				10294 11-20-000
U10502	1638.2	104.81	37.86	5A	3.9	0.86	12.49	4305.	277	1	1.07	4.33	52.2	10.51	11.47	3.0	9.2	
	7228	35.68	29.88		1.01	31.	0.18	4541.	15			0.66		-20.80	9.95		0.28	10502 12-16-005
U10584	1649.2	83.77	50.47	5X	3.8	1.00	13.55	5271.	283	1	1.07	5.09	61.5	10.25	10.19		0.87	NGC 6246A
	5529	39.08	43.64		1.01		0.11	5503.	30			1.04		-20.15				10584 09-27-101 2
U10893	1730.5	39.50	111.56	4	5.0	0.66	12.46	3122.	410	1	1.09	7.89	48.3	10.24	11.45	3.0	15.9	
	1626	24.59	70.22		1.07	50.	0.52	3296.	15			0.94		-20.13	9.93		0.49	10893 03-45-001 2
U11360	1847.3	49.50	49.81	10	3.8	0.92		3082.	175	1	1.06	2.30	36.6					
	1839	8.82	86.68		2.00	24.	1.27	3307.	30			0.44		10.56	9.40	3.5	8.1	11360 03-48-000
N 6907	2022.0	18.81	235.30	48	6.2	0.77	11.66	3186.	320	2	1.04	9.41	59.2	-20.91	10.00		0.28	NGC 6908, UGCA 418
	-2500	-30.80	43.93		1.03	41.	0.34	3269.	30			1.32						-4-48-006 2
N 6916	2022.4	93.36	10.46	48	4.5	0.73	13.36	3103.	350	1	1.07	3.41	44.2	9.91	11.35	1.8	27.6	
	5811	11.86	44.28		1.44	44.	0.96	3396.	40			0.72		-19.29	9.60		0.48	11554 10-28-004
U 420	2132.0	39.28	262.13	10	2.2	0.79	0.23	2927.	142	2	1.19	1.19	19.9		10.32	5.4		UGCA 420
	-1344	-42.24	40.90		1.01	39.	0.23	3068.	15	1.00		0.48		9.05				-2-55-000
U11864	2155.9	91.89	340.30	88	6.6	0.67	13.08	4322.	163	1	1.15	4.09	89.0	10.29	10.92	10.5	4.3	
	4203	-9.89	42.77		1.74	49.	1.20	4617.	15			0.72		-20.24	9.94		0.45	11864 07-45-003
U 428	2221.6	60.36	280.68	58	3.3	0.78		2836.	98	1	1.04	1.93	29.2	10.14	10.14	12.6		UGCA 428
	-344	-47.64	34.84		1.01	40.	0.21	3012.	10			0.42		9.24				-1-57-007
N 7309	2231.7	53.75	274.40	4X	3.6	1.00	12.95	4013.	142	1	1.06	1.81	44.0	10.25	9.49		0.18	
	-1037	-53.65	29.80		1.01	0.38	0.10	4156.	15			0.57		-20.14	9.49	5.1		-2-57-016 2
U 432	2236.4	60.99	279.74	5XP	4.2	0.71	0.67	2930.	268	1	1.05	3.29	38.1	10.79	9.50			UGCA 432
	-605	-51.99	30.55		1.01	71.	0.67	3092.	15			0.70						-1-57-018
U12213	2248.5	78.32	295.42	8X	3.1	0.95		3213.	115	1	1.05	2.68	31.3		9.50			12213 01-58-010
	702	-44.89	31.75		1.01	19.	0.15	3421.	15			0.57		9.38			30.1	
N 7610	2317.1	89.00	300.45	5	4.0	0.83	13.60	3560.	295	1	1.07	9.85	44.4	9.90	11.38	5.8		12511 02-59-025 2
	954	-46.56	25.52		1.01	35.	0.19	3766.	30			1.32		-19.28	10.15		1.76	
N 7757	2346.2	94.74	296.08	5A	3.8	0.89	13.04	2953.	173	1	1.06	4.17	34.9	9.97	9.61		0.44	12788 01-60-037 2
	354	-55.23	17.06		1.01	28.	0.13	3124.	15			0.59		-19.43				

TABLE 3
 NONDETECTED OR CONFUSED GALAXIES

NGC/UGC	α	δ	ℓ	b	SGL	SGB	T	a_H^b	r_H	$B_T^{b,i}$	
U 20	1.5	8001	120.85	17.61	16.5	17.6	8	3.9	0.67		
0004-06	4.3	-654	93.62	-66.92	286.7	9.7	13 P				ARP 146
U 93	7.7	3035	112.61	-31.18	324.5	17.4	8A	4.0	0.79	13.90	
0009-34	9.6	-3423	350.98	-79.05	260.9	-0.2					
U 112	9.6	4128	115.14	-20.53	335.9	18.3	9	3.4	1.00		
U 115	10.0	8806	122.64	25.53	24.8	16.0	9B	3.6	0.92		
U 128	11.2	3543	114.46	-26.26	330.0	17.3	8	3.7	0.88		
0016-19	16.3	-1917	78.56	-78.95	275.7	3.2	9	2.5	0.94		UGCA 5, DDO 1
U 282	25.7	307	111.67	-58.97	298.0	7.3	8X	3.1	1.00	13.77	
U 290	26.5	1537	115.10	-46.64	310.3	10.3	10	3.3	0.18		
U 303	27.8	4149	118.78	-20.61	336.7	14.9	9	3.6	0.74		
N 145	29.2	-526	110.02	-67.53	289.9	4.2	8B	3.0	0.94	13.12	
0029-40	29.8	-4032	318.54	-76.28	256.2	-5.8	10	1.7	1.00		
N 147	30.4	4814	119.81	-14.25	343.4	15.3	-5	22.8	0.67	9.71	DDO 3
U 329	31.0	224	114.02	-59.89	297.6	5.9	6A	3.3	0.74	14.38	
U 334	31.3	3110	118.57	-31.28	326.0	12.5	9AP	3.2	1.00	14.04	DDO 4
U 351	33.0	851	116.35	-53.54	304.0	7.1	1B	5.0	0.43	12.63	IC 34
U 372	34.8	4238	120.23	-19.89	337.7	13.8	9A	3.9	0.92		
U 393	36.0	1708	118.58	-45.36	312.3	8.4	9	3.1	0.36		
U 394	36.0	4143	120.41	-20.82	336.8	13.4	8X	3.7	0.38	14.28	
0039-34	39.6	-3428	318.30	-82.65	262.6	-6.1					
0044-22	44.7	-2251	110.74	-85.34	274.2	-4.2	10	2.3	0.74		UGCA 12
N 266	47.1	3200	122.54	-30.60	327.5	9.4	2B	5.5	0.95	11.71	
U 525	48.9	2926	122.98	-33.17	325.1	8.4	12XP	2.8	0.63	14.69	POSSIBLE DET. 4200 KM/S
0050-37	50.2	-3751	301.68	-79.55	259.8	-9.0					
0057-33	57.6	-3358	287.78	-83.18	264.0	-9.6	-5	4.7	0.82		SCULPTOR
U 628	58.3	1913	126.02	-43.33	315.7	3.8	9B	3.5	0.80		
U 655	101.2	4535	125.23	-16.96	341.6	9.6	9	5.1	1.00	12.64	
U 726	107.4	-201	133.64	-64.24	295.8	-4.1	8X	3.1	0.59	13.92	
0114+37	114.8	3710	128.68	-25.15	334.0	5.1	10	1.8	0.82		UGCA 16
N 521	122.0	128	139.71	-60.06	300.2	-6.6	4B	5.4	0.95	12.40	
N 523	122.5	3346	130.91	-28.32	331.2	2.6	13 P	4.9	0.32	12.96	ARP 158, IV ZW 45
N 536	123.6	3427	131.05	-27.61	331.9	2.6	3B	5.1	0.54	12.18	
U 1015	123.7	940	136.98	-51.99	308.2	-4.7	-2	2.9	0.58	15.15	IC 114
U 1026	124.5	1320	136.06	-48.37	311.8	-3.9	9	3.1	0.77		
U 1033	124.8	3118	131.90	-30.68	328.9	1.4	5	5.1	0.28	12.59	
U 1073	127.3	2536	133.72	-36.20	323.7	-0.8	9B	3.1	0.62	13.94	DDO 11
N 590	130.6	4440	130.73	-17.31	342.0	4.4	0B	6.3	0.54	12.18	
U 1118	131.2	318	142.99	-57.66	302.6	-8.3	8A	3.8	0.34	13.78	
0132-07	132.2	-715	151.93	-67.39	292.3	-11.4	10	1.7	0.45		UGCA 19
N 645	137.6	528	144.49	-55.10	305.1	-9.3	3B	4.4	0.48	12.66	
U 1205	140.6	838	143.95	-51.86	308.4	-9.0	3	5.2	0.32	12.48	IC 1723
U 1211	141.3	1333	141.87	-47.13	313.2	-7.7	10	4.4	0.70		
U 1230	142.7	2516	138.00	-35.77	324.5	-4.2	9	3.6	1.00		
N 678	146.8	2144	140.34	-38.92	321.4	-6.3	3	6.9	0.29	11.73	
N 684	147.3	2724	138.53	-33.44	326.8	-4.5	-2	5.3	0.33	12.51	IC 165
U 1291	147.3	2657	138.68	-33.87	326.4	-4.6	5	2.8	0.68	13.31	IC 1731
U 1329	149.1	1755	142.52	-42.40	318.0	-8.1	5B	3.7	0.39	13.89	DDO 16
U 1449	155.6	250	153.59	-55.77	303.9	-14.3	9BP	3.4	0.46	13.07	MARK 582, VV 122
U 1502	158.4	3007	140.36	-30.14	330.3	-5.8	10	3.2	0.54		
0200-09	200.7	-953	170.35	-65.66	291.4	-18.9	5 P	4.3	0.17		UGCA 23
N 801	200.7	3801	138.21	-22.46	337.8	-3.2	5	5.2	0.28	11.94	
U 1579	202.6	552	153.88	-52.27	307.4	-15.1	7B	3.5	0.96	13.36	IC 1776
N 818	205.7	3832	139.05	-21.67	338.6	-3.9	5X	5.4	0.45	11.62	
U 1634	205.7	4659	136.33	-13.63	346.4	-0.5	6X	6.1	0.94	12.36	

where the correction factor, f_a , was determined empirically from a correlation with galactic absorption, A_b :

$$f_a = \text{dex}(0.215A_b^2). \quad (3)$$

Evidence for this correlation is provided in the discussion below. Dimensions have *not* received an adjustment for line-of-sight inclination effects.

Paturel (1975) chose to convert minor axes completely independently of major axes; this procedure potentially produces the anomaly that the adjusted minor axis

exceeds the major axis. We prefer to apply the correction to the *ratios*, $r=b/a$, determined by Fisher and Tully (1975):

$$r_H = 0.91r_N + 0.09, \quad (4a)$$

$$r_H = 0.88r_V + 0.12, \quad (4b)$$

$$r_H = 0.91r_D + 0.09. \quad (4c)$$

Inclinations, i , are derived from the familiar formula:

$$\cos^2 i = (r_H^2 - r_0^2) / (1 - r_0^2), \quad (5)$$

TABLE 3—Continued

NGC/UGC	α	δ	ℓ	b	SGL	SGB	T	a_H^b	r_H	$B_T^{b,i}$	
N 828	207.1	3857	139.19	-21.19	339.1	-4.0	1 P	5.8	0.79	11.66	VI ZW 177
U 1721	211.5	3710	140.70	-22.59	337.8	-5.5	4B	3.8	1.00	13.16	
0214+37	214.6	3710	141.33	-22.38	338.1	-6.1					
U 1771	215.3	3741	141.27	-21.84	338.6	-6.0	9	3.7	0.83		
U 1780	215.9	4020	140.40	-19.32	341.1	-5.0	10B	3.5	0.27	13.75	
U 1803	217.9	635	158.60	-49.79	309.4	-18.5	10	3.9	0.30	13.82	
U 1810	218.4	3910	141.32	-20.24	340.2	-5.9	3 P	3.6	0.70	12.79	ARP 273, V ZW 223, VV 323
U 1830	219.3	4737	138.36	-12.28	347.9	-2.3	0B	7.0	0.83	12.18	V ZW 227
0219-21	219.8	-2121	201.64	-68.49	280.2	-25.5	10	1.7	1.00		UGCA 27
U 1857	221.6	3257	144.49	-25.77	334.9	-9.2	7	3.9	0.36	13.99	
U 1883	222.8	1115	156.61	-45.16	314.5	-18.0	7	3.8	0.34	14.46	
U 1886	222.9	3916	142.14	-19.83	340.7	-6.6	4X	6.9	0.56	11.50	
0223-10	223.9	-1003	179.74	-61.71	292.6	-24.5	9X	5.1	0.41		DDG 20
N 931	225.3	3105	146.12	-27.17	333.5	-10.7	4A	6.5	0.35	12.23	
U 1945	225.7	-134	169.00	-55.31	301.7	-22.8	9	3.7	0.43	13.25	
N 945	226.2	-1046	181.66	-61.75	292.0	-25.2	5B	3.9	0.92		
U 1981	227.8	43	167.24	-53.20	304.3	-22.6	10	2.7	0.89		
U 1986	228.0	-120	169.51	-54.76	302.2	-23.3	3	4.9	0.36	12.23	POSSIBLE DET. 1500 KM/S
0228-10	228.0	-1058	182.58	-61.53	291.9	-25.7	10	3.6	0.69		DDO 23
N 958	228.2	-309	171.67	-56.10	300.3	-23.8	5B	4.4	0.33	12.14	
0230-39	230.7	-3932	249.44	-65.69	259.9	-28.6	9B	2.9	0.41		NGC 986A
U 2064	232.3	2038	153.20	-35.85	324.4	-16.5	4XP	3.6	0.76	13.56	
U 2069	232.5	3725	144.76	-20.78	339.9	-9.1	6X	4.2	0.71	12.18	VV 96
U 2081	233.4	12	169.58	-52.72	304.2	-24.1	6X	4.4	0.70	13.67	
U 2094	233.8	3554	145.70	-22.05	338.7	-10.1	5B	3.8	0.96	12.70	POSSIBLE DET. 2600 KM/S
0234-05	234.5	-534	176.75	-56.75	298.1	-26.0	5B	2.2	0.79		UGCA 36
U 2109	234.9	3402	146.79	-23.64	337.1	-11.2	7X	3.2	0.90	13.15	
U 2116	235.3	3037	148.53	-26.68	334.0	-12.8	8	3.3	0.86		
U 2125	235.6	3151	147.98	-25.54	335.2	-12.3	5B	3.7	0.88	13.36	IC 1823
N 1022	236.1	-653	179.02	-57.36	296.8	-26.7	1B	4.4	0.92	12.08	
N 1024	236.5	1038	161.07	-43.90	315.1	-21.4	2A	6.8	0.41	11.91	ARP 333
N 1032	236.8	53	169.92	-51.64	305.2	-24.7	1	5.7	0.40	12.12	
U 2157	237.3	3821	145.26	-19.54	341.2	-9.5	8	3.5	0.36	13.55	
0237-34	237.5	-3444	237.30	-65.72	265.3	-30.2	-5				FORNAX
U 2174	239.1	3209	148.57	-24.94	335.8	-12.8	5X	3.7	0.96	13.63	
U 2179	239.5	3500	147.25	-22.36	338.4	-11.5	6B	2.9	1.00	13.82	
U 2185	240.0	4014	144.90	-17.61	343.1	-9.1	5	5.6	0.36	11.95	
U 2242	243.8	2008	156.37	-34.94	325.2	-19.2	10	2.0	1.00		
0246-00	246.3	-33	174.28	-51.11	304.5	-27.4	10	1.6	1.00		UGCA 42
U 2370	251.2	4227	145.81	-14.69	346.2	-9.8	10	5.5	0.12	13.52	
U 2435	254.9	3503	150.22	-20.83	340.1	-14.2	6A	4.2	0.82	13.11	
0255-04	255.8	-430	181.53	-52.10	300.9	-30.8	6B	3.5	0.53		UGCA 47
N 1167	258.6	3501	150.94	-20.48	340.5	-14.9	-2A	5.6	0.72	12.96	
U 2497	259.2	2855	154.49	-25.63	335.1	-18.2	8	5.2	0.30	12.88	
0301-25	301.7	-2528	216.94	-60.31	276.3	-35.4	9	2.9	0.90		UGCA 50, DDO 227
N 1186	302.2	4239	147.54	-13.53	347.4	-11.4	5B	7.3	0.45	11.17	
U 2526	302.6	3635	150.82	-18.72	342.3	-14.8	3	7.0	0.25	11.39	
0304-19	304.0	-1936	206.18	-58.19	283.6	-35.6	10	1.7	0.73		UGCA 51
U 2543	304.2	3739	150.53	-17.64	343.4	-14.4	8A	3.8	0.39	13.57	
U 2557	306.0	3827	150.41	-16.77	344.3	-14.3	8A	5.2	0.79	13.64	
0308+01	308.7	108	178.41	-45.94	308.3	-32.2	13 P	1.1	1.00	14.64	IC 298, ARP 147, I ZW 11
N 1241	308.8	-907	190.72	-52.32	296.5	-35.1	3B	5.5	0.71	12.45	ARP 304, VV 334
N 1247	309.8	-1040	193.09	-52.95	294.7	-35.6	3	5.0	0.25		UGCA 58
0310-25	310.0	-2519	217.38	-58.45	276.6	-37.3	13 P	1.0	0.82		UGCA 59
U 2596	310.2	4357	148.14	-11.67	349.4	-11.8	9A	5.0	0.59	12.76	
0311-02	311.8	-258	183.68	-48.06	304.0	-34.2	10	3.0	0.61		ARP 279, DDO 31

CONFUSED WITH NGC 1253

where the intrinsic flattening of galaxies is taken to be $r_0 = 0.20$ in Holmberg's system (Holmberg 1958).

We will now go on to justify the system of dimensions that has been chosen. Readers with weak stomachs may wish to pass to the next subsection.

Although we have chosen to publish dimensions in the Holmberg system, there are substantial possibilities of systematic errors in both the major and minor diameters. It must be noted that, if $j = N, V$, or D , then a_H/a_j is strongly correlated with a_H (or a_j) in the sense that as a_H decreases then a_H/a_j increases. The amplitude of the effect is quite strong: for late spirals, as a_H varies from

15' to 3', the ratio a_H/a_N varies from 1.2 to 1.6. It must be concluded that there is a systematic error in either the densitometrically reduced data by Holmberg (1958) or the eyepiece-estimate dimensions in the UGC and MCG and the heterogeneously derived sample in the BGC (and, it would follow, in the RC2).

A test of which system is in error is to look for a systematic effect as a function of apparent dimension in a plot of absolute magnitudes versus intrinsic diameters (Fig. 1). Intrinsic luminosities and diameters can be determined assuming distances defined by redshifts. Errors due to distances are not severe in such a plot

TABLE 3—Continued

NGC/UGC	α	δ	ℓ	b	SGL	SGB	T	a_H^b	r_H	$B_T^{b,i}$	
U 2617	312.7	4043	150.30	-14.16	347.0	-14.1	7X	5.6	0.39	12.51	
U 2623	313.4	3452	153.75	-18.99	342.1	-17.5	7B	4.5	0.93	12.78	
U 2655	315.4	4303	149.45	-11.93	349.2	-13.1	7X	4.7	0.48	12.41	
U 2702	319.7	3651	153.70	-16.64	344.5	-17.4		5.7	0.94	12.76	
U 2709	320.7	3830	152.89	-15.16	346.0	-16.6	3X	6.1	0.45	12.64	
0325-33	325.3	-3339	233.34	-55.97	265.6	-40.1	10	3.0	0.78		
N 1353	329.9	-2058	212.01	-52.90	282.4	-41.7	3X	4.7	0.46	11.76	UGCA 76
U 2789	331.5	6724	137.70	9.55	9.6	0.7	12B	5.6	0.73		
N 1376	334.7	-512	191.23	-44.80	303.3	-40.3	6A	3.2	1.00	12.54	
0336-04	336.0	-429	190.66	-44.13	304.3	-40.4	9A	3.7	0.70		UGCA 82
N 1437	341.7	-3601	237.36	-52.59	261.7	-43.0	1B	4.6	0.74	12.27	
U 2858	343.9	4548	152.03	-6.74	354.7	-15.3	8	6.2	0.73		
U 2906	355.1	7356	135.05	15.85	15.6	3.9	3	5.7	0.64	12.67	
N 1495	356.8	-4436	250.53	-48.99	249.3	-43.0	5	4.5	0.29		
U 2936	400.2	149	188.52	-35.55	315.1	-43.9	6	4.0	0.40	13.87	
0408-31	408.0	-3122	230.72	-46.83	266.5	-49.4	10	1.7	0.82		UGCA 89
U 2988	410.6	2521	170.18	-18.32	342.2	-33.1	3	5.0	0.39	13.42	
0410-33	410.9	-3308	233.38	-46.44	263.6	-49.5					
0422-21	422.5	-2117	218.08	-41.34	281.9	-54.0	10	3.1	0.54		UGCA 91
N 1569	426.0	6445	143.67	11.24	11.9	-4.9	10B	10.3	0.46	10.68	VII ZW 16
U 3059	427.1	335	191.39	-29.04	321.8	-49.2	8A	3.8	0.47	13.75	
N 1589	428.2	45	194.28	-30.37	318.1	-50.7	3	5.1	0.38	12.30	
U 3066	428.3	526	189.85	-27.74	324.4	-48.5	7X	3.2	0.77	13.77	
N 1618	433.7	-314	199.07	-31.29	313.1	-53.6	3B	4.0	0.40	12.60	
N 1620	434.0	-14	196.14	-29.67	317.7	-52.5	5	4.9	0.43	12.28	
N 1625	434.6	-323	199.36	-31.17	313.0	-53.9	3B	3.7	0.30	12.09	
U 3114	435.5	6632	142.97	13.16	13.8	-4.0	5	5.5	0.41	13.24	
U 3129	437.8	1700	181.22	-18.99	339.8	-43.4	10	4.3	0.56		
U 3165	444.5	2353	176.61	-13.49	347.7	-39.6	10A	5.0	0.64		
U 3214	455.4	-12	199.22	-25.08	322.0	-57.2	4	5.1	0.26	12.43	
0503+30	503.9	3046	173.76	-5.87	357.4	-36.7	10	7.6	1.00		UGCA 100
U 3259	508.2	7216	139.93	18.86	19.1	-0.4	7X	3.7	0.74	13.95	
U 3294	518.4	358	198.49	-18.01	334.8	-59.5	3A	5.6	0.54	12.76	
U 3326	532.2	7717	136.02	22.62	22.4	3.6	5	5.2	0.18	13.76	
N 2206	614.0	-2645	233.90	-19.13	244.2	-75.7	4X	3.9	0.60		UGCA 123
U 3583	650.2	1659	197.96	7.98	25.6	-57.4	10	11.2	1.00	11.42	
U 3714	706.8	7150	143.48	27.31	27.9	-2.5	12 P	3.2	0.86	12.14	
N 2365	719.5	2210	196.13	16.43	36.8	-51.7	1X	5.7	0.58	12.30	
0729+66	729.2	6659	149.10	28.96	30.3	-7.1	10	4.5	0.70		UGCA 123, DDC 44
0733+02	733.5	249	215.63	11.17	56.3	-69.0	10	4.0	0.72		UGCA 134, DDO 45
N 2424	737.3	3920	180.16	25.81	37.2	-34.1	3B	5.7	0.21	12.23	
U 4016	743.5	3908	180.72	26.92	38.6	-34.0	13 P	4.6	0.79	13.63	ARP 143, VV 117
U 4277	810.1	5248	165.88	33.54	39.0	-19.6	5	5.5	0.19	13.15	
N 2554	814.9	2337	199.72	28.83	54.3	-45.9	0 P	5.5	0.77	12.15	
U 4343	817.3	1731	206.40	27.18	59.8	-50.9	10	2.0	0.75		
U 4365	819.5	1934	204.47	28.42	58.7	-48.9	9	3.5	0.26	13.42	IC 2329
N 2618	833.3	52	224.87	23.40	85.5	-60.2	2A	5.2	0.85	12.16	
N 2648	839.9	1428	212.03	30.99	69.4	-49.9	1	5.5	0.37	11.80	ARP 89
0845-19	845.2	-1952	244.91	14.42	130.0	-62.9	4	6.1	0.20		UGCA 145
U 4623	847.1	7641	136.87	33.27	33.1	3.9	5	5.1	0.35	12.12	
U 4659	851.2	4717	172.80	40.11	47.9	-21.7	8A	3.7	0.43	13.92	
N 2684	851.3	4920	170.13	40.04	46.8	-20.0	12 P	1.6	0.90	13.28	
U 4669	852.3	1907	208.21	35.49	68.1	-44.5	9	2.6	0.89	14.25	
N 2713	854.7	306	225.67	29.15	87.5	-54.5	4B	5.8	0.41	11.85	
U 4701	855.6	7829	134.69	32.95	32.6	5.6	7A	3.4	0.50	14.10	
N 2730	859.5	1702	211.38	36.33	71.8	-44.8	9BP	2.7	0.79	13.13	

because uncertainty displacements are almost parallel to the relationship. Once the parameters of the correlation between magnitude and dimension have been defined for a given dimension convention then the relative displacement from the mean relation as a function of apparent size can be determined.

We have considered a sample of 535 Sbc-Sd galaxies with measured diameters and magnitudes and systemic velocities less than 3000 km s^{-1} , either observed by ourselves and listed in Table 1 or described in the literature. The relationship between absolute magnitude $M_B^{b,i}$ and intrinsic diameter A , assuming the Holmberg

convention, is³

$$M_B^{b,i} = -5.67 \log A_H - 11.29 - 0.67 \log h, \quad (6a)$$

and, assuming the UGC convention, is

$$M_B^{b,i} = -5.34 \log A_N - 12.54 - 0.34 \log h. \quad (6b)$$

³Scatter caused by distance uncertainties will cause the derived relationship to be somewhat flatter than the intrinsic relationship. Magnitudes and diameters are calculated assuming a Hubble constant of $100 \text{ km s}^{-1} \text{ Mpc}^{-1}$, and the relationship depends on the actual Hubble constant H_0 according to the term in h where $h = H_0/100$.

TABLE 3—Continued

NGC/UGC	α	δ	ℓ	b	SGL	SGB	T	a_H^b	r_H	$B_T^{b,i}$	
U 4780	903.8	1932	208.90	38.18	70.4	-42.3	8X	2.7	0.79	13.93	
U 4824	908.0	5127	166.97	42.48	48.0	-16.7	7A	3.8	0.31	13.42	
0908-08	908.4	-841	238.90	25.60	109.0	-56.2	3	7.2	0.24		UGCA 150
											POSSIBLE DET. 1650 KM/S
U 4858	910.6	1935	209.54	39.70	71.8	-41.1	10	2.6	0.94	14.31	DDO 58
U 4871	911.7	3927	183.36	43.81	56.1	-26.1	9X	2.9	0.39		DDO 59
U 4879	912.5	5303	164.66	42.89	47.6	-15.0	10A	3.8	0.64	12.99	VV 124
N 2815	914.1	-2326	252.18	17.40	135.6	-55.9	3B	5.8	0.38	11.38	UGCA 156
0917+76	917.2	7600	136.66	35.17	35.0	4.2	10	2.0	0.92		UGCA 158
0920-32	920.8	-3213	259.89	12.51	149.8	-52.6	1	7.6	0.38		IC 2469, UGCA 163
U 4998	920.9	6836	144.69	38.89	39.5	-1.7	10	3.1	0.68	14.16	
N 2857	921.3	4934	169.08	44.86	50.9	-17.0	5A	3.7	0.92	13.35	ARP 1
U 5005	921.6	2229	206.96	43.06	71.4	-37.3	10	2.6	0.83		
U 5015	922.7	3430	190.52	45.68	61.6	-28.5	8X	3.1	0.91	14.20	
U 5040	924.7	2901	198.35	45.32	66.3	-32.2	10	3.4	0.96	14.21	
U 5042	925.1	6641	146.70	40.08	40.9	-3.0	8B	2.0	1.00		
N 2900	927.7	422	229.37	36.89	92.4	-46.8	5BP	2.6	0.83	13.68	
U 5071	928.3	4234	178.86	46.89	56.6	-21.7	10	3.1	0.09		
U 5076	929.1	5205	165.22	45.56	50.3	-14.3	10	2.5	0.94	14.39	
U 5086	929.9	2142	208.80	44.66	73.7	-36.4	10	1.7	1.00		CONFUSED WITH NGC 2903
0930+55	930.5	5527	160.54	44.85	48.3	-11.5	13 P	0.5	0.75		UGCA 166, MARK 116, I Zw 18
N 2916	932.1	2156	208.70	45.22	73.9	-35.8	3AP	3.8	0.71	12.45	POSSIBLE DET. 700 KM/S
0933+88	933.0	8824	124.37	28.44	27.8	14.4	8A	3.8	0.89		
N 2962	938.3	524	229.99	39.68	92.9	-43.9	-2X	4.9	0.76	12.60	
U 5189	940.3	943	225.37	42.26	88.1	-41.4	10 P	4.8	0.39	12.41	
0940-05	940.9	-503	241.19	34.22	107.0	-47.4	8BP	2.0	0.20		UGCA 173, ARP 253, VV 52
0942-29	942.4	-2906	261.09	17.98	143.3	-48.8	9	3.2	0.68		PROB. CONF. W. PEC. GAL. 5' S.
U 5218	942.9	637	229.41	41.29	92.1	-42.4	7X	3.1	0.54	13.76	UGCA 179
N 2998	945.5	4418	175.74	49.80	57.8	-18.3	5X	3.9	0.54	12.51	
											PROBABLE DET. 4700 KM/S
N 3024	947.8	1300	222.48	45.40	85.7	-38.1	5	3.1	0.32	12.79	CONFUSED WITH NGC 3020
U 5286	948.5	914	227.28	43.80	90.0	-39.9	7A	3.3	0.74	13.58	
0948-18	948.8	-1815	254.12	26.85	126.9	-47.9	7B	2.9	1.00		UGCA 185
U 5302	950.3	6834	142.98	41.23	41.6	-0.1	8A	3.4	0.79	13.76	
N 3052	952.0	-1824	254.85	27.27	127.2	-47.2	5X	3.5	0.71	12.23	
N 3054	952.2	-2527	260.18	22.15	137.5	-47.1	3X	5.7	0.67		UGCA 187
U 5336	953.7	6916	141.98	41.08	41.3	0.7	10	4.4	0.91		DDO 66, HD IX, KAR 62
0956-24	956.0	-2456	260.51	23.10	136.7	-46.2	7B	4.3	0.30		UGCA 190
N 3074	956.7	3538	189.27	52.68	66.1	-22.8	5X	3.7	0.92	13.70	
N 3095	958.0	-3120	265.31	18.52	145.7	-45.1	5X	5.3	0.85	11.66	UGCA 192
U 5421	1001.3	5534	158.05	48.86	51.5	-8.5	9	3.1	0.23		PROBABLE DET. 1120 KM/S
U 5428	1001.3	6648	144.13	43.10	43.5	-0.6	10	1.7	1.00	15.85	DDO 71, KAR 33
U 5439	1003.0	19	240.15	41.87	102.5	-40.4	-5	4.8	1.00		SEXTANS C
U 5442	1003.0	6805	142.59	42.47	42.8	0.4	10	3.1	0.54		KAR 64
1003-07	1003.2	-730	247.90	36.85	112.5	-42.8	10	1.9	0.67		UGCA 200, KAR 65
N 3124	1004.2	-1859	257.69	28.82	128.3	-44.3	4X	4.6	0.85	11.83	UGCA 202
U 5464	1005.3	2947	199.24	54.17	72.3	-25.1	9	2.5	0.64		DDO 72
U 5470	1005.8	1233	225.99	49.11	89.0	-34.6	-5	12.0	0.79	11.04	DDO 74, KAR 67, LEC 1, REGULUS
1008-13	1008.7	-1332	254.31	33.56	120.9	-42.6	10	3.7	0.43		DDO 76
U 5495	1009.1	1641	220.68	51.61	85.2	-31.8	5	4.4	0.20	13.33	
U 5520	1011.3	6524	144.85	44.74	45.3	-0.9	5	3.4	0.67	13.60	
N 3175	1012.5	-2837	266.13	22.59	141.5	-42.3	3XP	6.8	0.39	11.25	UGCA 207
N 3200	1016.1	-1743	259.20	31.62	126.8	-41.4	3A	7.0	0.36		UGCA 210
N 3221	1019.6	2149	213.99	55.72	81.6	-27.0	9B	4.8	0.31	12.92	
U 5604	1019.7	4630	169.79	55.07	60.4	-12.4	5X	3.9	0.54	13.47	
U 5618	1020.5	2119	214.94	55.77	82.2	-27.1	12	1.7	0.23		
1022+67	1022.8	6755	141.13	43.59	44.1	1.7	10				DDO 78

The logarithmic *deviations* of individual intrinsic diameters from these mean relations are given as functions of apparent diameters in Figure 2. If the Holmberg data are in error then we anticipate *positive* deviations at small apparent dimensions, and if the Nilson data are in error then we anticipate *negative* deviations at small apparent dimensions. It is evident that the test indicates the errors are in the Nilson system.

There are at least two competing effects that could cause the observed downturn at small diameters in the Nilson data. In the first place, if there is intrinsic scatter in the magnitude-diameter relation then, comparing two

systems of equal magnitude at a common distance, the intrinsically smaller will be smaller in apparent dimensions, and the tendency will be to produce a correlation in the sense observed. However, the scatter in the relationship when only Virgo cluster spirals observed by Holmberg are used (hence, there is no scatter from distance uncertainties, and the data set is homogeneous) is less than half our observed scatter (Heidmann 1967; Tully 1972). The scatter in Figure 1 must be predominantly observational, and the origin of the downturn in the Nilson data in intrinsic scatter can almost certainly be discounted.

TABLE 3—Continued

NGC/UGC	α	δ	ℓ	b	SGL	SGB	T	a_H^b	r_H	$B_T^{b,i}$	
N 3245	1024.5	2846	201.90	58.22	75.9	-22.3	-2A	4.7	0.69	11.70	
U 5671	1025.1	6703	141.81	44.74	44.9	1.3	10	2.5	0.45		KAR 69
U 5692	1026.8	7053	137.89	42.17	42.1	3.8	9	5.6	0.66	12.93	DDO 82
N 3270	1028.7	2507	209.06	58.57	79.8	-23.5	3X	4.5	0.32	12.88	
1028-36	1028.8	-3636	274.00	18.01	151.3	-37.9					
U 5741	1032.0	1127	232.62	54.16	93.6	-29.4	6	4.2	0.20	12.84	IC 622
N 3287	1032.1	2154	215.40	58.51	83.2	-24.5	7B	3.3	0.52	12.60	
U 5776	1034.6	6433	143.47	47.17	47.5	0.5	13 P	1.0	1.00	14.77	MARK 149, VII ZW 339
1035-25	1035.1	-2504	268.39	28.41	136.6	-37.4	1B	6.4	0.81		UGCA 213
N 3320	1036.6	4739	165.86	57.26	61.2	-9.5	6	3.4	0.50	12.70	
N 3347	1040.5	-3605	275.85	19.67	150.3	-35.7	3B	5.9	0.71	11.85	
N 3358	1041.3	-3608	276.02	19.71	150.3	-35.5	0X	7.5	0.52	12.17	
U 5897	1045.0	1122	235.75	56.80	95.2	-26.5	5A	4.2	0.38	12.97	
1045-20	1045.7	-2037	267.90	33.47	131.3	-34.7	3B	3.9	1.00		UGCA 218
1046+65	1046.1	6500	141.71	47.70	47.9	1.7	10	2.7	0.73		UGCA 220
N 3394	1047.2	6559	140.62	47.04	47.1	2.4	5A	3.1	0.82	12.58	
U 5945	1047.7	1750	225.47	60.51	89.0	-23.2	10B	3.0	0.47	14.42	
U 5950	1048.1	1535	229.60	59.61	91.3	-24.1	13	3.1	0.54		
U 5999	1050.4	753	242.25	55.83	99.3	-26.6	10	2.6	0.89		DDO 90
U 6016	1051.2	5434	153.13	55.40	56.8	-3.6	10	3.4	0.75		CONFUSED WITH NGC 3448
U 6018	1051.5	2052	220.27	62.48	86.5	-21.0	10	2.0	1.00	0.01	
N 3451	1051.7	2730	205.91	64.04	80.4	-17.8	6	3.0	0.52	13.20	
N 3464	1052.2	-2051	269.60	34.09	131.8	-33.2	5B	4.3	0.77	12.23	UGCA 222
N 3512	1101.3	2818	204.49	66.23	80.7	-15.6	5X	2.7	0.95	12.99	
U 6138	1101.9	2800	205.26	66.33	81.0	-15.6	9	3.1	0.54	14.31	
1102+29	1102.2	2924	201.78	66.48	79.8	-14.9	13 P	0.5	0.89		MARK 36, HARD 4
U 6185	1105.3	816	246.09	58.91	100.4	-23.1	8X	2.7	0.57	14.11	
U 6205	1107.1	4622	162.83	62.39	65.2	-5.8	9	2.9	0.80	14.44	
1108-09	1108.8	-942	266.33	45.67	119.7	-27.5	4X	2.7	0.84		UGCA 228
U 6253	1110.8	2225	220.18	67.22	87.1	-16.3	-5	11.0	0.91	12.38	DDO 93, KAR 77, LED II
1114-27	1114.8	-2732	278.70	30.60	140.0	-28.6	9B	3.0	0.65		UGCA 230
1116+51	1116.4	5146	152.19	60.08	61.2	-1.8					
N 3660	1121.1	-823	269.14	48.37	119.1	-24.2	4B	4.2	0.80		UGCA 234
N 3692	1125.8	941	251.13	63.58	100.9	-17.8	3	4.5	0.30	12.02	
1126+29	1126.6	2914	202.36	71.80	82.3	-10.2	-5	3.8	0.75		URSA MAJOR, PAL 4
U 6497	1127.4	3854	173.73	69.49	73.6	-6.0	7	3.5	0.21		
N 3729	1131.1	5325	146.62	60.27	60.7	0.9	1BP	4.6	0.67	11.86	
1132+57	1132.5	5705	142.28	57.37	57.5	2.7	10	2.3	0.55		UGCA 240
U 6596	1135.0	5625	142.41	58.11	58.2	2.7	10B	2.0	0.62		
U 6614	1136.6	1725	240.09	70.55	94.3	-12.7	1A	5.0	0.89	12.97	
1139+36	1139.6	3621	177.32	72.80	76.9	-4.8	13	3.1	0.95		UGCA 244
U 6684	1140.7	3145	192.55	74.55	81.2	-6.4	10	1.7	0.73	15.00	
U 6716	1142.0	3614	176.93	73.29	77.2	-4.4	4	2.9	0.95	14.20	
N 3883	1144.2	2057	233.09	73.89	91.6	-9.7	3A	4.5	0.91	12.70	
N 3906	1147.0	4842	148.23	65.56	66.0	1.3	7BP	2.7	1.00	13.62	
1151-12	1151.8	-1212	281.83	48.04	124.9	-17.7	10	2.9	0.54		UGCA 252
N 3963	1152.4	5846	136.50	57.13	57.0	5.7	4X	4.3	0.94	11.77	
U 6900	1153.0	3149	189.68	77.06	82.1	-4.0	10	3.1	0.64	14.40	DDO 101, KAR 82
1155-14	1155.8	-1428	284.23	46.19	127.4	-17.3	10	2.0	0.47		UGCA 256, DDO 104
1156-14	1156.0	-1415	284.21	46.41	127.2	-17.2	12 P	1.9	0.83		UGCA 258, DDO 103
U 6968	1156.1	2834	204.21	78.27	85.4	-4.5	12	4.4	0.39	13.75	
U 6973	1156.3	4300	153.97	71.10	71.9	0.7	2 P	4.9	0.53	12.52	IC 750
N 4025	1156.6	3804	165.53	74.69	76.6	-1.0	6B	4.2	0.64	13.62	DDO 107
U 6978	1156.7	-218	277.95	57.74	115.2	-14.1	10	2.2	0.65		
N 4026	1156.9	5114	141.93	64.21	64.3	3.7	-2	6.4	0.31	11.70	
1158-24	1158.0	-2427	288.49	36.71	137.8	-18.6	10	2.6	1.00		UGCA 261
											POSSIBLE CONF. W. UGCA 263

In the second place, there could be a coupling between two observed correlations. There is (i) a slight deficit of edge-on systems among the smaller systems in the sample of 535 Sbc-Sd galaxies compared with the expected number if galaxies are oriented randomly and their intrinsic flattening is 5 to 1 (see the discussion below concerning inclination uncertainties), and (ii) there is a tendency for face-on galaxies to lie to the left of the regression line. This latter effect would be explained if the corrections for internal absorption have been underestimated by $\sim 40\%$ (see § IIIe). The sense of coupling

is the following. Among the smaller galaxies in apparent dimensions there is a surplus of face-on systems, and these tend to lie at negative deviations from the regression line. Burstein (private communication) anticipated this coupling existed as an explanation for the downturn at small dimensions seen in both the Holmberg and Nilson data. However, if absorption corrections were increased by 40% for an individual galaxy, the maximum horizontal displacement in Figure 1 would be 0.075 in the log, and the typical displacement would be 0.03–0.04. This effect is much smaller than the

TABLE 3—*Continued*

NGC/UGC	α	δ	ℓ	b	SGL	SGB	T	a_H^b	r_H	$B_T^{b,i}$	
1158+48	1158.0	4803	145.27	67.09	67.3	2.7	10	1.6	0.90		UGCA 262
U 7000	1158.6	-101	277.86	59.11	114.1	-13.3	10B	1.9	0.83	14.10	POSSIBLE CONF. W. NGC 4030
N 4036	1158.9	6210	132.98	54.26	54.0	7.7	-2	5.0	0.60	11.40	
N 4050	1200.4	-1605	286.40	44.95	129.3	-16.5	3B	3.9	0.76	11.75	
U 7040	1201.3	2543	219.26	79.21	88.5	-4.4	8B	2.9	0.65	13.93	
N 4085	1202.8	5038	140.60	65.16	65.2	4.4	5X	3.7	0.41	12.42	POSSIBLE CONF. W. NGC 4088
N 4111	1204.5	4321	149.52	71.69	72.1	2.2	-2A	6.3	0.29	11.50	POSSIBLE CONF. W. UGC 7089
N 4124	1205.6	1039	269.56	70.39	103.2	-8.3	-2A	6.0	0.49	12.02	IC 3011
U 7136	1206.8	1417	264.04	73.61	99.8	-6.9	-5	3.3	0.80	13.85	IC 3019
U 7176	1208.4	5034	138.71	65.58	65.5	5.2	10	2.6	0.37		DDO 111
U 7186	1208.8	1818	255.44	77.03	96.1	-5.1	10	2.7	0.25	14.15	DDO 112
U 7189	1208.8	7506	126.46	42.03	41.7	12.3	8B	3.1	0.54	13.70	
U 7200	1209.7	1246	268.93	72.72	101.5	-6.7	9	2.9	0.85	14.28	
N 4185	1210.8	2847	201.45	81.46	86.3	-1.4	4	4.3	0.78	12.84	
N 4193	1211.3	1327	268.88	73.51	100.9	-6.1	5X	3.6	0.53	12.95	IC 3051
U 7254	1212.5	1344	269.26	72.90	100.8	-5.7	10	3.1	0.82	13.98	IC 3059, DDO 115
U 7255	1212.5	1419	268.16	74.40	100.2	-5.5	5	3.5	0.26	13.34	IC 3061
1212+36	1212.5	3630	161.05	78.06	79.1	1.4	10	1.7	1.00	0.01	UGCA 276, DDO 113, KAR 90
1212+09	1212.5	952	275.14	70.47	104.5	-6.9	10	1.6	0.90		UGCA 275
1212-35	1212.9	-3521	294.77	26.67	149.6	-17.0		5.2	0.56		
N 4212	1213.1	1411	268.88	74.36	100.4	-5.4	4A	4.8	0.79	11.80	
N 4222	1213.9	1335	270.59	73.54	101.0	-5.4	7	4.5	0.21	13.29	IC 3087
U 7326	1215.1	1240	273.04	73.27	102.0	-5.4	10	2.9	0.34	14.03	IC 3105
N 4246	1215.4	728	279.68	68.54	107.0	-6.9	5A	3.6	0.67	13.26	IC 3113
N 4248	1215.4	4741	138.69	68.68	68.6	5.4	13	5.0	0.42	13.19	
U 7339	1215.7	946	277.43	70.70	104.8	-6.1	10	2.6	0.54	14.59	IC 3118
U 7357	1216.6	2242	243.88	81.29	92.5	-2.0	5X	2.7	0.95	14.44	
N 4274	1217.4	2953	191.43	82.64	85.7	0.3	2B	8.7	0.40	10.70	
1218-34	1218.2	-3428	295.83	27.71	148.9	-15.8					
N 4289	1218.5	400	284.39	65.49	110.6	-7.1	5	5.5	0.17	13.04	POSSIBLE DET. ≥ 2500 KM/S
N 4294	1218.8	1147	277.14	72.85	103.1	-4.8	6B	4.3	0.49	12.26	POSSIBLE CONF. W. NGC 4299
N 4302	1219.2	1453	272.53	75.69	100.1	-3.8	5	7.7	0.32	11.79	TURN 61A CONFUSED WITH NGC 4298
U 7434	1219.6	2620	220.57	83.36	89.2	-0.3	8	3.1	0.32	14.50	
N 4330	1220.7	1139	278.77	72.91	103.4	-4.4	5	6.2	0.27	12.27	
N 4380	1222.8	1017	281.94	71.81	104.8	-4.3	2A	5.3	0.66	12.19	
U 7510	1223.0	1232	279.47	73.94	102.7	-3.6	9	3.3	0.24		IC 3311
U 7518	1223.3	750	284.54	69.51	107.2	-4.9	5	3.7	0.28	13.51	IC 3322
N 4388	1223.3	1256	279.18	74.33	102.3	-3.4	3 P	8.6	0.31	11.17	
N 4396	1223.4	1557	274.30	77.10	99.4	-2.5	8	5.0	0.40	12.55	
N 4402	1223.6	1323	278.81	74.78	101.9	-3.2	3	5.6	0.38	11.53	
N 4410	1223.9	918	283.70	70.95	105.8	-4.3	2 P	2.4	0.83	13.50	NGC 4410A
U 7548	1224.3	1327	279.32	74.90	101.9	-3.1	10	2.2	0.44	14.45	IC 3355, DDO 124
U 7550	1224.4	1156	281.36	73.49	103.3	-3.5		2.4	0.85	14.15	IC 3358
N 4441	1225.0	6505	127.11	52.13	52.0	11.3	-2XP	6.4	0.80	12.39	
N 4438	1225.3	1317	280.42	74.84	102.1	-2.9	0AP	10.5	0.52	10.85	ARP 120, VV 188
N 4462	1226.7	-2254	296.35	39.41	137.5	-11.9	2B	6.1	0.44	11.87	
U 7630	1227.1	1141	283.84	73.46	103.8	-2.9	10	2.5	0.70		IC 3418, DDO 130
1227-08	1227.7	-808	293.99	54.09	123.0	-8.2	4B	3.5	0.92		UGCA 282
N 4485	1228.2	4158	137.92	74.83	74.8	5.9	10B	3.3	0.94	12.32	AKP 269, VV 30, TURN 69A
N 4488	1228.3	838	287.42	70.61	106.8	-3.5	0BP	6.5	0.37	13.09	CONFUSED WITH NGC 4490
U 7674	1229.4	1227	284.98	74.36	103.2	-2.2	10	2.0	0.92	15.09	IC 3459
U 7692	1230.2	1303	285.05	74.99	102.7	-1.8	-5	4.2	0.93	13.95	IC 3475, DDO 132, KAR 154
U 7695	1230.2	1420	283.54	76.22	101.4	-1.4	9	4.0	0.80	13.23	IC 3476
1230-00	1230.6	-16	293.17	61.98	115.5	-5.4	10	1.7	1.00		UGCA 285, KAR 155
1230+11	1230.6	1137	286.81	73.64	104.1	-2.1	3XP	1.0	0.78	15.72	IC 3483, VV 43
U 7710	1231.2	-222	294.10	59.93	117.6	-5.8	10	2.3	0.94		DDO 134

amplitude of the downturn in the Nilson data, and consequently the test illustrated by Figure 2 stands as evidence in favor of Holmberg dimensions.

However, there is rather convincing evidence that contradicts our conclusion in the microphotometry of galaxies in the vicinity of the Coma cluster by Aaronson *et al.* (1980). Those authors found good agreement between their microphotometer dimensions and UGC values over a wide range of apparent sizes. Consequently, we do not feel at all confident that we have resolved the question of which diameter system is correct.

Likewise, there is a difficulty evident when an intercomparison is made of the ratio of minor to major diameters determined by various investigators. Holmberg ratios systematically suggest that galaxies are more *face-on* than do ratios derived from the UGC, MCG, or BGC. There is *tentative* evidence from structural characteristics such as spiral arms or rings that suggest the Holmberg ratios systematically underestimate the inclination.

Inclinations for late systems are particularly poorly determined. Histograms are given in Figure 3 which

TABLE 3—*Continued*

NGC/UGC	α	δ	ℓ	b	SGL	SGB	T	a_H^b	r_H	$B_T^{b,i}$	
1231-10	1231.3	-1023	295.92	51.97	125.4	-7.9	9	2.7	0.57		UGCA 287
N 4533	1231.8	236	292.85	64.86	112.8	-4.3	9	3.8	0.20	13.34	PROBABLE CONF. W. NGC 4536
N 4540	1232.3	1550	283.64	77.80	100.2	-0.5	6X	3.3	0.83	12.24	
N 4569	1234.3	1326	288.47	75.62	102.6	-0.7	2X	11.7	0.50	9.91	CCNFUSED WITH LOCAL EMISSION
1234+39	1234.8	3901	136.39	78.01	76.0	6.4	10 P	1.3	0.74		UGCA 290, ARP 211, VV 42
U 7795	1235.2	723	293.09	69.72	108.5	-2.2	10	2.2	0.79	14.93	DDO 139
U 7808	1236.1	1045	292.06	73.07	105.3	-1.1	3	5.0	0.19	13.93	IC 3608
N 4593	1237.0	-504	297.45	57.40	120.6	-5.1	3B	5.1	0.65	11.35	
U 7834	1238.3	1045	293.90	73.16	105.4	-0.5	10	2.9	0.65	14.16	IC 3647, KAR 180
N 4607	1238.7	1209	293.51	74.56	104.1	-0.1	3B	4.2	0.33	13.08	
N 4633	1240.1	1438	293.34	77.06	101.8	1.0	7B	3.4	0.47	13.44	IC 3688
											CONFUSED WITH NGC 4634
N 4634	1240.2	1434	293.49	77.00	101.9	1.0	7	4.3	0.35	12.55	CONFUSED WITH NGC 4633
U 7883	1240.4	-57	298.48	61.57	116.8	-3.2	6	4.7	0.35	13.01	
U 7919	1242.4	1219	296.83	74.84	104.2	0.9	-5	4.2	0.64		IC 3720, DDO 145
1244+26	1244.3	2650	241.22	88.80	90.3	5.2	-5 P	1.5	0.70	14.70	A 1244
1244+36	1244.5	3649	128.48	80.53	80.6	7.7		1.8	0.71		IC 3772
N 4682	1244.7	-948	301.25	52.79	125.7	-4.5	6	4.4	0.58		
N 4689	1245.3	1402	299.13	76.60	102.7	2.0	5A	5.9	0.95	11.58	PROBABLE DET. 1550 KM/S
1246-03	1246.7	-344	301.89	58.86	120.0	-2.5	10	2.7	0.37		DDO 149
N 4705	1246.9	-455	302.02	57.68	121.1	-2.7	4X	4.4	0.37		
N 4712	1247.2	2544	289.36	88.28	91.6	5.5	4A	3.7	0.43	13.16	CONFUSED WITH NGC 4725
U 7982	1247.3	308	301.97	65.73	113.4	-0.5	12	4.8	0.31	13.08	POSSIBLE DET. 1200 KM/S
U 7995	1248.2	7839	123.05	38.75	38.5	15.1	10	3.1	0.86		
N 4771	1250.8	132	304.03	64.13	115.2	-0.1	7A	5.6	0.29	11.89	
N 4779	1251.3	959	304.89	72.57	107.0	2.3	4B	3.3	0.87	12.87	
N 4818	1254.3	-815	305.25	54.33	124.8	-1.8	2X	5.4	0.41	11.12	
N 4845	1255.4	150	306.70	64.39	115.2	1.1	1A	7.1	0.32	11.30	
U 8081	1255.6	1508	310.46	77.64	102.3	4.7	9	1.7	0.82		DDO 157
U 8107	1257.5	5337	120.15	63.74	64.3	13.2	10B	3.9	0.48	13.80	
N 4904	1258.4	14	308.14	62.74	116.9	1.4	6B	3.7	0.66	12.49	POSSIBLE DET. 1200 KM/S
U 8155	1300.7	804	311.69	70.47	109.5	4.1	12 P	4.7	0.89	13.00	
N 4941	1301.6	-517	308.79	57.17	122.4	0.7	2X	6.4	0.66	11.66	UGCA 321
N 4948	1302.3	-740	308.72	54.79	124.8	0.2	7B	2.5	0.39		POSSIBLE DET. 600 KM/S
N 4958	1303.2	-744	309.10	54.70	124.9	0.4	-2B	5.9	0.37	11.30	PROBABLE CONF. W. 1302-07
1304-23	1304.4	-2351	307.51	38.62	140.5	-3.7	7X	2.7	0.66		UGCA 325
U 8211	1305.3	5240	117.24	64.55	65.4	14.2	5	2.2	0.86	15.23	
U 8253	1308.2	1200	320.23	73.95	106.2	6.9	9	2.6	0.94		
N 5005	1308.5	3719	101.72	79.27	81.1	12.5	4X	8.1	0.58	10.42	
N 5020	1310.2	1252	322.88	74.64	105.4	7.5	4X	4.8	0.86	12.30	
1310+41	1310.5	4143	107.30	75.02	76.7	13.6	5	1.4	0.89		UGCA 336
1310+42	1310.7	4204	107.59	74.68	76.4	13.7	10	1.7	0.91		UGCA 337
1312+42	1312.9	4216	106.40	74.36	76.2	14.1	10	2.6	0.43		UGCA 342
N 5073	1316.7	-1436	312.94	47.47	132.4	1.7	5	4.9	0.22		UGCA 346
1317-22	1317.1	-2200	311.53	40.14	139.5	-0.4	5XP	2.8	0.73		UGCA 348
U 8398	1318.6	4259	103.85	73.30	75.6	15.2	10	1.7	0.73		
1322+42	1322.6	4245	101.21	73.20	76.0	15.9	10	1.3	1.00	0.01	UGCA 354
1322+45	1322.6	4508	104.50	71.04	73.5	16.2	9	1.1	0.85		UGCA 355
N 5174	1326.9	1116	333.72	71.57	108.0	11.1	5	5.3	0.58	12.25	NGC 5175
N 5172	1326.9	1718	345.86	76.64	102.0	12.5	4X	4.8	0.61	12.41	
1330-24	1330.2	-2425	314.80	37.24	142.8	1.8					
1330-42	1330.3	-4204	311.13	19.88	159.5	-3.7					POSSIBLE DET. CONF. W. LOCAL HI
N 5216	1330.4	6257	115.05	53.81	54.9	18.1	-5 P	4.8	0.70	13.23	ARP 104, VV 33
N 5218	1330.5	6301	115.06	53.74	54.9	18.2	3BP	3.1	0.82	13.04	ARP 104, VV 33
1330+50	1330.6	5005	106.47	65.96	68.5	17.9	10	1.7	0.64		UGCA 361
N 5211	1330.6	-46	324.24	60.11	120.1	8.9	3X	3.7	0.73	13.00	

show the distribution of observed axial ratios for all galaxies of intermediate and late morphological types observed by us or others with redshifts less than 3000 km s⁻¹. The histogram of types 5 ≤ T ≤ 6 (Fig. 3c) is representative of types other than very late. The distribution is roughly what is anticipated if galaxies are intrinsically flattened 5 to 1 and viewed at random orientations (in fact, there is probably a slight deficiency of very edge-on systems, with the deficiency most significant at small angular sizes). With late systems which are intrinsically large, the same statement can be made (Fig. 3b). By contrast, among the smaller galaxies typed T ≥ 8 there is a distinct lack of systems observed to be very flattened (Fig. 3a). However, *some* systems do exist

as flat as any of early type, and the evidence from kinematic studies (e.g. Tully *et al.* 1978) is that the gas in dwarf irregulars does lie in a rotating disk. It will be assumed that the intrinsic flattening of dwarfs is the same as that for luminous disk systems, but the consequence will surely be that we systematically *underestimate* the inclinations of members of this class.

There has been an attempt to correct dimensions for the effects of absorption in our Galaxy but not for the tilt of the external galaxy. It was noted that the points lying farthest to the left of the mean relationship in Figure 1 were inevitably at low galactic latitude. In Figure 4, deviations from the mean magnitude-log diameter line are plotted as a function of galactic absorption,

TABLE 3—Continued

NGC/UGC	α	δ	ℓ	b	SGL	SGB	T	a_H^b	r_H	$B_T^{b,i}$		
1332-12	1332.0	-1205	319.20	49.16	131.1	6.0	10	2.3	0.68		UGCA 364, KAR 227	POSSIBLE DET. 1500 KM/S
N 5221	1332.5	1405	342.46	73.26	105.6	13.1	3 P	4.4	0.30	13.01	ARP 288, VV 315	
U 8577	1333.1	4501	99.34	70.31	73.8	18.0	9	2.2	0.30			
1333-29	1333.8	-2900	314.63	32.56	147.4	1.1	10	2.6	0.51		UGCA 365	
N 5239	1333.9	738	333.35	67.55	112.1	11.9	48P	3.3	0.96	13.62		
U 8601	1334.4	4800	102.79	67.58	70.7	18.5	9	1.9	0.50			
U 8604	1334.4	6633	115.97	50.23	51.1	18.4	5X	2.6	0.83	14.44		
U 8659	1338.7	5541	108.81	60.33	62.6	19.3	10	1.9	0.92			
1339+43	1339.2	4332	94.14	70.55	75.5	19.0	10	1.4	0.89		UGCA 371	
U 8670	1339.5	4108	89.18	72.79	78.0	18.9	7X	1.9	1.00	15.11		
1344+41	1344.7	4133	87.72	71.83	77.6	19.9	10	1.4	0.66		UGCA 373	
U 8721	1345.3	4036	85.29	72.43	78.6	20.0	8X	2.0	0.70			
U 8726	1345.6	4044	85.47	72.29	76.5	20.0	6	3.5	0.29	14.13		
U 8740	1347.1	429	336.71	63.22	116.0	14.3	2X	3.1	0.95	13.42		
U 8775	1349.9	5113	101.33	63.55	67.3	21.0	6	2.3	1.00	13.80	IC 951	
1350+39	1350.2	3937	80.80	72.28	79.7	20.8						
N 5356	1352.4	535	340.50	63.48	115.3	15.8	3	4.4	0.33	12.86		
U 8856	1353.8	3020	48.53	75.53	89.7	20.8	13	2.5	0.27	15.19		
N 5389	1354.5	5959	108.56	55.55	57.9	21.2	0X	6.4	0.31	12.73		
1355+43	1355.4	4309	86.86	69.30	76.0	21.9	10	1.7	1.00	0.01	UGCA 377	
N 5395	1356.5	3740	73.16	72.50	81.9	22.0	3AP	4.4	0.48	12.01	ARP 84, I ZW 77, VV 48	
U 8914	1357.3	5236	100.85	61.77	65.8	22.1	10	1.7	1.00	0.01		
N 5403	1357.8	3825	74.81	71.89	81.1	22.2	3	4.7	0.26	13.08	VV 310	
N 5422	1358.9	5524	103.50	59.28	62.8	22.2	0	5.1	0.23	13.01		
U 8936	1359.0	4938	96.59	64.03	65.0	22.5	10	2.3	0.81			
N 5443	1400.5	5603	103.78	58.61	62.0	22.3	3B	4.8	0.39	12.22		
U 8959	1400.5	6908	113.78	46.97	48.1	20.6	9	2.9	0.80			
N 5440	1400.8	3500	63.82	72.90	84.8	22.7	1	5.0	0.55	12.60		POSSIBLE DET. 3000 KM/S
U 8987	1401.9	1634	4.05	69.96	104.6	20.6	9B	5.3	0.21	13.48		
N 5477	1403.8	5442	101.60	59.49	63.5	22.9	9	3.0	0.76	14.26	DDD 186	
N 5470	1404.0	616	346.54	62.36	115.4	18.8	3	3.9	0.23	13.17		
1404+44	1404.6	4441	86.80	67.05	74.3	23.6	10	1.6	0.90		UGCA 385	
1405+44	1405.6	4440	86.47	66.92	74.3	23.8						
U 9050	1406.6	5127	96.97	61.86	66.9	23.6	10	2.2	1.00	0.01		
U 9068	1408.3	4833	92.35	63.87	70.1	24.1	8A	2.7	0.63			
U 9073	1408.7	2544	32.20	72.12	95.0	23.5	5	2.7	0.79	13.95	IC 4381	
N 5533	1414.0	3534	62.60	70.18	84.4	25.4	2A	5.6	0.58	12.43		
N 5560	1417.5	413	349.23	58.65	118.4	21.5	38P	5.6	0.29	12.27	ARP 286	
N 5579	1418.3	3525	61.42	69.39	84.6	26.2	6XP	3.0	0.71	13.85	ARP 69, VV 142	
N 5577	1418.7	340	348.99	58.04	119.0	21.7	4A	4.7	0.35	12.58		
U 9245	1423.8	5633	99.45	56.31	61.0	25.5	7B	3.3	0.78	14.02	DDD 191	
1432-13	1432.8	-1331	337.90	41.96	137.6	19.5	9B	1.9	0.75		UGCA 391	
1435+45	1435.9	4524	80.41	62.19	73.1	29.1	13	1.4	0.43		UGCA 392	
U 9452	1437.6	5408	93.86	56.70	63.2	27.9	9	2.3	0.42			
U 9452	1437.8	5406	93.78	56.70	63.3	27.9	9	2.3	0.42			
N 5719	1438.4	-7	351.21	51.96	124.5	25.3	2XP	5.0	0.43	12.57		POSSIBLE CONF. W. NGC 5713
U 9508	1443.5	4919	85.70	58.98	68.4	29.7	10A	2.2	0.72			
N 5750	1443.7	-1	352.90	51.15	124.8	26.6	0B	4.8	0.61	12.39		
U 9537	1446.4	3512	57.67	63.85	84.7	32.0	3	3.8	0.27	13.66		
1448-20	1448.5	-2015	337.43	34.26	145.8	20.1	9B	2.8	0.62		UGCA 395	
N 5777	1450.0	5910	98.19	52.02	57.2	28.2	3	5.0	0.19	12.96		PRCBABLE CONF. W. UGC 9570
U 9570	1450.2	5909	98.14	52.01	57.3	28.2	9	2.5	0.88			
N 5774	1451.2	347	359.41	52.49	121.3	29.5	7X	4.3	0.86	12.68		CONFUSED WITH NGC 5775
U 9567	1452.8	3102	48.17	62.83	89.6	33.5	9	1.9	0.67			
U 9632	1456.4	5359	90.56	54.65	62.6	30.6	7A	2.5	0.76	14.85		

A_b (this latter parameter is defined in § IIIe). This empirical correlation implies a very steep dependence on latitude: at $|b| \sim 30^\circ$ a typical adjustment is only 4%, while at $|b| \sim 20^\circ$ the adjustment is $\sim 11\%$, and by $|b| \sim 10^\circ$ the adjustment is $\sim 70\%$. Consequently, for galaxies at high galactic latitudes the correction is negligible.

Very close to the plane, the correction can become unrealistically large. Presumably, galaxies that are cataloged at very low galactic latitudes lie in regions of relatively low obscuration. Consequently, the largest correction to diameters that is applied is $f_a = 2.0$.

The RC2 recommends a correction for tilt (see also the BGC; Heidmann, Heidmann, and de Vaucouleurs

1971; Dickel and Rood 1978), but the proposition has been disputed (Tully 1972) because of the difficulty in disentangling corrections to magnitudes and diameters. We feel the matter still has not been resolved and adopt the extreme position of no correction.

e) Apparent Magnitudes

In column 8, line 1, are *apparent magnitudes*, $B_T^{b,i}$, corrected for galactic absorption by an amount, A_b , and inclination by an amount, A_i . The *total absorption correction*, $A_b + A_i$, is given in column 8, line 2.⁴ The

⁴ A_i could not be calculated if dimensions or types were unknown.

TABLE 3—Continued

NGC/UGC	α	δ	l	b	SGL	SGB	T	a_H^b	r_H	$B_T^{b,i}$
U 9647	1457.5	3302	52.43	61.79	87.1	34.4	9	2.7	0.68	14.43
1459+50	1459.1	5003	84.33	56.46	66.9	32.0	10	1.7	0.64	UGCA 399
U 9682	1501.9	-39	357.21	47.51	127.1	30.8	9	3.0	0.38	
U 9733	1506.0	8123	117.13	34.40	34.4	20.2	10	1.7	0.82	
N 5874	1506.4	5456	90.47	52.92	61.1	31.7	5A	3.9	0.68	13.14
1506-10	1506.7	-1030	349.09	39.51	138.2	28.3	3BP	3.0	0.95	UGCA 400
N 5875	1507.7	5244	87.18	53.94	63.4	32.6	3	3.9	0.54	12.59
U 9749	1508.2	6723	104.97	44.84	47.8	27.1	-5	31.6	0.66	12.39
U 9784	1512.6	6252	99.67	47.52	52.2	29.4	10	2.3	0.68	DDC 199, URSA MINOR
U 9792	1513.6	5	0.88	45.85	127.4	33.8	-5	15.5	0.88	
U 9794	1513.8	1042	13.98	52.13	114.9	36.6	9B	4.4	0.33	
N 5905	1514.0	5542	90.56	51.60	59.8	32.4	3B	6.5	0.79	12.35
U 9803	1515.2	2936	45.74	57.93	91.1	38.4	10	1.7	1.00	12.54
N 5908	1515.3	5535	90.24	51.50	59.8	32.6	3AP	4.4	0.48	
1518-23	1518.3	-2328	341.90	27.67	152.4	24.6	5	4.1	0.82	
N 5930	1524.3	4151	67.86	55.31	75.3	38.3	3XP	3.1	0.45	12.67
1524-11	1524.4	-1158	351.93	35.52	141.9	31.5	7	1.7	0.91	UGCA 409
N 5949	1527.2	6455	100.56	44.99	49.2	29.9	5A	3.5	0.53	12.43
N 5945	1528.0	4305	69.69	54.38	73.6	38.7	2B	5.1	0.78	12.58
U 9896	1531.4	6744	103.31	42.95	46.2	28.8	5	2.6	0.77	13.63
U 9899	1531.7	6825	104.02	42.50	45.5	28.5	5	2.0	0.85	13.52
N 5981	1536.8	5933	93.21	47.00	54.1	33.5	5	4.2	0.20	12.77
U10009	1543.1	419	11.83	42.57	125.2	42.1	10	1.9	0.42	12.85
U10031	1544.5	6145	95.31	45.10	51.2	33.2	9B	2.7	0.89	
N 5996	1544.7	1802	29.50	48.63	106.7	45.1	12BP	2.7	0.52	
U10090	1553.1	6113	93.97	44.44	51.1	34.4	9	1.7	1.00	12.80
U10105	1555.4	5851	90.77	45.19	53.3	35.5	10	2.2	0.79	
U10140	1559.6	1853	32.51	45.63	105.7	48.6	10	1.7	1.00	
U10214	1605.0	5533	85.74	45.15	55.8	38.8	5BP	5.8	0.27	12.80
U10266	1610.4	4902	76.43	45.96	62.5	43.1	9	2.2	0.58	13.97
U10312	1615.5	3119	50.98	45.24	86.0	50.9	12	2.7	0.68	
N 6109	1615.7	3507	56.37	45.65	80.2	49.9	13 P	1.7	1.00	14.53
U10334	1616.7	6358	95.83	40.83	46.4	34.8	10B	2.6	0.54	14.67
U10376	1622.6	6533	97.43	39.64	44.5	34.1	9	2.5	0.94	DDC 205
U10401	1626.0	5700	86.53	41.95	52.0	40.3	9	2.3	0.61	
1635+66	1635.6	6619	97.75	38.13	42.7	34.5	-5			
N 6223	1642.5	6140	91.78	38.76	45.8	38.5	13 P	5.0	0.74	12.09
U10565	1646.9	4849	75.20	40.04	57.7	48.0	10	1.7	0.91	VII ZW 657
1648-03	1648.9	-301	15.25	24.80	145.5	54.1	3B	3.3	0.91	
N 6240	1650.5	229	20.73	27.28	137.3	57.2	13 P	4.0	0.46	
U10605	1653.0	8323	116.28	30.45	30.3	21.3	10	2.6	0.88	13.64
U10642	1657.3	-28	18.85	24.33	143.5	57.3	-5	20.5	0.54	13.04
U10676	1701.8	2635	47.86	34.33	89.1	62.0	10	3.2	0.54	13.61
U10770	1712.5	5923	88.18	35.51	43.8	42.5	9BP	2.7	0.46	
U10791	1715.5	7227	103.72	33.02	35.1	31.4	9	3.6	1.00	
U10795	1716.2	3058	53.92	32.46	77.7	63.1	10	2.7	0.60	14.00
U10809	1717.8	2458	47.30	30.41	90.1	65.9	13	2.4	0.42	15.01
U10822	1719.4	5758	86.37	34.72	43.8	44.2	-5	37.7	0.64	11.71
U10903	1731.7	2354	47.33	27.07	90.1	69.2	10	1.8	0.64	
U10910	1732.9	3357	58.34	29.81	67.6	64.3	10	2.3	1.00	
U10921	1735.7	1724	41.01	23.83	108.5	71.5	10	1.8	0.82	DDC 208, DRACO
U10958	1741.8	6653	96.81	31.60	35.4	37.4	9	2.5	0.70	
U11027	1751.2	2435	49.74	23.14	82.5	73.0	10	2.9	0.68	
U11039	1752.9	1833	43.87	20.51	103.0	75.4	10	1.9	1.00	14.81
U11081	1758.0	8108	113.10	29.01	29.1	24.2	10	1.7	0.82	13.56
U11109	1802.8	4645	74.00	27.19	42.6	57.2	10	2.0	0.92	

magnitudes are in the total blue magnitude system introduced in RC2, although the corrections differ from those in RC2. By preference, the sources for B_T magnitudes are the RC2, the CGCG, and corrected Harvard magnitudes (from the BGC). The Zwicky magnitudes, m_Z , require a correction dependent on the apparent areas of the images $a_H^2 r_H$ (Balkowski *et al.* 1974):

$$B_T = 0.81m_Z + 2.55, \quad a_H^2 r_H < 5; \quad (7a)$$

$$B_T = 0.60m_Z + 5.15, \quad 5 \leq a_H^2 r_H < 8; \quad (7b)$$

$$B_T = 0.62m_Z + 4.55, \quad 8 \leq a_H^2 r_H < 16; \quad (7c)$$

$$B_T = 0.47m_Z + 6.05, \quad a_H^2 r_H \geq 16; \quad (7d)$$

where area is in square arc minutes. The coefficients are slightly different from those given by Balkowski *et al.* (1974) because the corrections are to the B_T system rather than the Holmberg system. The Harvard magnitudes as corrected in the BGC, m_c , received the following adjustment:

$$B_T = 0.99m_c - 0.19. \quad (8)$$

TABLE 3—Continued

NGC/UGC	α	δ	ℓ	b	SGL	SGB	T	a_H^b	r_H	$B_T^{b,i}$	
U11111	1803.3	2307	49.36	20.02	82.1	76.1	9B	2.2	0.85		POS. CONF. W. UGC 11113 + COMP.
U11125	1805.8	1141	38.66	14.84	134.3	77.9	5	3.3	0.72	13.64 IC 4688	
U11224	1822.4	3646	64.56	20.97	43.0	67.8	10	2.1	1.00		
N 6632	1823.0	2730	55.43	17.56	55.7	76.3	4A	5.1	0.48	11.84	
U11279	1832.2	3705	65.65	19.25	37.7	68.0	10	1.9	0.91		
U11291	1834.1	3047	59.57	16.56	41.7	74.2	7	3.9	0.31	13.62	
U11303	1835.7	3314	62.07	17.17	38.4	72.0	3	2.6	0.58	13.75	
U11321	1838.7	4413	73.16	20.46	32.0	61.2	10	2.5	0.87		
U11392	1900.5	3443	65.58	13.03	21.9	70.8	10	2.3	0.27		
U11400	1903.2	7858	110.71	26.18	26.2	26.6	10	2.0	0.59		
N 6789	1916.3	6354	94.99	21.52	23.3	41.5	10	3.1	1.00	12.66	
N 6792	1919.4	4302	74.91	13.19	16.4	62.0	3B	5.0	0.58	12.20	
1943-23	1943.6	-2318	17.27	-21.99	224.8	49.1	10	3.6	0.87		UGCA 415
U11482	1946.9	702	46.06	-9.43	265.4	74.2	10	5.7	0.45	13.76	
U11496	1953.0	6733	100.10	19.38	19.6	37.2	9	3.9	1.00		
U11498	1954.8	545	45.90	-11.77	265.5	71.9	3B	7.1	0.38	12.19	
U11582	2028.6	2007	62.77	-11.11	311.5	66.8	9	5.0	0.61	13.39	
N 6926	2030.5	-211	43.25	-23.44	262.5	60.0	10	3.5	0.70	12.60	
U11635	2046.0	7958	113.55	22.18	21.6	24.4	4	5.3	0.43	12.55	
2143-21	2143.8	-2128	30.53	-47.67	256.4	34.0	-5	6.0	1.00		UGCA 421, CAPRICORNUS
U11841	2150.8	3842	88.98	-11.89	336.3	44.6	8	6.3	0.15		
U11878	2200.0	1805	76.16	-28.81	306.9	45.2	12 P	2.4	0.81	14.19	
2208-10	2208.7	-1041	49.00	-48.84	271.4	34.8					
N 7241	2213.4	1859	79.58	-30.24	308.5	42.1	4BP	5.2	0.30	12.32 II ZW 174	PEC. PROF. 1446 KM/S, CONF. W. U119647
U11973	2214.7	4115	94.29	-12.62	337.9	39.7	4X	6.6	0.34	11.77	
U11979	2216.0	4528	96.90	-9.26	343.0	38.2	9B	5.9	1.00		
N 7253	2217.2	2908	87.36	-22.80	322.1	41.2	13 P	3.1	0.49	13.83 ARP 278, VV 242	
U12015	2221.0	1936	81.64	-30.50	309.4	40.4	7X	2.3	0.86	14.97	POSSIBLE DET. 3200 KM/S
N 7280	2224.1	1554	79.56	-34.24	304.7	39.3	-2	3.5	0.71	12.76	
N 7303	2229.2	3042	90.65	-23.00	323.8	38.5	12 P	2.8	0.77	12.91 NGC 7304	
2234-25	2234.3	-2530	28.82	-59.88	260.1	22.2	9A	3.0	0.90		UGCA 430
2234-40	2234.7	-843	57.09	-53.21	276.7	29.9	10	1.7	0.82		
2245-40	2245.8	-4047	357.11	-61.40	247.9	12.0					UGCA 431
U12206	2247.2	3306	95.55	-22.94	326.5	34.6	1B	5.2	0.61	13.58	
N 7421	2254.1	-3736	2.76	-63.85	251.6	12.3	2B	4.1	1.00	12.63	
2257+25	2257.8	2550	93.87	-30.42	317.8	32.3				14.93	
2304+12	2304.2	1228	87.07	-42.72	302.5	29.1	-5	2.9	1.00	14.07 UGCA 435, PAL 13, PEGASUS	DET. -383 KM/S, POS. MAG. STR.7
N 7490	2305.0	3206	98.69	-25.56	325.2	30.8	4	4.6	0.94	12.05	
U12388	2306.0	1233	87.63	-42.89	302.7	28.7	7	2.9	0.44		
U12411	2309.8	4832	106.57	-10.88	344.0	28.6	9	5.5	0.14		
2310-37	2310.0	-3728	0.91	-66.91	253.3	9.6	5	2.9	0.47		
N 7515	2310.3	1224	88.76	-43.56	302.8	27.7	12	2.7	0.84	13.35	
U12423	2310.6	608	83.99	-48.89	296.0	26.2	5	5.2	0.19	12.82 TURN 137B	
N 7513	2310.6	-2837	24.00	-68.28	261.4	13.6	3B	4.2	0.80	12.46 UGCA 437	
U12477	2314.7	1825	93.86	-38.80	309.7	27.7	-2 P	3.4	0.70		NGC 7578A,B, ARP 170, VV 181
N 7599	2316.6	-4232	348.09	-65.90	249.4	6.1	5B	5.8	0.42	11.48 IC 5308	
2323-32	2323.7	-3240	11.87	-70.84	258.9	9.3	10	2.3	0.81		PROBABLE CONF. W. NGC 7590
N 7664	2324.2	2448	99.69	-33.94	317.1	26.3	5	4.9	0.59	12.36 UGCA 438, UKS 2323-326	
N 7685	2328.0	337	87.64	-53.34	294.5	21.4	5	3.0	0.86	14.00	
2333+18	2333.0	1802	98.79	-40.98	310.0	23.3	10A	1.4	0.77	15.02 UGCA 440	
N 7711	2333.1	1502	97.23	-43.75	306.8	22.7	-2 P	6.0	0.45	13.08	
2340-45	2340.0	-4527	335.68	-67.33	248.6	1.1	7	4.7	1.00		A 2340
U12776	2343.7	3306	107.60	-27.54	326.6	22.7	3BP	4.4	0.80	12.99	
U12893	2357.9	1657	105.91	-43.95	310.1	17.3	8A	3.1	0.91	13.86	POSSIBLE DET. 1000 KM/S

It must be cautioned that the photoelectric magnitudes in the B_T system involve aperture corrections which create a vulnerability to systematic errors if there are systematic errors in diameters as suggested in the previous section. Note that for both diameters and magnitudes the errors might be distance dependent. There is also the *possibility* of systematic errors related to inclination since the RC2 dimensions are adjusted for tilt, and, hence, the aperture corrections leading to the B_T magnitudes are modified as a function of tilt.

The magnitudes are corrected for absorption in the observed galaxy, A_i , and in our Galaxy, A_b :

$$B_T^{b,i} = B_T - A_i - A_b. \quad (9)$$

These corrections are described immediately below.

i) Corrections for Internal Absorption

Magnitudes are adjusted to account for internal absorption as a function of inclination, i , by an amount A_i :

$$A_i = -\alpha [\ln(e^{-\sec i} + \beta) + 1]. \quad (10)$$

The coefficients have the values $\alpha=0.3$ and $\beta=0.01$ for $1 \leq T \leq 12$ (otherwise $\alpha=0$). The formalism for the correction may look elaborate, but it reduces to two simple

TABLE 4
ALTERNATE NAMES

Designation	Common Name Or Source
M	Messier
IC	Index catalog
UGCA	<i>Catalogue of Selected Non-UGC Galaxies</i> (Nilson 1974)
A, NGC xxxx A	Anonymous (BGC)
Holmberg, Ho	Holmberg (1958)
Arp	<i>Atlas of Peculiar Galaxies</i> (Arp 1966)
Mark	Markarian and Lipovetskii (1967–1974)
Zw, Zw compact	Zwicky (1971 and privately circulated lists)
VV	<i>Atlas and Catalogue of Interacting Galaxies</i> (Vorontsov-Velyaminov 1959)
Arak	Arakelian (1975)
DDO	van den Bergh (1959, 1966)
Haro	Haro (1956)
Turn	Turner (1976)
Kar	Karachentseva (1968)
Maffei	Maffei (1968)
ScI	ScI galaxies (Rubin <i>et al.</i> 1976)
RMB	Rubin, Moore, and Bertiau (1967)
M81 dw A, etc.	Lo and Sargent (1979)
Phoenix	Canterna and Flower (1977)
Sag DIG	Cesarsky <i>et al.</i> (1977)
ScI DIG	Laustsen <i>et al.</i> (1977)
UKS	United Kingdom Schmidt (Longmore <i>et al.</i> 1978)
Other Names	Refer to RC2

regimes which have some physical sense:

$$A_i \approx \alpha(\sec i - 1), \quad i \text{ small};$$
$$A_i \approx \text{constant}, \quad i \text{ large}.$$

The face-on limit is the standard secant law which describes the absorption of light arising from *within* or *behind* the obscuring region. The correction is to “face-on” rather than to “absorption free.” The edge-on limit can be interpreted as the flux from sources *in front* of all obscuring matter, for example, from the front side of a halo or bulge.

The coefficient $\beta=0.01$ was chosen to give a break in the secant law in agreement with Holmberg’s (1958) data on Sc galaxies (see Fig. 4 in that paper). The break from the small i to the large i regime occurs at $i \approx 77^\circ$.

TABLE 5
COEFFICIENTS OF THE MAJOR DIAMETER TRANSFORMATIONS

Source	c_i	k_i
Nilson:		
Sb-Im	0.85	0.24
SO-Sab, IO	0.73	0.33
Vorontsov-Velyaminov:		
Sb-Im	0.83	0.31
SO-Sab, IO	0.67	0.41
de Vaucouleurs:		
Sb-Im	0.87	0.28
SO-Sab, IO	0.86	0.37

Holmberg (1958) proposed that the amplitude parameter, α , was type dependent, being greater for earlier spirals. Heidmann, Heidmann, and de Vaucouleurs (1971) suggest the coefficient is independent of type for Sa through Sc galaxies. Fisher and Tully (1975) found evidence that the obscuration in dwarf galaxies is comparable with that found in Sc systems. We adopt $\alpha=0.3$ for types $1 \leq T \leq 12$, and $\alpha=0$ for early systems and peculiars. Both the value of the coefficient and the assumption regarding a type dependence are uncertain. There was evidence in § III d that $\alpha \sim 0.4$ would be more appropriate for $4 \leq T \leq 7$. On the other hand, if dimensions had been adjusted as a function of inclination (see § III d), then the coefficient would require reduction in compensation (Tully 1972; Dickel and Rood 1978). With $\alpha=0.3$ our corrections are quite similar to those in the RC2 for $i < 60^\circ$ and by Sandage and Tammann (1974) for $i < 60^\circ$ and $i \approx 90^\circ$. Our corrections exceed those in the RC2 by up to 0.5 mag for $i > 60^\circ$ (but diameters are adjusted in RC2) and exceed those by Sandage and Tammann by up to 0.2 mag in the interval $60^\circ < i < 85^\circ$. The respective corrections are illustrated in Figure 5.

ii) *Corrections for Galactic Obscuration*

Magnitudes are corrected for obscuration within our Galaxy by the amount A_b :

$$A_b = -0.149 + 6.41 \times 10^{-4} N_H, \quad (11)$$

where the local neutral hydrogen flux N_H is given by

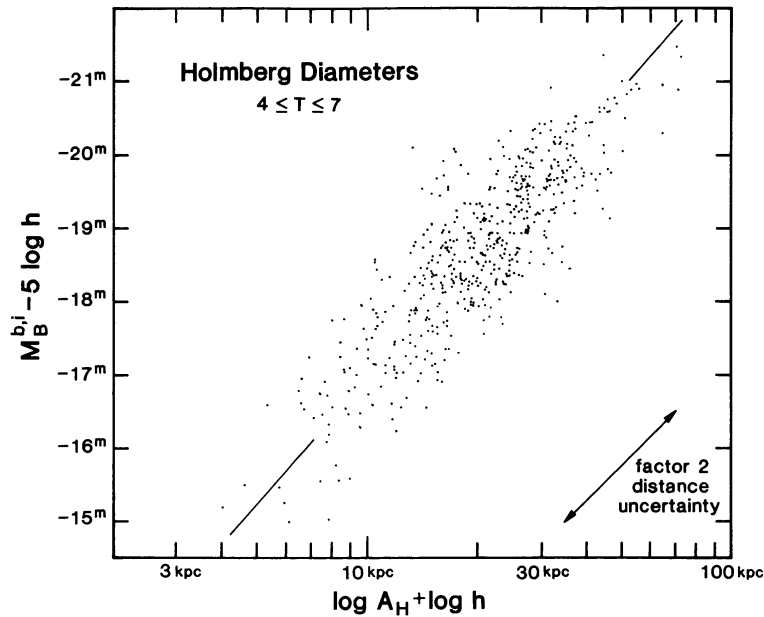


FIG. 1.—Absolute magnitude-intrinsic diameter diagram for 535 Sbc-Sd galaxies in the Holmberg system of diameters. Distances were determined from redshifts assuming $H_0 = 100h \text{ km s}^{-1} \text{ Mpc}^{-1}$. The straight line represents a least-squares fit. An equivalent plot can be made using Nilson diameters.

separate functions for the two galactic hemispheres. In the south,

$$N_H = 323 / \sin |b|, \quad (12a)$$

while in the north,

$$N_H = 323 / \sin b + [105 - 3.8b - 89 \cos (l - 140^\circ)]. \quad (12b)$$

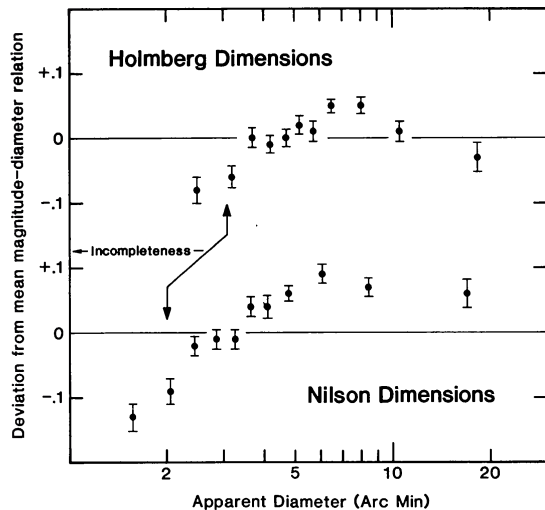


FIG. 2.—Deviations from the best-fit magnitude-diameter relation as a function of apparent diameter. The deviation plotted along the ordinate is $\Delta \log A = \log A - \log A^M$ where an individual galaxy has a diameter A and the best-fit diameter at the luminosity of the galaxy is A^M . The upper plot shows the trend of deviations when Holmberg diameters are used, and the lower plot shows the trend when Nilson diameters are used. Each point is the mean of ~ 50 galaxies, grouped by apparent diameter. Error bars are standard deviations of the mean.

The units of N_H are $10^{18} \text{ atoms cm}^{-2}$, 2.23 times one contour unit on the maps by Heiles (1975). The relationship between A_b and N_H is derived from a formula given by Burstein and Heiles (1978). A term has been dropped which describes variations in the gas to dust ratio and has an effect of less than 20%. The relationship between N_H and galactic coordinates l and b provide an analytic description of the distribution of high latitude H I in the maps by Heiles (1975). The 1σ scatter between “predicted” and observed N_H is 25% in N_H for $b < -20^\circ$ in the south and 20% for $b > 30^\circ$ in the north. We fail to predict the much larger values of N_H in the zones $150^\circ < l < 195^\circ$, $b > -45^\circ$ in the south and $330^\circ < l < 20^\circ$, $b < 40^\circ$ in the north but, probably because of heavy obscuration, the catalog contains very few galaxies that lie in either of those regions.

We feel that these corrections are a reasonable compromise between the complicated corrections in the RC2 which cannot be justified because of the uncertainties in the coefficients and corrections which do not attempt to account for large-scale variations as a function of galactic

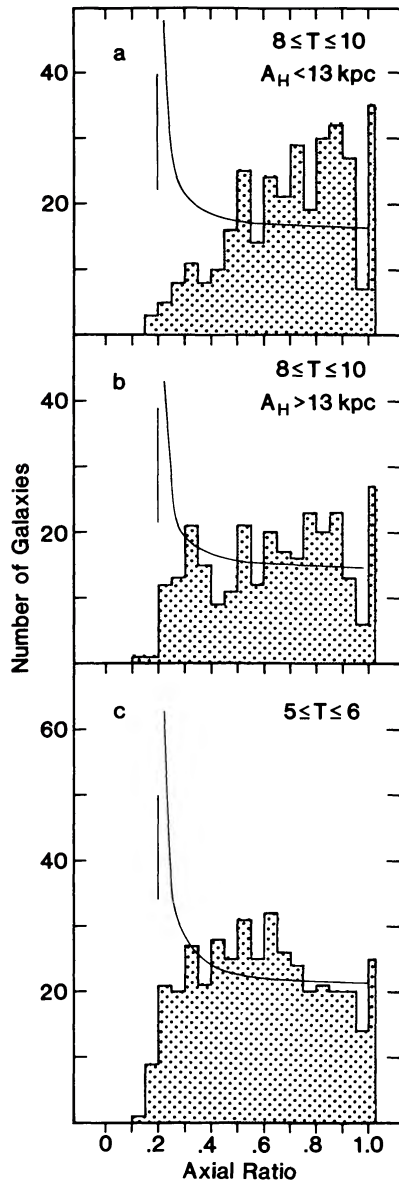


FIG. 3.—Histograms of the distribution of observed axial ratios for galaxies known to have redshifts less than 3000 km s^{-1} : (a) 314 galaxies with $8 \leq T \leq 10$ and $A_H < 13 \text{ kpc}$; (b) 281 galaxies with $8 \leq T \leq 10$ and $A_H > 13 \text{ kpc}$; and (c) 410 galaxies with $5 \leq T \leq 6$. The solid curves indicate the expected distribution if galaxies all have an intrinsic thickness of $r_0 = 0.20$, are randomly oriented, and are fairly sampled.

longitude and between the hemispheres. The amplitudes of our corrections are substantially lower than those in the RC2 (where $A_b \approx 0.2 \text{ mag}$ at the poles) but quite in line with the intent of the corrections by Sandage (1973). Sandage proposed that $A_b \approx 0$ at the poles, although by correcting to above the absorbing layer with the term $(\csc b - 1)$ he effectively used $A_b = 0.12 \text{ mag}$ at the poles. With our correction, there is 0.06 mag of absorption at the south galactic pole and zero absorption at the north galactic pole. In the north, the quadrant centered on

$l = 140^\circ$ deviates from a $\sin^{-1} b$ formulation in that N_H values are very low ($A_b = 0$ for $b \geq 53^\circ$), while in the quadrant centered on $l = 320^\circ$, N_H values are low near the pole ($A_b = 0$ for $b \geq 80^\circ$) but are *higher* than the $\sin^{-1} b$ prediction at mid-latitudes, $20^\circ < b < 50^\circ$. In all quadrants, in both hemispheres, the predicted absorption at locations with $|b| < 20^\circ$ are similar to the Sandage (1973) values.

f) Velocities and Line Profile Widths

In column 9, lines 1 and 2 are *heliocentric velocities* determined from the midpoint of the 21 cm profile (using the optical convention $v = c\Delta\lambda/\lambda_0$) and *velocities adjusted for solar motion* of 300 km s^{-1} toward $l = 90^\circ$, $b = 0^\circ$. Column 10, line 1 gives 21 cm *profile widths* at 20% of the peak intensity, while line 2 gives *uncertainties* associated with the velocity and line profile measurements. In column 11, line 1, there is a code which identifies the *telescope and spectral resolution* that was used to obtain the most useful profile on each system. The code is explained in Table 6.

The line profile width, W_{20} , is defined to be the full width at a level equal to 20% of the peak profile intensity (in km s^{-1}). The choice of the 20% level is a compromise between two empirical considerations. If the level were very high, the measurement would be sensitive to the level of peak intensity which depends on the details of the H I distribution within each galaxy. If the level were much lower than 20%, the line width would be too sensitive to noise in the observed spectrum. The error estimates are subjective, depending on baseline curvature, signal-to-noise, the steepness of the edges of profiles, and possible low intensity wings. Very occasionally, the error in both the profile width and the systemic velocity may be much larger than the estimated error if only one peak of a broad profile was sufficiently above the noise to be identified, or conversely, noise was mistaken for a second peak.

While flux might be lost because of the finite beam sizes, the H I profile width is not expected to be seriously altered for most normal galaxies. With only 13 exceptions, the Holmberg diameter was always smaller than the HPBW of the telescope. As long as the velocity turnover has been reached within this diameter the profile should be unaffected except in amplitude. This condition is likely to be realized in most galaxies, with the possible exception of extreme dwarf irregulars.

The profile widths that are listed were *corrected* for instrumental resolution. Consider the observed broadening of a rectangular profile by an amount δ_0 to be the product of internal motion δ_I and instrumental resolution δ_R :

$$\delta_0 = (\delta_I^2 + \delta_R^2)^{1/2}. \quad (13)$$

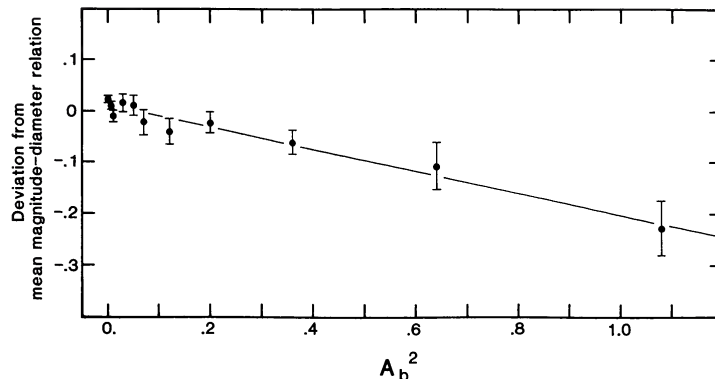


FIG. 4.—Deviations $\Delta \log A$ from the best-fit magnitude-Holmberg diameter relation as a function of galactic absorption squared. Galaxies have been binned by A_b , and means with mean deviations are plotted. A least-squares linear fit is illustrated.

The first two terms of the binomial expansion provide the approximation:

$$\delta_0 \approx \delta_I + \delta_R^2 / 2\delta_I. \quad (14)$$

The correction formula is

$$(W_{20})_{\text{corrected}} = (W_{20})_{\text{observed}} - \delta_c, \quad (15)$$

where $\delta_c = \delta_0 - \delta_I = \delta_R^2 / 2\delta_I$. From a number of profiles observed with two resolutions it was concluded that $2\delta_I \approx 100 \text{ km s}^{-1}$. Consequently, $\delta_c \approx 5 \text{ km s}^{-1}$ if the instrumental resolution was 22 km s^{-1} and $\delta_c \approx 0$ if the instrumental resolution was 5.5 km s^{-1} .

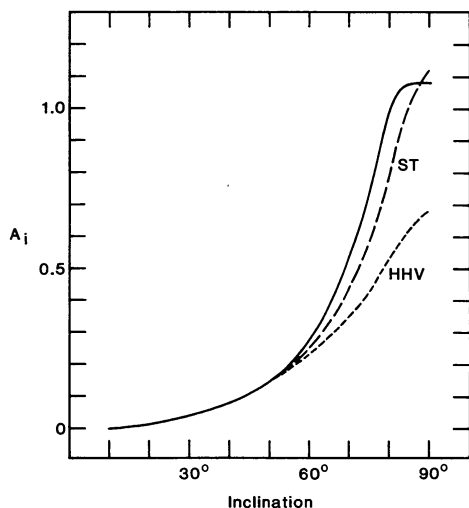


FIG. 5.—A comparison of the inclination corrections used in this catalog for all galaxies of types Sa through Im (solid curve) with those by Sandage and Tammann (1974) for Sc galaxies (ST) and those in the RC2 and by Heidmann *et al.* (1971) for Sa through Sdm systems (HHV). The corrections used in this catalog are almost identical to the corrections proposed by Holmberg (1958) for Sc galaxies.

g) H I Fluxes

The observed flux density in the neutral hydrogen line, adjusted for the effects of resolution, are recorded in column 12, line 1, and uncertainties are given in line 2. The correction factor to account for the effects of a finite beam are given in column 11, line 2. The integrated flux density F_H is

$$F_H = 0.236 \int S dv \ 10^6 M_\odot \text{ Mpc}^{-2}, \quad (16)$$

where S is the flux density in Jy and dv is in km s^{-1} . The 5σ detection limit is 0.09 Jy for a single observation with the polarization channels nonoverlapping. If the line width is 100 km s^{-1} then the corresponding limiting detectable signal is $2 \times 10^6 M_\odot \text{ Mpc}^{-2}$.

The neutral hydrogen flux densities have received a correction to account for the resolution effects of the finite observing beam, following Fisher and Tully (1975):

$$F_c = F_H \left[1 + (0.75 a_H^b / \theta)^2 \right]^{1/2} \left[1 + (0.75 b_H^b / \theta)^2 \right]^{1/2}, \quad (17)$$

where a_H^b and b_H^b are the major and minor Holmberg diameters corrected for galactic obscuration and θ is the HPBW of the telescope. The correction factor that is

TABLE 6
TELESCOPE AND RESOLUTION

Code	Telescope (m)	Resolution (km s^{-1})
1	91	22
2	43	22
3	91	5.5
4	43	5.5
5	100	5.5
6	100	22

recorded is $f_F = F_c/F_H$. Corrections are less than 50% except in three cases, and only 3% of the corrections are greater than 30%.

h) Intrinsic Parameters

We have assumed distances and determined *intrinsic diameters* (col. 13, line 1), *luminosities* and *absolute magnitudes* (col. 14, lines 1 and 2), *indicative total masses* (col. 15, line 1), *H I masses* (col. 15, line 2), *percentage of mass in the form of neutral gas* (col. 16), *indicative mass to light* and *H I mass to light ratios* (col. 17, lines 1 and 2).

Distances were generally derived from corrected systemic velocities and a Hubble constant of $H_0 = 100h \text{ km s}^{-1} \text{ Mpc}^{-1}$. Galaxies associated with the (6° radius) Virgo and (3° radius) Fornax clusters were placed at common distances determined by the barycentric velocity of each cluster ($10.7h^{-1}$ and $13.4h^{-1} \text{ Mpc}$, respectively). Very nearby galaxies with velocities less than 100 km s^{-1} were set at $1h^{-1} \text{ Mpc}$. There are *flags* in column 13, line 2, to identify those galaxies which are in Fornax (F), Virgo (V), or very local (L).

The intrinsic parameters were derived with the following formulae, where Dh^{-1} is the assumed distance:

$$\text{diameters: } A_H = 0.292 a_H^b Dh^{-1} \text{ kpc}, \quad (18)$$

$$\text{luminosities: } L_B = \text{dex} [0.4(5.48 - M_B^{b,i})] h^{-2} L_\odot, \quad (19)$$

$$\text{H I mass: } M_H = F_c 10^6 D^2 h^{-2} M_\odot, \quad (20)$$

$$\text{total mass: } M_T = 2.02 \times 10^4 A_H (W_{20}/\sin i)^2 h^{-1} M_\odot. \quad (21)$$

The total mass estimator is the Keplerian approximation to the mass interior to the Holmberg radius, the formulation proposed by Faber and Gallagher (1979):

$$M_T = V_H^2 A_H / 2G, \quad (22)$$

where V_H is the circular velocity at the radius $A_H/2$. The assumption is made that the mass is spherically distributed interior to the Holmberg radius, which leads to an overestimate of the mass inside this radius. However, the effect is probably more than offset by a neglect of the mass at exterior points. The coefficient in equation (21) was determined by comparison of our line width parameter and values for the rotational velocity at the Holmberg diameter for 22 galaxies tabulated by Faber and Gallagher:

$$0.5W_{20}/\sin i = 1.2V_H. \quad (23)$$

If $i < 30^\circ$, then total mass was *not* calculated because of the large deprojection uncertainty.

IV. SYNOPSIS OF THE SAMPLE

In total, 1171 of 1787 candidates (66%) were satisfactorily detected. Of the 1252 galaxies in the original sample, 919 (73%) were detected. Of 247 galaxies that were observed from the supplemental list drawn from the UGC, 103 (42%) were detected.

Histograms of the observed velocities are given for the original sample and supplemental UGC sample in Figure 6. There are two strong biases that must be kept in mind regarding these samples. In the first place, they *excluded* galaxies which had already been observed spectroscopically at the time the survey began. Second, the existence of the Local supercluster, at a mean redshift of $\sim 1000 \text{ km s}^{-1}$, implies there must be a gross departure from a uniform distribution of galaxies.

From an extrapolation of the histogram for the original sample it can be crudely estimated that 100 to 150 galaxies were not detected because of the velocity cutoff at 3000 km s^{-1} imposed by the receiver bandwidth. In fact, in a very nonsystematic way, observations were made with coverage of higher redshift intervals, and 39 galaxies from the original sample were detected. Hence, it is expected that $\sim 10\%$ of the galaxies in the original sample were not detected because they have systemic velocities greater than 3000 km s^{-1} . It would follow that for $\sim 15\%$ of the original sample the velocities were in the observed range, but the H I fluxes fell below our threshold. Another few percent might have been confused with neighbors or with local emission.

It is possible to estimate our completion as a function of systemic velocity, if one ignores for the moment the caveats regarding the biases in the sample. Let the function $N(<v)$ describe the number of galaxies detected with velocities less than v . The observed relation-

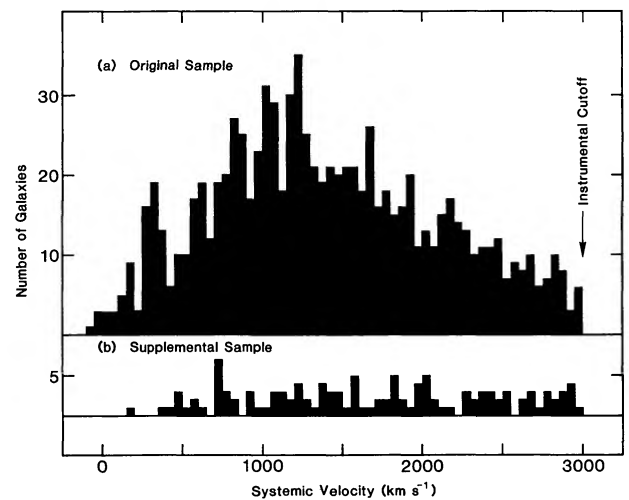


FIG. 6.—Histograms of the systemic velocities of the detected galaxies. (a) The original observing list of 1252 galaxies. (b) The supplemental UGC sample which provided completion to specific size limits.

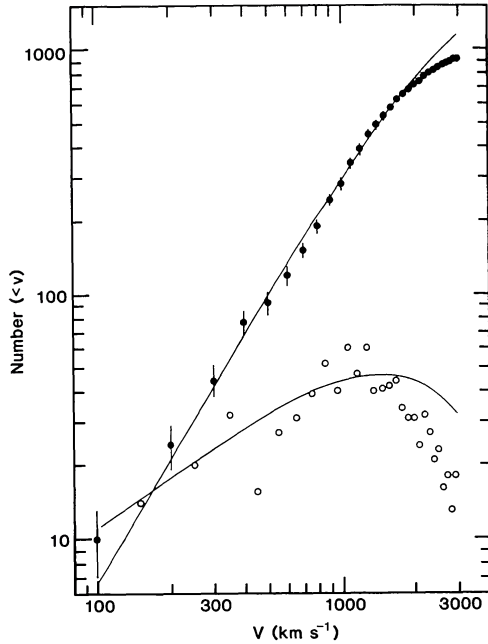


FIG. 7.—The number of galaxies in the original sample of 1252 galaxies with systemic velocities less than v , as a function of v (points with error bars), and the number of galaxies in this sample with velocities in 100 km s^{-1} increments of v (open circles). The solid curves illustrate a fit by a Schechter-type luminosity function with a slope parameter $\alpha = -1.6$ and a cutoff parameter $M_H^* = 3 \times 10^9 M_\odot$.

ship is displayed in Figure 7. It is seen that there is a linear dependence of $\log N$ on $\log v$ for $v < 1500 \text{ km s}^{-1}$.

Now let $n(v_1)$ describe the number of galaxies per unit volume that have sufficient flux to be observed at a redshift v_1 . Then

$$N(<v) = \frac{\Omega}{H_0^3} \int_0^v n(v_1) v_1^2 dv_1, \quad (24)$$

where Ω steradians of sky has been inspected and H_0 is the Hubble constant. The term $n(v_1)$ can be estimated by assuming the Schechter (1976) luminosity function, but replacing luminosities with H I masses, M_H :

$$\begin{aligned} \phi(M_H) dM_H &= \phi^*(M_H/M_H^*)^\alpha \\ &\times \exp(-M_H/M_H^*) d(M_H/M_H^*). \end{aligned} \quad (25)$$

Then

$$n(v_1) = \int_{M_H^{\text{lim}}}^{\infty} \phi(M_H) dM_H, \quad (26)$$

where the lower integration limit is defined as a function of velocity through equation (20), assuming a minimum detectable signal F_c^{lim} .⁵ A reasonable fit to the observed dependence of $N(<v)$ with v is obtained at low velocities if the parameters $\alpha = -1.6$ and $M_H^* = 3 \times 10^9 h^{-2} M_\odot$ are chosen (solid curves in Fig. 7). Evidently, there is substantial incompleteness at $v > 1500 \text{ km s}^{-1}$.

In our system of magnitudes, Schechter's (1976) parameter L^* has the value $1 \times 10^{10} h^{-2} L_\odot$, so $M_H^*/L^* = 0.3$. This ratio is consistent with the values found for intrinsically luminous galaxies in Tables 1 and 2. The slope parameter, α , is steeper than the $\alpha = -1.25$ found for the luminosity function in blue light, but such an effect is consistent with the well-known trend for the ratio M_H/L to increase toward fainter galaxies.

The differential relationship, the observed number of galaxies in intervals of velocity, is shown in Figure 7 as open circles. This relationship is noisier but more sensitive to the location of the turnover from a power law and again suggests that the sample rapidly becomes incomplete beyond $v \approx 1500 \text{ km s}^{-1}$. Faith in the luminosity function fit would lead to the conclusion that ~ 200 galaxies with $v > 1500 \text{ km s}^{-1}$ are missing. That is, one galaxy in three with sufficient flux to have been detected was missed in the interval $1500 < v < 3000 \text{ km s}^{-1}$.

Of course, the fact that the peak in the differential relationship is at a velocity characteristic of the Local supercluster may not be fortuitous. Couple to this concern the exclusion from the sample of those galaxies with known velocities at the time the survey began and the ill-defined mixture of morphological types. It would not be wise to consider the fit of a luminosity function as other than suggestive or to consider the argument for completion to be totally compelling. However, similar conclusions regarding completion can be drawn from Figure 6b, the histogram of the detected velocities of galaxies in the supplemental UGC sample. It is evident that many of the nondetections in this sample must have systemic velocities greater than the cutoff at 3000 km s^{-1} , although the observed distribution is too broad to permit an estimate of the actual numbers. All but 12 of the galaxies with velocities less than 1000 km s^{-1} are earlier than Sc or within 30° of the galactic plane, or in the Virgo cluster. Neither this supplementary sample nor any other investigation published since our original

⁵The assumption is required that the sample is H I flux limited. There is a correlation between observed flux and apparent dimension such that for a given F_c^{lim} there is an associated a_H^{lim} (with some type dependence). There was a size cutoff associated with our original sample of $a_H^{\text{cut}} \approx 2.5$. If $a_H^{\text{lim}} \gg a_H^{\text{cut}}$ (i.e., the sample really is H I flux limited) then our percentage detections would be low, while if $a_H^{\text{lim}} \ll a_H^{\text{cut}}$ then our detection statistics would be very high, and F_c^{lim} would effectively be set by the dimensions cutoff (i.e., detections for the smallest systems would be well above the noise). From our detection statistics, we submit that $a_H^{\text{lim}} \approx a_H^{\text{cut}}$.

sample was defined has demonstrated the existence of a significant number of galaxies that should have been in our sample but were not.

Consequently, our conclusions are that, taken in conjunction with redshifts in the literature, this sample is very complete for galaxies (i) with systemic velocities less than 1000 km s^{-1} , (ii) of types Sc and later, (iii) and

Holmberg diameters greater than $3'$, (iv) at $|b| > 30^\circ$, and (v) with $\delta > -33^\circ$.

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Note added in proof.—Kennicutt (private communication) has pointed out an error in the distance-dependent quantity M_H in a few instances in Table 1. The distances to galaxies flagged F (for Fornax), V (for Virgo), or L (for Local) were to be treated as special cases, but they were not. An erroneous value of M_H can be corrected by multiplying the tabulated value by $(100 D/V_0)^2$, where V_0 is the systemic velocity of the galaxy and the distance D is 13.4 Mpc for a galaxy in the Fornax cluster, 10.7 Mpc for a galaxy in the Virgo cluster, and 1.0 Mpc for a local system. The errors in M_H propagate to the ratios M_H/M_T and M_H/L . The other distance-dependent quantities (dimensions, luminosities, and total masses) were calculated correctly.

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